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# 3D/4D AREA NAVIGATION SYSTEM DESIGN, DEVELOPMENT, AND IMPLEMENTATION

Volume II Support Data and Program Listings

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SECTION 1  
INTRODUCTION AND  
SUMMARY

1.1 Summary of Volume II

This volume describes the detailed design and final implementation of the software for the 3D/4D Base and ILS and 2D/Time Control Systems. The systems were constructed by modifying the software structure used for the ANS-70A Area Navigation System.

A description of the 3D/4D software effort requires some knowledge of the ANS-70A software structure. A brief functional description of the ANS-70A software is given in the following paragraphs.

Sections 2 and 3 describe the software modifications used to effect the BASE and 2D/Time Control Systems respectively. Section 4 presents the RNAV to ILS interface design procedure. Sections 5 and 6 present the development of the lateral and longitudinal control laws respectively. Program listings are found in the appendices.

1.2 Overview of ANS-70A Software System

The ANS-70A software system has several different priority levels. The highest level of software functions have been assigned to processor channels. Each channel is allocated processing time on a sequential basis. Channels of particular interest for the present treatment are the Navigation and CDU Application Channels. Major functions assigned to these channels are illustrated in Figures 1-1 and 1-2.

The classification of major functions for the Navigation Channel remains unchanged for the 3D/4D systems. Secondary functions have been added to the software modules that support the major tasks of Aircraft Systems Coupler (ASC) Input, Lateral Navigation, and ASC Output. Navigation tasks that are unique to the 3D/4D Base and 2D Plus Time Control systems are described in Sections 2.0 and 3.0 respectively.

the CDU Channel. In addition to providing software for the CDU interface, this channel supervises tasks related to navigation support and Flight Plan Management.

Background support for the navigation function is provided by routines called the Radio Selection Program, Kalman Filter, and the Flight Plan Monitor. Each of these programs is called on a cyclic basis by the CDU Main Program. The first two routines are used without modification for the 3D/4D systems.

The Flight Plan Monitor serves as an interface between the Navigation software and the Flight Plan Editor. A primary task for the Flight Plan Monitor consists of retrieving flight plan parameters required by the Lateral and Vertical Navigation routines. Another major task consists of supervising flight plan maintenance that is required at waypoint passage. 3D/4D modifications to the Flight Plan Monitor are given in later sections of this volume.

Figure 1-3 illustrates software interfaces that are required for Flight Plan Management. Initial verification of flight plan revisions entered via the CDU are performed by the CDU Software. If a given revision fails initial tests, processing of the entry is discontinued and error annunciation is given on the CDU scratchpad. Valid revisions are recorded in the Flight Event Table by calling the Flight Plan Editor. Flight Plan parameters required by the Navigation software are then updated by the Flight Plan Monitor.

In addition to recording flight plan revisions, the Flight Plan Editor performs all geometry computations that are required as internal flight plan parameters (e.g., distance and course information). The impact of Base Offsets on the Flight Plan Editor is treated in Section 2.2.

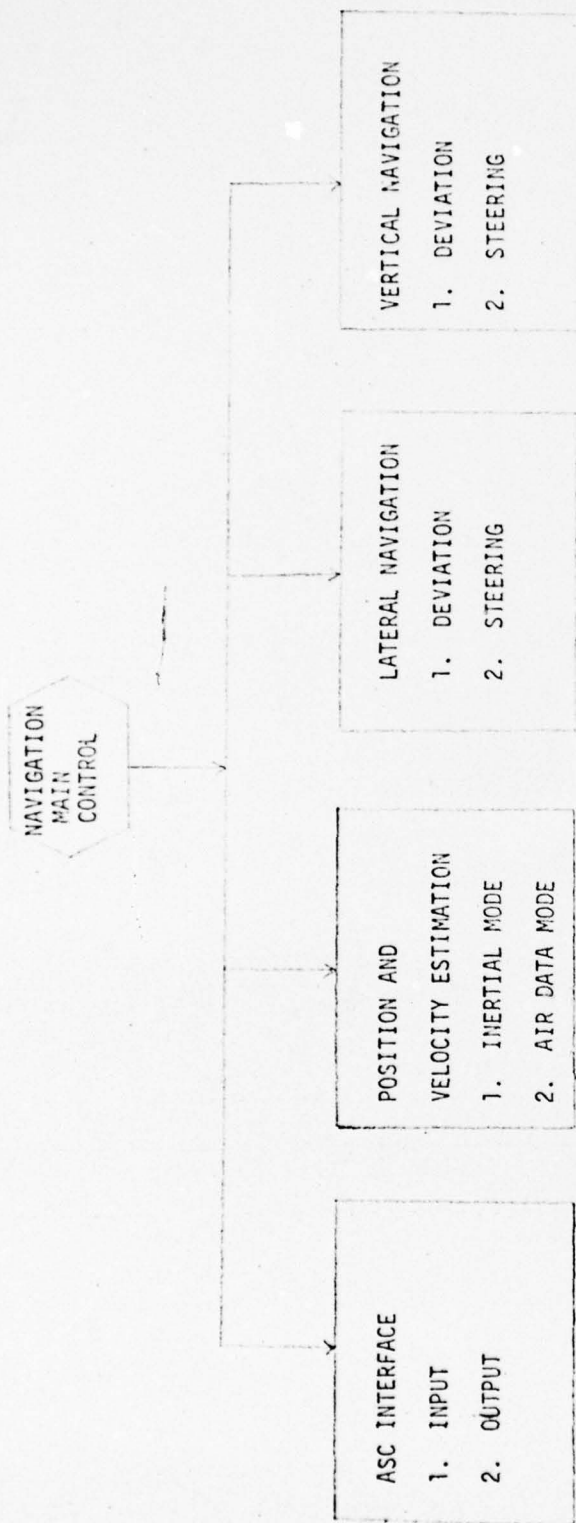


FIGURE 1-1

Major ANS-70A Functions for the Navigation Channel

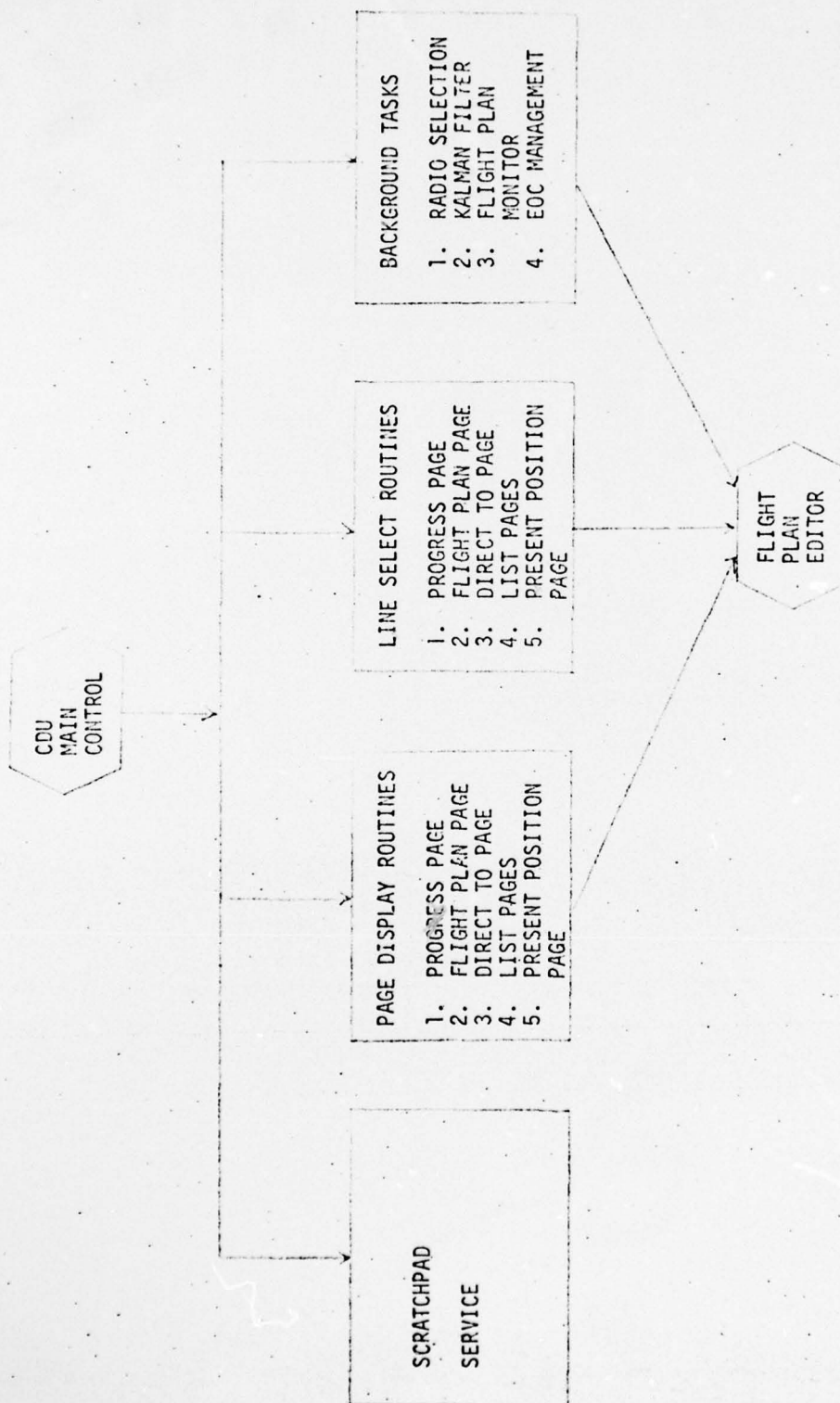


FIGURE 1-2

Major ANS-70A Functions for the CDU Channel



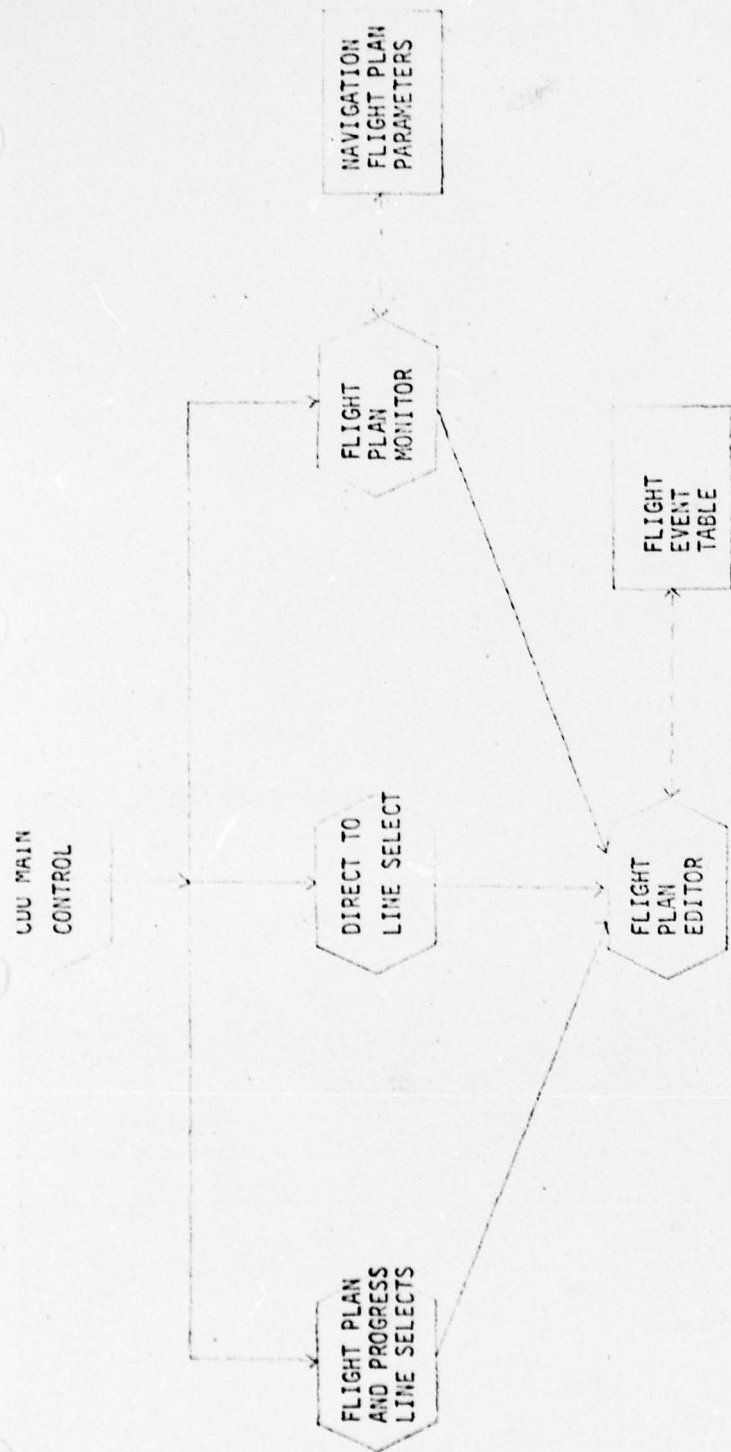


FIGURE 1-3  
ANS-70A Software Interfaces for Flight Plan Management

## Section 2 3D/4D BASE SYSTEM

A major goal for the software design stage was to construct a software package that minimized the impact of 3D/4D operational requirements on the existing ANS-70A Software Interfaces. In addition to ensuring system integrity, additional goals consisted of ensuring flexibility for additional changes and minimizing core requirements to the extent that software overlays could be avoided.

A core reduction effort was required before the 3D/4D tasks could be added to the ANS-70A configuration. Approximately 500 words of core were freed for 3D/4D usage by deleting software for Holding Patterns, the Inertial mode of navigation, Heading and Armed modes, and Commanded Vertical Angle. An additional 1500 words were gained by reducing the Data Base to 1000 words.

Once the core reduction effort was completed, the following major software tasks were implemented:

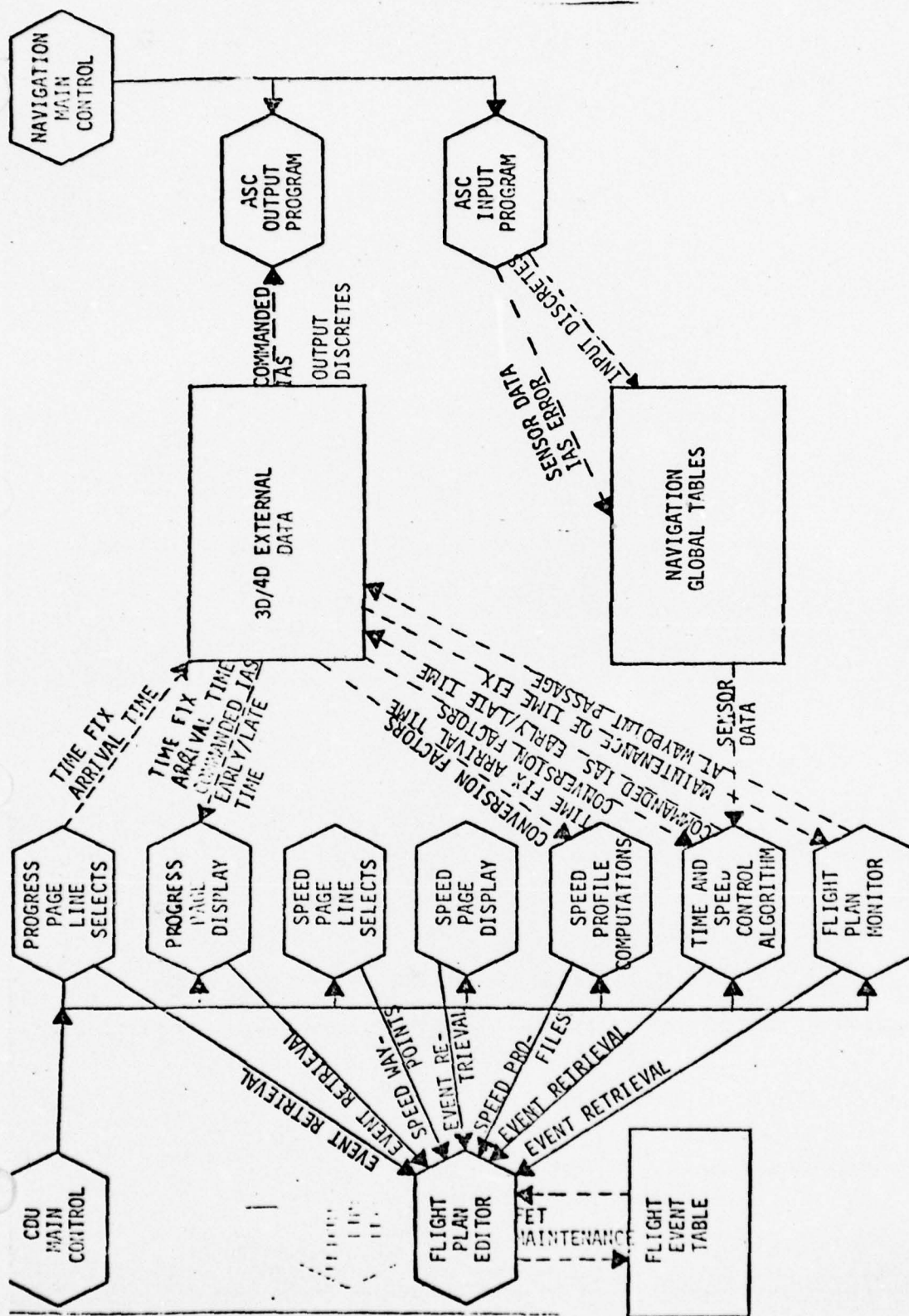
- 1) External Data Files
- 2) Base Offsets
- 3) Speed Page
- 4) Speed Profile Algorithm
- 5) Time Control Algorithm
- 6) Navigation Modifications
- 7) ASC Modifications

Each of these items is explained in detail by sections 2.1 through 2.6.

Software and data interfaces required for the major software tasks are illustrated in Figures 2.1 through 2.3. Routines for Base Offsets, the Speed Page, the Speed Profile Algorithm, and the Time Control Algorithm are supervised by the CDU Main Control Program. The ASC interface and navigation computations are controlled by the Navigation Main Control Program.







SOFTWARE INTERFACES FOR TIME CONTROL

FIGURE 2-2



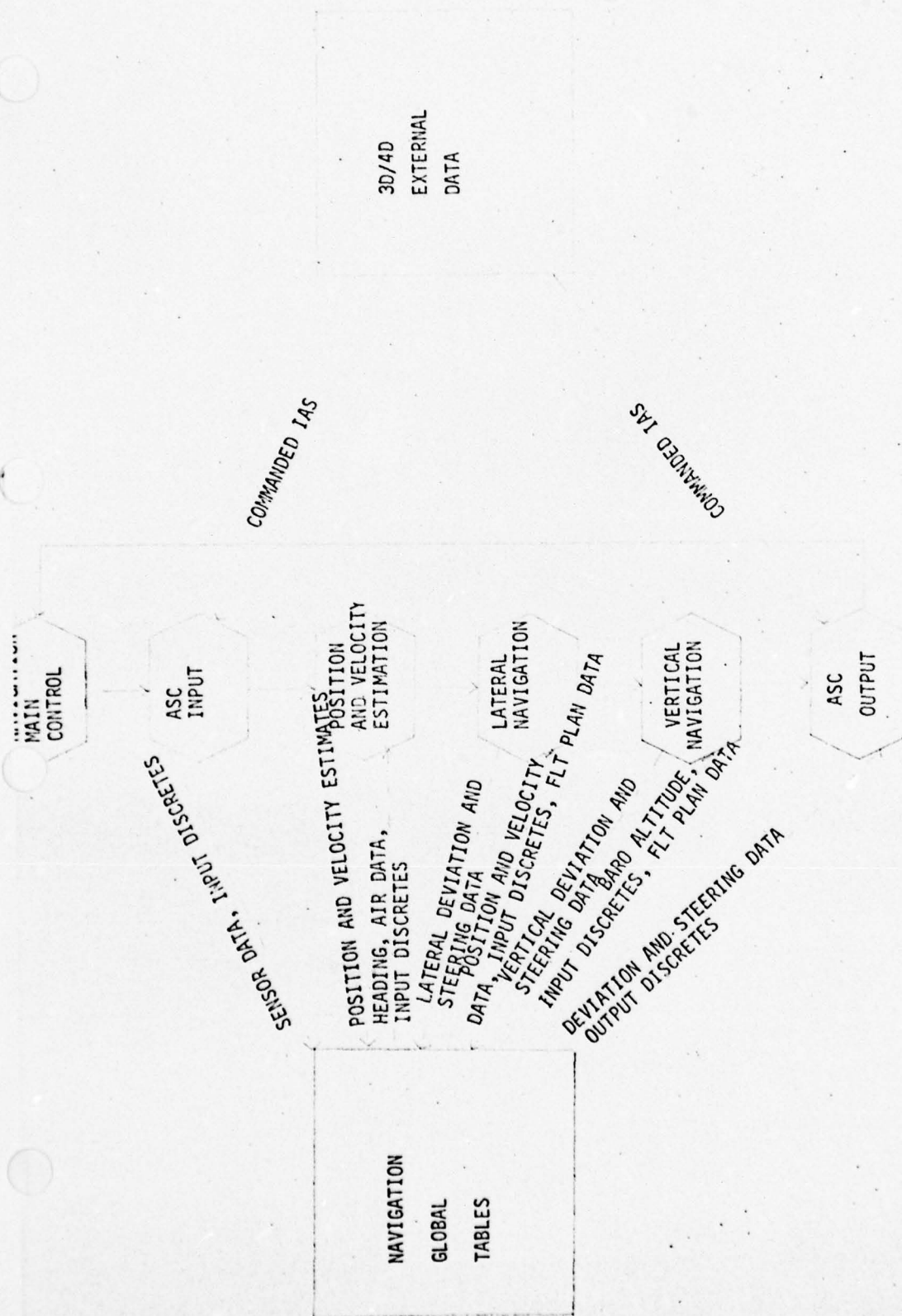


FIGURE 2-3  
Software Interfaces for Navigation and ASC Interfaces

## 2.1 External Data Files

Program descriptions given in later sections of this volume reference data parameters whose data declarations are external to the given programs. The purpose of this section is to provide data descriptions for this external data set.

Data parameters required by more than one program have been classified by function into three basic categories. Separate compilation units have been assigned to each class of parameters for core allocation purposes. Each unit has been given a corresponding INSERT file which provides data declarations. Programs that require data declarations for a given function include an INSERT statement for the appropriate file.

The three basic EXTERNAL data files used for the Base System are 1) 3D/4D External Data File, 2) Flight Plan Editor File, and 3) the Navigation Global Tables File. A description of the data parameters assigned to each file is given below.

### 2.1.1 3D/4D External Data

The majority of EXTERNAL variables that are unique to the 3D/4D Task II effort are defined by the 3D/4D External Data Insert and 3D/4D External Data Preset files. Data definitions for this set of variables are given below.

<u>Symbolic Name</u>	<u>Assigned Value</u>	<u>Description</u>
VALID	0	Used to assign a valid status to 3D/4D Integer parameters that are treated as boolean data.
INVALID	1	Used to assign an invalid status to the same set of Integer parameters described for the VALID synonym.

The following list of synonyms are used for VCOMIF.

<u>Synonym Name</u>	<u>Assigned Value</u>	<u>IAS Data Display On Progress Page</u>	<u>Description</u>
IASVALID	15	Value of IAS that is maintained in VCOMI.	A valid commanded IAS has been calculated by the Time and Speed Control algorithm.
NODATA	31	----	No IAS has been entered on the Speed Page.
IVGMT	14	GMT?	Either GMT has not been entered on the Present Position Page, or a power interrupt of duration exceeding two seconds has invalidated GMT.
IVTAS	13	TAS?	The Air Data Sensor input for TAS is invalid.
IVALT	11	ALT?	The Altimeter Sensor input for Baro Altitude is invalid.
IVCOCH	7	CRS!	A Teardrop Procedure is required to capture at least one of the legs used for Time Control computations.

#### Integer Declarations

<u>Symbolic Name</u>	<u>Initial Value</u>	<u>Description</u>
IASMSK	"FFFFFF00"	Mask used in "AND" operations for the removal of the IASF component.
TFIX	0	ASCII identifier of the waypoint assigned as the Time-Fix.
TCOM	0	Commanded time of arrival for the Time-Fix. TCOM is recorded in GMT units (i.e., as a fraction of 1200 hours).
TFIXF	Invalid	Validity flag for TFIX.
VCOMIF	Invalid	Validity flag for VCOMI and VCOMT.
TCOMF	Invalid	Validity flag for TCOM.
TIMERF	Invalid	Validity flag for TIMERR.
COMPRF	INVALID	Validity flag that is assigned a VALID status by the Flight Plan Monitor whenever a flight plan revision has occurred. SPDPFR, the Speed Profile Routine, assigns an INVALID status to COMPRF whenever speed profile computations are performed.



<u>Symbolic Name</u>	<u>Initial Value</u>	<u>Description</u>
TCONF	INVALID	Validity flag that is assigned a VALID status by the speed profile routine whenever speed profiles are updated. TCONF is assigned an INVALID status whenever Time Control computations are performed.

#### Real Declarations

<u>Symbolic Name</u>	<u>Initial Value</u>	<u>Description</u>
MINR	.00000001	Minimum magnitude that REAL numbers may be assigned on the U-1108.
VCOMI	.050	Commanded IAS displayed on the Flight Progress Page and IAS instrument. VCOMI is a fraction of 1000 kts.
VCOMT	.050	Commanded TAS calculated by the Speed and Time Control Algorithm.
MINRATE	.038566097	Value of 40 kts/min Speed Gradient. $\text{MINRATE} = 1 / \{ (40 \text{ KT/MIN}) / (1000 \text{ KT LAT VEL BASE}) * 60 \text{ MIN/HR} * 10.8039624 \text{ HRS LAT TIME BASE} \}$
EARLY	.0	Expected arrival time error for the Time-Fix. EARLY is expressed in Lateral Navigation Time Units. The Early Lat. Display on the Flight Progress Page is based on the value of EARLY. A positive value indicates a late status.
TIMERR	.0	Magnitude of EARLY. TIMERR is used by the CDU software for display of EARLY/LATE data on the Progress Page.



### 2.1.2 Flight Plan Editor Files

Lateral and vertical flight plan parameters maintained by the Flight Plan Editor are illustrated in Figures 2-4 and 2-5. The IASR, IASI, IASF, POFSI, and POFSIC components are the only parameters that are unique to the 3D/4D systems. Descriptions for this set of parameters are given below.

The component structure for IAS parameters is given as follows:



The IASF component is used to record the status of the IAS entry. Synonyms used for this parameter are given below.

<u>Synonym Name</u>	<u>Assigned Value</u>	<u>Description</u>
PIAS	7	Pilot-Defined IAS.
PRQUOTE	11	Profile IAS Displayed on the Speed Page as ".
PRDOWN	13	Profile IAS Displayed on the Speed Page as ↓.
PRUP	14	Profile IAS Displayed on the Speed Page as ↑.
NOIAS	15	No IAS Specified.

The first 24 bits of the entry are used to record the actual IAS magnitude as a REAL-valued fraction of 1000 kts. Although real arithmetic operations are required for the 3D/4D Speed Control and Profile Algorithms, it is also necessary to provide the capability of integer masking operations for the IASF component. Thus, the user is provided with both REAL (IASR) and INTEGER (IASI) component declarations for the IAS parameter.

WORD NUMBER	LABEL	MEANING
-3	VERS	Current Flight Plan Version (VERSFE)
-2	ABEVNO	Absolute Event Number for Event
-1	CNTRWORD	Control Word
0	WYPTID	Waypoint ID
1	WYPTLAT	Waypoint Latitude
2	WYPTLONG	Waypoint Longitude
3	WYPTVAR	Magnetic Variation (Not Supplied by the Editor)
4	POFS/POFSF	Parallel Offset (POFSFE)
5	AOFS	Along Track Offset and Status
6	DFTO	Distance from "TO" LE
7	APOF	Along Path Offset (Always = AOFS)
8	CRSI	Course In
9	CRSO	Course Out
10	AWYID	Airway ID
11	IASR/IASI IASF	Indicated Airspeed Word and Flag

FIGURE 2-4  
Lateral Event Parameters Maintained by the  
Flight Plan Editor

WORD NUMBER	LABEL	MEANING
-3	VERS	Current Flight Plan Version (VERSFE)
-2	ABEVNO	Absolute Event Number for Event
-1	CNTRWORD	Control Word
0	WYPTID	Waypoint ID
1	WYPTLAT	Waypoint Latitude
2	WYPTLONG	Waypoint Longitude
3	WYPTVAR	Magnetic Variation (Not Supplied by Editor)
4	POFS	Parallel Offset (POFSFE)
5	AOFS	Along Track Offset
6	DFTO	Distance from "TO" LE
7	APOF	Along Path Offset (Always = AOFS)
8	VPAI	Vertical Path Angle In
9	VPAO	Vertical Path Angle Out
10	ALTD	Altitude at VE

FIGURE 2.5  
Vertical Event Parameters Maintained by the  
Flight Plan Editor

The POFS component is used to record both parallel and base offsets. This component is defined as follows:

POFS/POFSI

POFSF

Base and Parallel offsets are treated as Real-valued fractions of  $\pi$  times the radius of earth in nautical miles. The component declarations for POFS, POFSI, and POFSF are similar in structure to IASR, IASI, and IASF, respectively. Synonyms applicable to the POFSF component are given below. Figure 2-6 illustrates the Base Leg waypoints identified by the POFSF synonyms.

POFSF Synonyms

<u>Symbolic Name</u>	<u>Assigned Value</u>	<u>Description</u>
PARALLEL	7	Identifies Parallel Offset Entry. The synonym "PARALLEL" serves a dual purpose. The Flight Plan Editor monitors the POFSF component for one-to-one replace edits to determine the Insertion/Deletion of Parallel Offsets for the Flight Plan. Procedures that use the Flight Plan Editor "GET" routines test the POFSF component for a value of "PARALLEL" to determine the existence of a Parallel Offset.
BASEOFST	8	Identifies the POFSI component as a base offset. This value is used to inform the Flight Plan Editor that the Flight Plan Revision is for a Base Offset.



<u>Symbolic Name</u>	<u>Assigned Value</u>	<u>Description</u>
STRT90	13	Identifies initial waypoint associated with a base offset that provides a 90 degree capture with the localizer leg.
END90	11	Identifies final waypoint associated with a base offset that provides a 90 degree localizer capture.
STRTBASE	12	Identifies initial waypoint associated with a base offset that provides a shallow capture of the localizer leg.
ENDBASE	10	Identifies waypoint whose CRSI component defines the Base Leg for a Base Offset defined for a shallow localizer capture angle.
INTERCEP	9	Identifies waypoint whose CRSI and CRSO components define the intercept point for localizer capture.
NOPOFS	15	No offset entry has been made.
CANCEL	14	Identifies an edit that cancels an existing offset.

POFSE is used to record the value of an existing Parallel or Base Offset.

PFSTAT is used to record the present status of offsets. Synonyms PARALLEL, BASEOFST, and NOPOFS are used to indicate offset status.

With the exception of the Flight Plan Editor, POFSE and PFSTAT are treated as read-only parameters. Any requirement to change the offset parameters is accomplished via a one-to-one replace edit with the desired change specified via the POFSE component.

### 2.1.3 Navigation Global Tables

External parameters required for navigation computations are stored in the Navigation Global Tables. A single version of this file is used for all three Task II systems. The remaining portion of this section describes 3D/4D modifications to the Navigation Global Tables.

The ANS-70A version of the ADHD table has been expanded to include sensor inputs for Indicated Airspeed Error, Localizer Deviation, Glideslope Deviation, and HSI Course Input. A description of the ADHD components used for the 3D/4D systems is given below.

<u>Symbolic Name</u>	<u>Component Position</u>	<u>Description</u>	<u>Validity Flag</u>
LAT	0	Aircraft Latitude as maintained by the Lateral Filter.	N/A
LONG	1	Aircraft Longitude as maintained by the Lateral Filter.	N/A
PSIM	2	Magnetic Heading	PSMF
BALT	3	Barometric Altitude	BALF
TAS	4	True Air Speed	TASF
VRT	5	Vertical Rate (not input for the 3D/4D system)	N/A
PALT	6	Pressure Altitude (not input for the 3D/4D system)	N/A
DELV	7	Indicated Air Speed Error	DELVF
LOC	8	Localizer Deviation	LOCF
GS	9	Glideslope Deviation	GSF
HSICRS	10	HSI Course Input	HSICRSF

ANS-70A Lateral Deviation computations always reference the parent waypoint of the Lateral To-Event. Similar computations for the 3D/4D system use the leg intersection of the path actually being flown as the frame of reference. The following set of parameters is used for this task:

<u>Symbolic Name</u>	<u>Description</u>
TOLEG	Array used to record the coordinates of the leg intersection defined for the Lateral To-Event.
BFLEG	Work area used to record bearing from the leg intersection to the aircraft.
BTLEG	Work area used to record bearing from the aircraft to the leg intersection.
DTLEG	Distance between the aircraft and the oncoming leg intersection.

Parameters used to record ASC input discretes that are unique to the 3D/4D systems are given below.

<u>Symbolic Name</u>	<u>Description</u>
APENG	Status of the Auto-Pilot-Engaged discrete. APENG is assigned a TRUE status whenever the Area Nav system is coupled to the Auto-Pilot.
RNAVENG	Status of the RNAV-Engaged discrete. RNAVENG is assigned a TRUE status whenever the RNAV system provides lateral navigation and possibly lateral steering.
VNAVENG	Status of the VNAV-Engaged discrete. VNAVENG is assigned a TRUE status whenever the RNAV system provides vertical navigation and possibly vertical steering.



## 2.2 Base Offsets

Figure 2-6 illustrates the software interfaces that have been implemented for the Base Offset function. The key interface is provided by the Flight Plan Editor Utility Module. A description of this module will follow a brief summary of the roles played by the CDU Line-Select and Flight Plan Monitor modules.

Classification of a CDU scratch-pad entry as a candidate for a Base Offset is performed by the CDU software. Base Offset entries are permitted for waypoints that appear on the Flight Plan, Progress, or Speed pages. Valid candidates are passed onto the Flight Plan Editor Utility Module for additional processing. "ERROR" is annunciated on the scratch-pad if either of the following conditions invalidates the edit: range tests are failed, or the existing flight plan already includes a parallel offset.

Automatic cancellation of an existing Base Offset occurs following passage of the last waypoint associated with the given offset. This task is performed by the Flight Plan Monitor. The Base Offset is cancelled whenever waypoint passage occurs for the waypoint whose POFSF component has an assigned value of INTERCEP or END90.

The Flight Plan Editor Utility Module provides an interface between the CDU software and a modified version of the ANS-70A Flight Plan Editor. All flight plan revisions entered by the pilot are routed through this module. Most of the major software tasks required for the Base Offset function are provided by this module. The remaining portion of the section provides a description of tasks that have been implemented for the Flight Plan Editor.

A primary task consists of verifying geometry requirements for Base Offset entries. Figure 2-7 illustrates the basic geometries for Base Offsets.



Geometry requirements for the Two-Waypoint configuration are given as follows:

$$(1) \quad X = ||\text{COCH}(W_{I-1})|-90^\circ| \leq 2^\circ$$

$$\text{and } |\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$$

$$(2) \quad X = ||\left[ \sum_{j=I-1}^I \text{COCH}(W_j) \right] |-180^\circ| \leq 2^\circ$$

$$\text{and } |\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$$

$$\text{and } Y = ||\text{COCH}(W_I) |-90^\circ| \leq 2^\circ$$

$$\text{and } |\text{POFS}(\text{WKPTR})| * (\pi Y / 180^\circ) \leq 0.2 \text{ NM}$$

Geometry tests that must be performed for the Three-Waypoint configuration are given as:

$$(1) \quad X = ||\text{COCH}(W_{I-1})|-90^\circ| \leq 2^\circ$$

$$\text{and } |\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$$

$$(2) \quad X = ||\left[ \sum_{j=I}^{I+1} \text{COCH}(W_j) \right] |-90^\circ| \leq 2^\circ$$

$$\text{and } |\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$$

$$\text{and } Y = ||\left[ \sum_{j=I-1}^{I+1} \text{COCH}(W_j) \right] |-180^\circ| \leq 2^\circ$$

$$\text{and } |\text{POFS}(\text{WKPTR})| * (\pi Y / 180^\circ) \leq 0.2 \text{ NM}$$

This set of tests is intended to provide protection against absurd offset geometries. If the geometry is found to be valid, POFS and POFSF components are updated for the offset waypoints and recorded in the Flight Event Table. If the geometry requirements are not met, control is returned to the CDU software. In either case, a return argument is used to indicate the status of the Base Offset entry.

A second major task consists of enforcing a set of operational rules that have been imposed on all flight plan revisions. The purpose of this set of rules is to insure that flight plan revisions do not invalidate the geometry for an existing Base Offset.

Special operational rules are required for DIRECT TO entries. As with the ANS-70A system, an existing Parallel Offset is cancelled whenever a valid DIRECT TO revision is made. A Base Offset, however, is cancelled only if the resulting flight plan revision affects the Base Offset waypoint configuration. A summary of the logic used to cancel Base Offsets for DIRECT TO entries is given in Table 2-1.

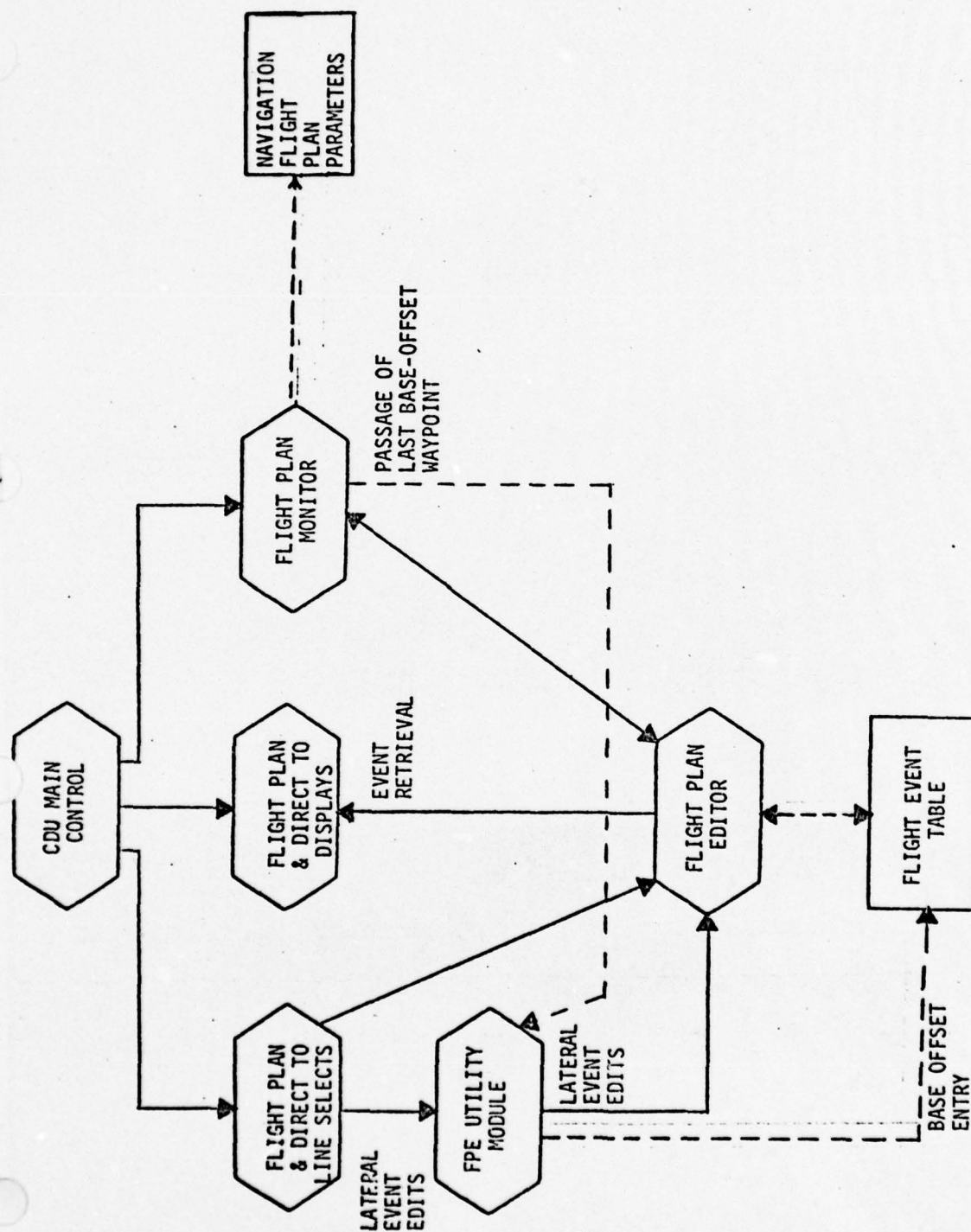
Operational rules that are implemented for remaining flight plan revisions are given as follows:

- 1) A Base Offset entry is to be inhibited whenever the current flight plan includes a Parallel Offset. The converse is also true, i.e., a Parallel Offset entry is not allowed for a flight plan that already includes a Base Offset.
- 2) The magnitude of an existing Base Offset may be revised at any time. A Parallel Offset may be overwritten at any time by entering another Parallel Offset into the flight plan.
- 3) No flight plan revision is allowed that would change the geometry of an existing Base Offset configuration.

Table 2-2 provides a summary of the logic that has been implemented for the above set of rules. PFSTAT, which appears in the table, is a parameter which is used to record current offset status. PFSTAT has three possible states: BASEOFFST, PARALLEL, or NOPOFS. POFSF is an input parameter that is used to identify a flight plan revision. POFSF is assigned one of 4 possible states

by the calling program: BASEOFST, PARALLEL, NOPOFS, or CANCEL. A description of this set of data parameters is given in Section 2.1.2.

The Utility Module provides four routines that are called by the CDU software. The ADD4D and REPLY4D routines are used for all flight plan revisions that occur on the Flight Plan, Speed, and Progress pages. The ADDDIR and REPDIR routines are called for DIRECT TO edits. Program listings for this set of routines are given in Appendix A.



**FIGURE 2-6**  
**Software Interfaces for Base Offsets**



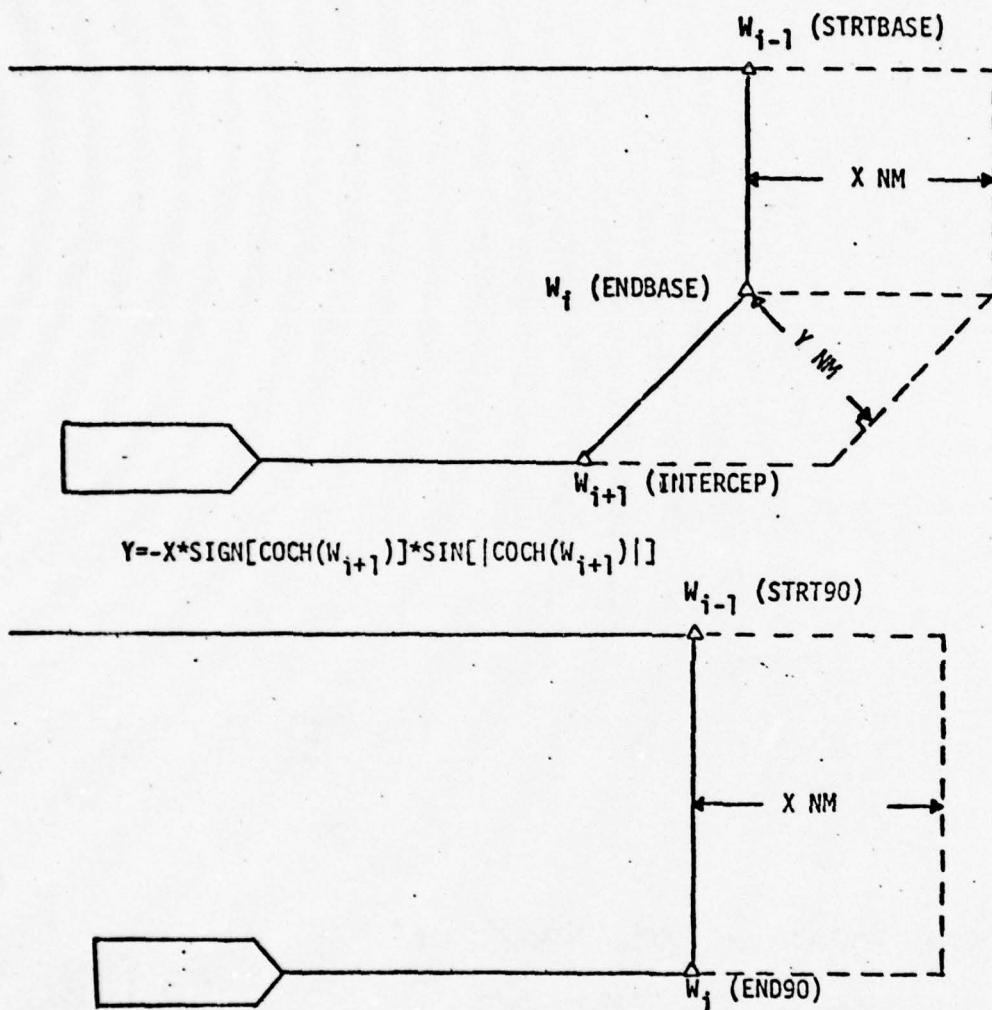


FIGURE 2-7  
Basic Geometries for Base Offsets

Type of DIRECT TO

Requirements for cancelling an  
existing Base Offset

DIRECT TO the TO-  
Waypoint

The TO-Waypoint must be a Base  
Offset waypoint.

DIRECT TO the  
Scratchpad entry

The TO-Waypoint must be a Base  
Offset waypoint.

DIRECT TO a waypoint  
in the flight plan other  
than the TO-Waypoint

The flight plan must contain a  
Base Offset waypoint that is  
entered either at or before the  
"DIRECT TO waypoint."

TABLE 2-1

Operational rules used to cancel Base Offsets  
for DIRECT TO entries

DECISION LOGIC		NP = NOPOFS B = BASEOFFST P = PARALLEL C = CANCEL											
	CONDITIONS	ACTIONS											
		NP	NP	NP	NP	B	B	B	B	B	P	P	F
	PESTAT (CURRENT OFFSET CONFIG.)	NP	B	NP	P	NP	B	B	B	B	P	P	F
	POFSF (DESIRED OFFSET CONFIG.)	NP	B	NP	P	NP	NP	B	B	B	P	P	F
	EDIT TOUCHES BASE OFFSET					N	Y						S
	GEOMETRY CHECKS ARE SATISFIED		N	Y				N	Y				F
	CANCEL OFFSETS								X	X	X	X	
	ENTER NEW OFFSET			X	X				X		X		
	PASS EDIT TO FPE	X			X	X					X		
	MARK BASE OFFSET WAYPOINTS			X					X				
	EDIT DISALLOWED		X				X	X					X
	CDU PREVENTS OCCURRENCE										X	X	

TABLE 2-2  
Summary of Logic used to Implement Operational Rules for Flight Plan Revisions

### 2.3 Speed Profile Algorithm

Software interfaces required for implementation of the Speed Profile Algorithm are shown in Figure 2-8. An IAS entry on the Speed Page is recorded as a flight plan parameter in the Flight Event Table. A description of the IAS parameter was given in Section 2.1.2.

Speed profile computations are implemented within the CDU channel by a routine called SPDPRF. Computations are performed whenever a flight plan revisions occurs.

Special logic is required for the From-Waypoint. This waypoint is always treated as a speed-control waypoint whenever the flight plan contains an IAS entry. This is done to ensure that a speed profile presently being flown will not be changed at waypoint passage.

The task description for SPDPRF is given below. A diagram illustrating the use of program parameters is given in Figure 2-9. A program listing of SPDPRF is given in Appendix B.



## Task Specification for SPDPRF

### Procedure Type

Integer Procedure SPDPRF

### Module

3D/4D Time and Speed Algorithms

### Task Summary

Speed profile computations are performed for all lateral events that are not considered to be speed-control waypoints. (Speed-Control waypoints are waypoints for which speed has been entered via the CDU.) The lateral FROM-event is treated as a speed-control waypoint to ensure that a speed profile presently being flown will not change at waypoint passage. Results of profile computations are recorded in the IASR/IASI/IASF component structure for lateral events.

### Notation

W(J)      Used to denote the Jth lateral event

IASR(J)   Used to denote the value of the IASR component for W(J). Similar notation is used for other components defined by the Flight Plan Editor.

### Internal Data Structures

#### Integer Data

FRST	Absolute Lateral Event Number Index for the initial speed-control waypoint of a given profile.
LAST	Absolute Lateral Event Number Index for the final speed-control waypoint of a given profile.
FRST.STATUS	Used to record the validity of FRST for a given profile.
LAST.STATUS	Used to record the validity of LAST for a given profile.
J	Absolute Event number of the Jth lateral event.

#### Real Data

PROFDST The along-track distance between W(FRST) and W(LAST).  
DVEL The velocity change between W(J-1) and W(LAST).  
DJ The along-track distance between W(J-1) and W(J).  
DELDIST The along-track distance between W(J) and W(LAST).  
T1 The time required to fly from W(J-1) to W(LAST) at a rate of 40 knots/minute.  
AVEV The average velocity required for a linear speed profile between W(J-1) and W(LAST).  
T2 The time required to fly from W(J-1) to W(LAST) assuming a constant velocity of AVEV.  
DPP The distance required to realize a velocity change of DVEL at the rate of greater than or equal to 40 knots/minute.

#### Calling Sequence

SPDPRF()

#### Return Values

Speeds assigned to intermediate profile points are recorded in the Flight Plan Editor's FET structure.

#### Task Description

IF a flight plan revision has occurred since the last speed profile computation  
THEN

BEGIN ... SPDPRF loop.

Starting with the FROM-waypoint, scan the flight plan for a speed entry.

IF no speed entry has been found

THEN

BEGIN No Speed Entry loop.

Update bookkeeping to indicate that another attempt to compute speed profiles is not required for the present flight plan (this is intended to assist CDU keyboard response time).

```

    RETURN to calling program.
END No Speed Entry loop.
Assign the first speed to the FROM-waypoint.
Tag the FROM-waypoint as FRST.
Assign VALID to FRST.STATUS.
WHILE FRST.STATUS EQL VALID DO
BEGIN    ...FRST Valid loop
    Assign INVALID to LAST.STATUS
    Starting with W(FRST+1) scan the flight plan for a speed-control
    waypoint.
    IF the speed-control waypoint is found
    THEN
        BEGIN    ...LAST Valid loop
            Assign VALID to LAST.STATUS.
            Tag the speed-control waypoint as LAST.
            Determine PROFDST, the along-track distance between W(FRST)
            and W(LAST).
            IF LAST NEQ (FRST+1)    ...Note that speed profile computations,
            i.e., the Profile loop, will be hypassed if successive lateral
            events are defined as speed-control waypoints.
        THEN
            BEGIN    ...Profile loop.
                IF the speed for W(FRST) and W(LAST) are equal
                THEN
                    BEGIN    ...Same.Speed loop.
                        FOR J=(FRST+1) STEP 1 UNTIL LAST DO
                            BEGIN    ...Assign Same Speed loop
                                Assign the speed for W(FRST) to W(J).

```

$$IASR(J) = \text{SQRT}[V_0^2 + (V_F^2 - V_0^2) * \frac{D}{DPP}]$$

Where:

D=DJ  
 $V_0 = IASR(J-1)$   
 $V_F = IASR(LAST)$   
 $DPP = DJ + DELDIST$

Assign either PRUP or PRDOWN to the IASF component of W(J) for CDU display purposes.

END ...Linear loop

ELSE ...At this point it has been determined that an average speed rate less than 40 kts/min is required to fly from W(J-1) to W(LAST).

IF an average rate of less than 40 kts/min is also required to fly from W(J) to W(LAST), assign IASR(J-1) to IASR(J).

BEGIN ...40 Kts/Min loop

Determine DPP, the distance required to realize a velocity change of DVEL at the rate of 40 Kts/Min, i.e.,  
 $DPP = T1 * AVEV$

IF the distance, DELDIST, between W(J) and W(LAST) is greater than or equal to DPP

THEN

BEGIN ...No Change loop

Assign IASR(J-1) to IASR(J) and PRQUOTE to IASR(J).

END ...No Change loop

ELSE

BEGIN ...Min Rate Zone loop

Calculate a velocity for W(J) that is based on a 40 kt/min velocity rate between W(J-1) and W(J), i.e.,

$$IASR(J) = \text{SQRT}[V_0^2 + (V_F^2 - V_0^2) * \frac{D}{DPP}]$$



Where

$V_0 = \text{IASR}(J-1)$

$V_F = \text{IASR}(\text{LAST})$

$D = \text{DPP} - \text{DELDIST}$

Assign either PRUP or PRDOWN to IASR(J-1).

END      ...Min Rate Zone loop

END      ...Min Rate Zone loop

END      ...Velocity Change loop

END      ...Profile loop

Define parameters for next cycle of FRST.VALUE loop:

FRST=LAST.

FRST.STATUS=LAST.STATUS.

LAST.STATUS=INVALID

END      ...LAST Valid loop

END      ...FRST Valid loop

Update bookkeeping to indicate that speed profile computations have been performed for the existing flight plan.

END      ...SPDPRF loop

RETURN to calling program.

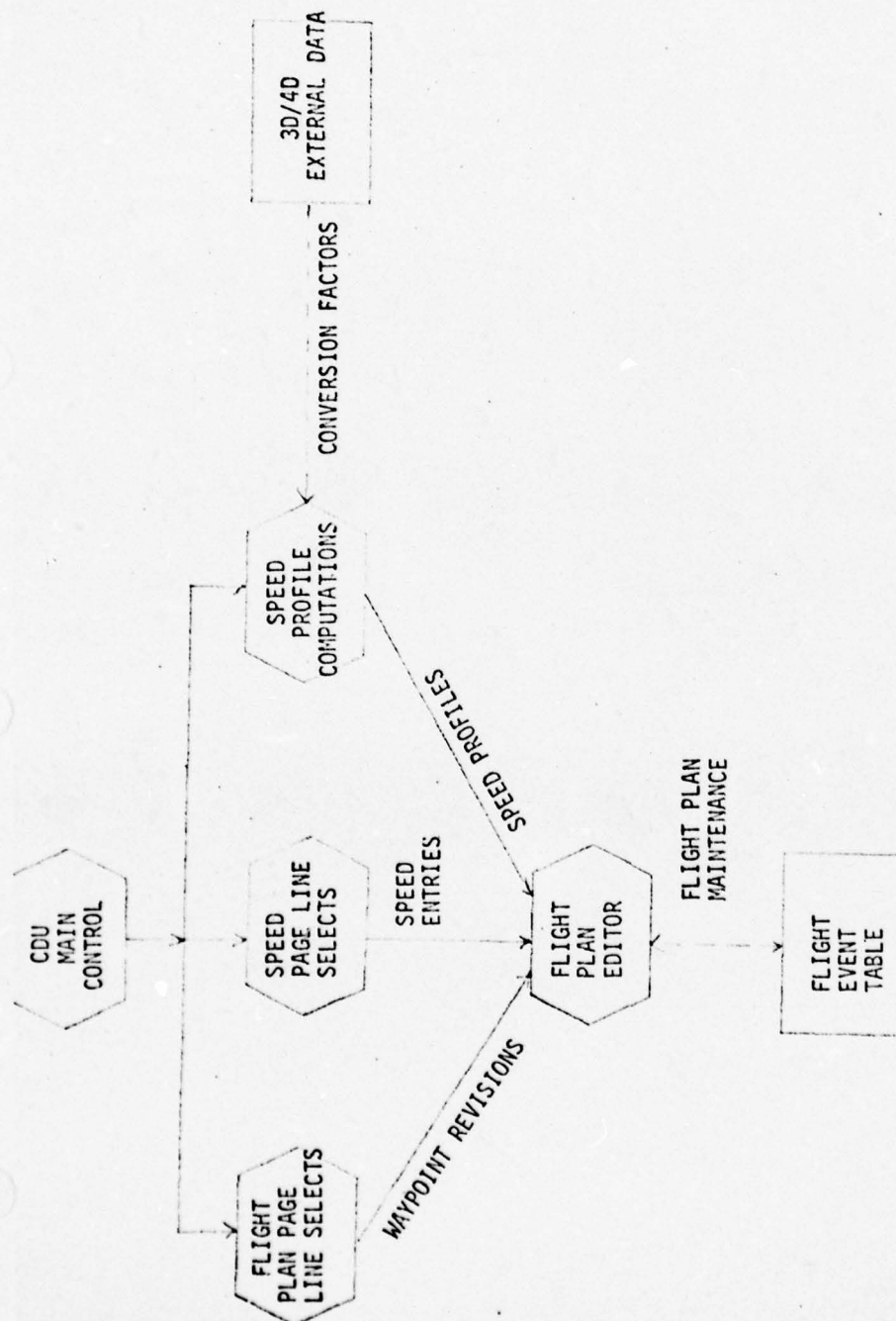


FIGURE 2-8

Software Interfaces for Speed Profiles

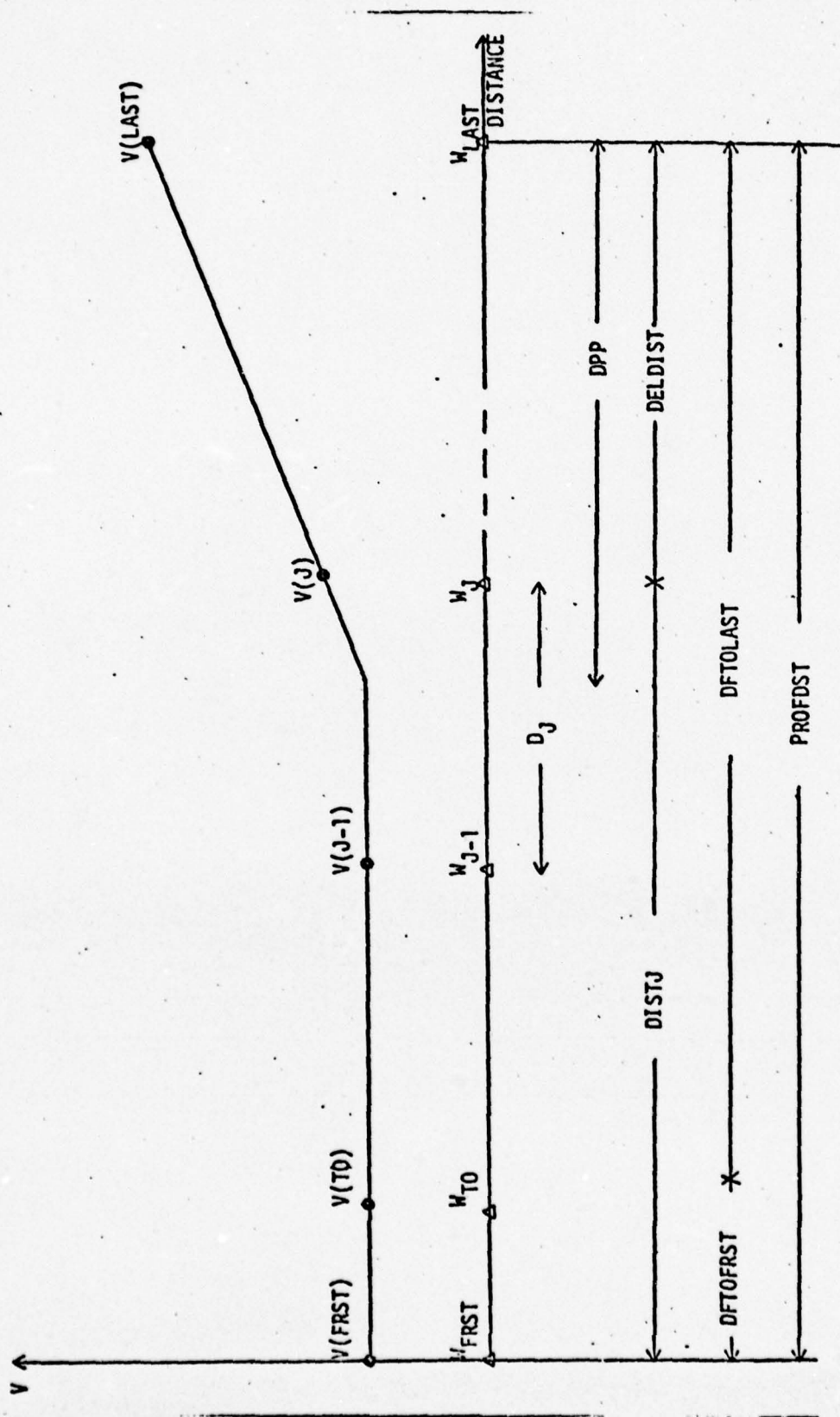


FIGURE 2-9  
Description of Program Parameters used to implement the Speed Profile Algorithm

## 2.4 Time Control Algorithm

Figure 2-8 illustrates the basic software interfaces required for maintenance of the Time Control parameters. Data declarations for the Time Control Parameters were given in Section 2.1.1. With the exception of aircraft sensor data, all parameters are maintained by procedures that are called by the CDU Main Control procedure. The Time Fix and Commanded Arrival Time are CDU entries made on the Flight Progress Page. The same page is used to display the software computations for Commanded IAS and Arrival Time Error (Early/Late Indication). The Flight Plan Monitor monitors waypoint passage of the Time-Fix to determine the necessity of invalidating algorithm computations.

### 2.4.1 CDU Display of Time Control Parameters

The last two line pairs of the Flight Progress Page are used for the display of Time Control parameters. Data declarations for this set of parameters are given in Section 2.1.1. Line pair #5 provides information for the Time-Fix, TFIX, Commanded Arrival Time, TCOM, and Commanded Air Speed, VCOMI. The validity flags TFI XF and TCOM F are monitored to determine the need to display blank data fields for TFIX and TCOM, respectively. The value stored in VCOMI is displayed for the Commanded Air Speed data field whenever VCOMIF has an assigned value of IASVALID.

Line pair #6 is used for the Early/Late and Navigation Downmode displays. The latter function is identical to that defined for the ANS-70A system. Values for the Early/Late display are recorded in TIMERR and EARLY. The EARLY label is displayed whenever EARLY is valid and negative; LATE is displayed for a valid positive value. The value recorded in TIMERR is used for display of the Early/Late data line. No display is required for the Early/Late label and data lines whenever the validity flag TIMERF is assigned an INVALID status.



#### 2.4.2 CDU Line-Select Operations

Line pair #5 for the Flight Progress Page provides the pilot with the capability of designating a waypoint as the Time-Fix and a Commanded Arrival Time for this waypoint. The two data fields used to enter this information may be entered (or revised) separately or simultaneously.

Rules governing line-select entries are as follows:

##### TIME Entries:

- 1) The same range checks used for GMT entries on the Present Position Page apply to the Time Entry.
- 2) The value of the Time Entry is recorded in TCOM and the associated validity flag, TCOMF, is assigned a VALID status.

##### WAYPOINT Entries:

- 1) The waypoint must be stored in the Flight Plan prior to the WAYPOINT entry on the Flight Progress Page.
- 2) A valid entry is recorded in TFIX. TFIXF is assigned a VALID status to indicate that a Time-Fix has been designated.

A single scratch pad entry of a minus (-) sign is used to invalidate both fields. An INVALID status is assigned to both TFIXF and TCOMF whenever this entry is made.

#### 2.4.3 Functional Description of Time Control Algorithm

The description of the Time Control Algorithm uses the following notation:

$i$  Subscript used to represent the  $i^{TH}$  waypoint. The following values of  $i$  will be of special significance:

- $i = 0$  For the FROM-WAYPOINT
- $= 1$  For the TO-WAYPOINT
- $= T$  For the waypoint designated as the time-fix.

$W_i$  The  $i^{TH}$  waypoint.

$CRS_i$  The course into  $W_i$  as given by the flight plan.

$WATK_i$	The along-track component of wind for W is $WATK_i = -(NWDN * \cos(CRS_i) + EWND * \sin(CRS_i))$ , where NWND and EWND represent present lateral filter estimates for north and east wind components, respectively. $WATK_i$ denotes the present along-track component of wind.
$\overline{VNOM}$	The nominal value for present commanded TAS. $\overline{VNOM}$ is a function of $\overline{V}_0, \overline{V}_1$ , the time estimated to fly the along-path distance between $W_0$ and $W_1$ , and the actual distance from the aircraft to the TO waypoint.
VCOM	The present commanded IAS of the aircraft. VCOM represents the commanded IAS displayed on the Flight Progress Page.
$\overline{VCOM}$	The present commanded TAS of the aircraft.
VACT	Air data sensor input for present aircraft TAS.
VACT	Present aircraft IAS as given by the speed and time control algorithm.
$V_i$	The IAS (Indicated Air Speed) associated with $W_i$ .
$\overline{V}_i$	The TAS (True Air Speed) associated with $W_i$ .
$\overline{TTGCOM}_i$	The commanded (actual) time required to reach $W_i$ . In particular, the commanded time required to reach the desired time fix, $\overline{TTGCOM}_T$ , is given by $\overline{TTGCOM}_T = (\text{Time commanded to arrive at the time fix}) - (\text{Present Time})$ .
$\overline{TTGNOM}_i$	The nominal time required to reach $W_i$ . $\overline{TTGNOM}_i$ is a function of IAS entries and flight path geometry.
$D_i$	The leg distance between $W_{i-1}$ and $W_i$ . $D_i$ is defined as the actual distance from the aircraft to the To-Waypoint.
$D_i'$	That portion of $D_i$ that is to be flown at a constant speed.
$D_i''$	That portion of $D_i$ that requires a velocity change.

An important concept of the Task II Speed Control Philosophy is the utilization of minimum 40 knot/minute speed change profiles. Pilot reaction to speed changes is not required until a minimum speed change of 40 knots/minute is needed to reach a desired airspeed. This means that the speed profile for any given leg may be presented as one of the two situations depicted in Figure 10.

Ignoring wind, let K denote the proportionality factor that represents the proportion of nominal speed that is required to arrive at the time fix on schedule (K=1 if no change in the nominal profile is required to meet the desired schedule).

Then  $V_{COM} = K \cdot V_{NOM}$  where K is to be determined from the relation:

$$K = \overline{TTGNOM}_T / \overline{TTGCOM}_T$$

As noted before,  $\overline{TTGCOM}_T$  is merely the difference between the time (GMT) commanded to arrive at  $W_T$  and the present time (Present value of GMT).  $\overline{TTGNOM}_T$  is given by summing the nominal times required to fly all legs until  $W_T$  is reached, i.e.,

$$\overline{TTGNOM}_T = \frac{MTG'}{\overline{V}_0 + WATK_1} + \frac{MTG''}{(\overline{V}_0 + \overline{V}_1)/2 + WATK_1} + \sum_{i=2}^T \left( \frac{D_{i-1}'}{\overline{V}_{i-1} + WATK_{i-1}} + \frac{D_{i-1}''}{(\overline{V}_{i-1} + \overline{V}_i)/2 + WATK_{i-1}} \right).$$

In the above expression,  $MTG = MTG' + MTG''$  is the actual distance from the aircraft to the To-Waypoint.  $MTG'$  and  $MTG''$  are analogous to  $D_1'$  and  $D_1''$ , respectively.

Having found K, the value of the commanded TAS for the present leg is given by  $V_{COM} = K \cdot V_{NOM}$ . The best available

along-track component of wind for the present leg is given by using the Lateral Filter's Estimates for north and east wind components. This dynamic computation for along-track wind cannot be proportionately modified for the remaining portion of the present leg. At best, it may only be used to directly modify the dynamic computations for  $V_{COM}$  and  $V_{NOM}$ . Thus,

$$\overline{V_{COM}} + W = K \cdot (\overline{V_{NOM}} + WATK_1) \text{ or}$$

$$\overline{V_{COM}} = K \cdot \overline{V_{NOM}} + WATK_1 \cdot (K-1), \text{ where } WATK_1 \text{ represents the present component of along-track wind.}$$



$\overline{VCOM}$  represents the present commanded true air speed that is necessary to arrive at  $W_T$  on time. The corresponding commanded IAS is computed by the relationship

$$VCOM = (1-K_1h) * \overline{VCOM}$$

The value used for  $K_1$  is the value relating present IAS to present TAS and is computed as follows. The present aircraft IAS ( $\overline{VACT}$ ) is not directly available to the computer but can be computed from the IAS command ( $VCOM$ ) and IAS airspeed error ( $\Delta V$ ) signals which are available from the max allowable airspeed instrument, i.e.,

$$VACT = VCOM + \Delta V.$$

Present values for aircraft TAS ( $\overline{VACT}$ ) and altitude ( $h$ ) are resident in the RNAV computer memory. Using the relationship

$$VACT = \overline{VACT} (1 - K_1h),$$

the altitude proportionality constant,  $K_1$ , may then be determined by combining the above equations, i.e.,

$$(1-K_1h) = (VCOM + \Delta V)/\overline{VACT}$$

$$\text{and } K_1 = (\overline{VACT} - VCOM - \Delta V)/(h * \overline{VACT})$$

With  $h$  in feet,  $K_1$  should vary from 0.00001 to 0.000015. Because of sensitivity problems as  $h$  becomes small,  $K_1$  is to be limited to the above values in the IAS to TAS speed conversions. In the TAS to IAS conversion regarding the commanded velocity the  $(1-K_1h)$  ratio can be used directly, avoiding any sensitivity problem.

The Commanded Speed displayed on the Flight Progress Page is then given by:

$$VCOM = (1-K_1h) * \overline{VCOM}$$

The final portion of the algorithm deals with the early/late computation. This computation is based upon the expected time error at the time-fix that would result by flying the present leg at the actual rather than commanded TAS.



As before, let:

$\overline{VCOM}$  Represent the present value for commanded TAS.

$\overline{TTGCOM}_T$  Represent the commanded time required to reach  $W_T$ .

$\overline{VACT}$  Represent the present air data sensor input for TAS.

Also, let:

$D_T$  Represent the modified along-track distance from the aircraft to  $W_T$ . The modification consists of using actual distance from the aircraft to the To-waypoint for the present leg.

$\overline{TTGACT}_T$  Represent the time required to traverse  $D_T$  assuming a TAS of  $\overline{VACT}$ .

Since the Distance,  $D_T$ , must be flown to arrive at  $W_T$  using either velocity, it follows that:

$$\begin{aligned} D_T &= (\overline{VACT} + WATK_1) * \overline{TTGACT}_T \\ &= (\overline{VCOM} + WATK_1) * \overline{TTGCOM}_T \end{aligned}$$

The expected time error,  $\overline{TTGACT}_T - \overline{TTGCOM}_T$  is then given by:

$$(\overline{TTGACT}_T - \overline{TTGCOM}_T) = \overline{TTGCOM}_T * \left[ \frac{(\overline{VCOM} + WATK_1)}{(\overline{VACT} + WATK_1)} - 1 \right]$$

where a positive error is to be displayed as a LATE indication.

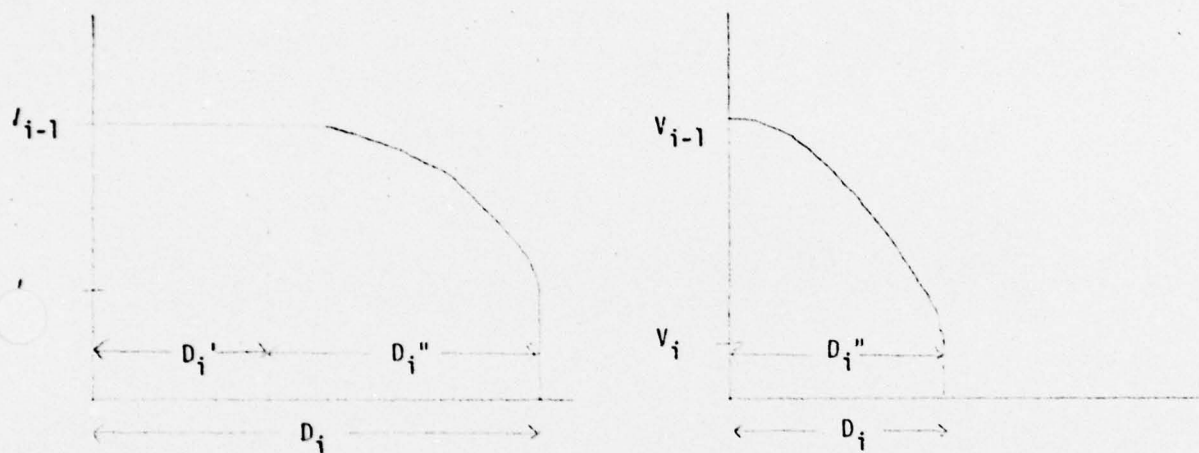


FIGURE 2-10

Speed Profiles

$D_i''=0$  whenever  $V_{i-1}=V_i$  and  $D_i'=0$  whenever a speed change in excess of 40 KTS/Min is required for the entire leg distance  $D_i$ .

#### 2.4.4 Software Implementation of the Algorithm

Algorithm computations are performed by procedure TIMCNTRL. Although control is given to this procedure every cycle by the CDU Main Control Program, computations are only attempted whenever either 1) ten seconds have elapsed since the last algorithm computation, or 2) a Flight Plan revision has occurred since the last execution of the algorithm.

Since TIMCNTRL is a procedure called within the CDU channel, it is possible for sensor data maintained by the Navigation channel to change during any given execution of the algorithm. To ensure that the same set of parameters is used for a given algorithm computation, it is necessary to take a snapshot of the sensor data as part of the initialization logic for the algorithm.

A task description for TIMCNTRL is given below. A program listing of TIMCNTRL is given in Appendix C.

#### Task Specification For TIMCNTRL

##### Procedure Type

Procedure TIMCNTRL( )

##### Module

40 Time and Speed Algorithms

##### Task Summary

The Time and Speed Control Algorithm is based upon speed and time errors with respect to a waypoint (the Time-Fix) for which an arrival time has been assigned. The value calculated for VCOMI, the Commanded Velocity displayed on the Flight Progress Page, represents the present indicated air speed that should be flown to arrive at the Time-Fix on schedule. The computation for TIMERR provides the best estimate of the total time error that is expected for the desired arrival time. Computations for VCOMI are provided whenever the Present Flight Plan, exclusive of the From-event, contains at least one speed waypoint. The computation for TIMERR is made whenever the validity flag WFIXF indicates that a Time-Fix has been defined for the system.

## Notation

- W(J)** Used to denote the Jth Lateral Event.
- IASR(J)** Used to denote the value of the IASR component for W(J). Similar notation is used for other components defined by the Flight Plan Editor.

## Internal Data Structure

### Synonyms

- INITEVNO** Initial Absolute Event Number required for retrieval of event data from the Flight Plan Editor.

### Integer Data

- J** Event Number for the Jth Event.
- CNTRL** Control parameter for the main loop.
- VTIMF** Flag used to control computations for the case where a Time-Fix has not been entered but VCOMI is to be calculated for the To-waypoint.

### Real Data

- PREVIASR** Temporary storage used to record IASR(J-1).
- PREVDFTO** Temporary storage used to record DFTO(J-1).
- TTGACT** Present estimate of actual time required to reach the Time-Fix.
- TTGCOM** Commanded time to reach the Time-Fix.
- COCHPREV** Temporary storage used to record CRSO(J-1)-CRSI(J-1).
- HZ** Altitude used for IAS to TAS conversion.
- LEGDST** Along-track distance from W(J-1) to W(J).
- WATK** The along-track component of wind applied to W(J).
- WATKTO** The along-track component of wind applied to the leg presently being flown.
- KALT** The altitude proportionality constant used for conversions between IAS and TAS.
- TASPREV** Temporary storage used to record computed TAS for W(J-1).
- TASJ** Temporary storage used to record computed TAS for W(J).
- DV** The speed change between W(J-1) and W(J).
- T1** The time required to fly from W(J-1) to W(J) at a rate of 40 kts/min.



AVEV	The average ground velocity required for a linear speed profile between W(J-1) and W(LAST).
T2	The time required to fly from W(J-1) to W(J) assuming a constant velocity of AVEV.
DPP	The portion of the leg between W(J-1) and W(J) that requires a speed change.
DELT	The expected time required to fly from W(J-1) to W(J).
DP	The portion of the leg between W(J-1) and W(J) that should be flown at the velocity assigned to W(J-1).
GMTCONV	Conversion factor used to convert GMT to navigation time units.
VGNOM	Nominal ground velocity calculated for the present leg.
KSCALE	Scaling factor used to protect against overflow.

#### Calling Sequence

TIMCNTRL( )

#### Return Values

VCOMI	Commanded IAS for the present leg that is to be displayed on the Flight Progress Page and IAS instrument.
VCOMIF	Validity flag for VCOMI.
TIMERR	Expected time error for arrival at the Time-Fix.
TIMERF	Validity flag for TIMERR.

#### Task Description

IF 10 seconds have not elapsed since the last execution of the Time Control Algorithm  
 AND a Flight Plan revision has not occurred since the last cycle  
 THEN RETURN to calling program.

Update own clock reading.

Update own version of Flight Plan Revision number

Assign INVALID status to TIMERF, the validity flag for arrival time error.

Comment: assign an initial validity status to VCOMIF, the validity flag for commanded IAS.

IF VCOMIF=

```

IF invalid GMT THEN IVGMT
ELSE IF invalid aircraft true air speed THEN IVTAS
ELSE IF invalid aircraft altitude THEN IVALT
ELSE NODATA) NEQ NODATA

```

THEN RETURN to calling program.

IF the Lateral From-event is invalid

OR no speed is defined for this event

THEN RETURN to the calling program. Note that VCOMIF will have a value of  
NODATA and TIMERF will have an INVALID STATUS.

Comment: Keep a snapshot of sensor data, i.e.,

ACTAS = Aircraft True Air Speed

ACALT = Aircraft Altitude

ACIASERR = IAS Instrument Error

ACNWND = North Component of Wind

ACEWND = East Component of Wind

Assign IASR component of the Lateral From-Event to PREVIASR.

Assign DFTO(FROM) to PREVDFTO.

Initialize event number index by assigning INITEVNO to J.

Initialize nominal time-to-go, TTGNOM, to 0.0.

Initialize COCHPREV to value of CRSO(FROM)-CRSO(FROM).

Assign an initial status of VALID to VTIMF to ensure computations are performed  
for TO-waypoint.

WHILE the Jth event is not the Time-Fix.

AND the (J=J+1)th event is valid.  
AND VTIMF EQL VALID.

GIN ... Calculate TTG block.

IF event J is a Vertical event

THEN

BEGIN ...Vertical Event block

IF event J is the Vertical TO-event

THEN assign value of ACALT to HZ.

ELSE assign ALTD(J) to HZ.

END ...Vertical Event block

ELSE

IF event J is a Lateral event . ...Note that End-Of-Continuity events  
are bypassed.

THEN

BEGIN ...Lateral Event block

Calculate LEGDST, the distance from W(J-1) to W(J), i.e.,

$LEGDST = DFTO(J) - PREVDFTO.$

Update PREVDFTO to value of DFTO(J).

Calculate WATK, the along-track component of wind, i.e.,

$WATK = -(ACNWND * \cos(CRSI(J)) +$   
 $ACEWND * \sin(CRSI(J))).$

Calculate KALT, the altitude proportionality constant, i.e.,

$KALT = \frac{[ACTAS - VCOMI - ACIASERR]}{[HZ * ACTAS]}$

Limit KALT to the interval (.00001, .000015)

Convert IAS for W(J-1) to TAS, i.e.,

$TASPREV = \frac{PREVIASR}{(1.0 - HZ * KALT)}.$

Convert IAS for W(J) to TAS, i.e.,

$TASJ = \frac{IASR(J)}{(1.0 - HZ * KALT)}.$

Calculate DV, the speed gradient between W(J-1) and W(J), i.e.,

$DV = TASJ - TASPREV.$

Calculate T1, the time required to fly from W(J-1) to W(J) at a rate of 40 kts/min.

$T1 = |DV * MINRATE|.$

Calculate AVEV, the average ground velocity required for a linear speed profile between W(J-1) and W(J), i.e.,

$AVEV = 0.5(TASPREV + TASJ) + WATK$

Calculate T2, the time required to fly from W(J-1) to W(J) assuming a constant velocity of AVEV, i.e.,

$T2 = |LEGDST / AVEV|$

IF the velocity change, DV, between W(J-1) and W(J) requires a velocity rate greater than or equal to 40 kts/min (i.e., if  $T2 \leq T1$ )

THEN

BEGIN ...Linear Profile Block

Assign T2 to DELT, the time required to fly the leg from W(J-1) to W(J).

Assign LEGDST to DPP, the portion of the leg into W(J) that requires a speed change.

END      ...Linear Profile Block

ELSE      ...Part of the leg into W(J) should be flown at the velocity for W(J-1), the remaining portion at a velocity rate of 40 kts/min. Calculate time and distance parameters for the portion requiring a speed change.

BEGIN      ...40 kts/min Block

Assign T1 to DELT.

Assign T1\*AVEV to DPP.

END      ...40 kts/min Block

IF W(J) is the Lateral To-Event

THEN

BEGIN      ...To-Event Block

Assign IASVALID to VCOMIF to indicate VCOMI computation has been performed.

Assign value of TFIKF to VTIMF.

Save the along-track wind component for the Lateral To-Event, WATK, in WATKTO.

Save value of KALT in KALTTO.

IF the velocity change, DV, between W(J-1) and W(J) requires a velocity rate that exceeds 40 kts/min (i.e., if  $T2 < T1$ )

OR the distance from the aircraft to the Lateral To-Event is within that portion of the leg that requires a velocity change (i.e., if  $MTG \leq DPP$ )

THEN

BEGIN      ...To-Event Velocity Change Block

Calculate VGNOM, the present nominal aircraft velocity (GS-referenced at this point) that must be flown to arrive at the Time-Fix on schedule, i.e.,

$$V_0 = TASP_{REV} + WATK$$

$$V_F = TAS_J + WATK$$

$$VGNOM = \sqrt{V_0^2 + (V_F^2 - V_0^2) \frac{MTG}{DPP}}$$



Calculate DELT, the time required to fly from aircraft present position to W(J) if the aircraft is on schedule, i.e.,

IF DMTG > DPP  
 THEN DELT = T2 + (DMTG > DPP)/VGNOM  
 ELSE

$$\text{DELT} = \frac{2 * \text{MTG}}{(\text{VGNOM} + \text{TASJ} + \text{WATK})}$$

END ...To-Event Velocity Change Block

ELSE ...Velocity change is not required for present portion of leg into the Lateral To-Event.

BEGIN ...To-Event constant velocity block.

Assign velocity for W(J-1) to VGNOM, i.e.,

$$\text{VGNOM} = \text{TASPREV} + \text{WATK}$$

BEGIN ...Excessive Course Change block.

Tag commanded IAS display as invalid by assigning IVCOCH to VCOMIF.

RETURN to calling program. Note that TIMERF is returned with an INVALID status and VCOMIF indicates that "CRS" will appear for the commanded IAS display on the Progress Page:

END ...Excessive Course Change block.

ELSE

BEGIN ...Leg Capture Compensation block.

Compensate for aircraft turn made for leg capture at W(J-1), i.e.,

$$\text{DELT} = \frac{\text{TASPREV} * [|\text{COCHPREV}| - 2 * \text{TAN}(\frac{|\text{COCHPREV}|}{2})]}{g * \text{TAN}(25^\circ)}$$

where g=Acceleration due to gravity.

Increment TTGNOM by DELT.

END ...Leg Capture Compensation block.

END ...Beyond To-Event block.

Update COCHPREV to value of

$$\text{COCHPREV} = \text{CRSO}(J) - \text{CRSI}(J)$$

D ...Lateral Event block.

.D ...Calcttg Block

Calculate      1) K, the proportion of nominal speed that is required to arrive at  
                 the Time-Fix on schedule, and  
                 2) TTGCOM, the commanded Time-To-Go for arrival at the Time-Fix, i.e.,

IF TIMERR = (TCOMF .V. TFIXF) NEQ VALID

...Computations for TIMERR, K, and TTGCOM are dependent upon status of pilot  
entries for Time-Fix and Commanded Arrival Time

THEN

BEGIN    ...TTGCOM Invalid Block

    K = KSCALE    ...Reversionary Mode. Set K = (1) \* (Scale Factor).

    KVAL = VALID    ...Indicate K valid for later computation of VCOMI.

END    ...TTGCOM Invalid Block

ELSE

BEGIN    ...TTGCOM Valid Block

    Update Commanded Arrival Time, I.E.,

$TTGCOM = (TCOM - GMTS) / GMTCONV$

    Determine validity of computation for K. K is invalid when TTGCOM approaches  
    zero, I.E.,

    IF  $TTGNOM * KSCALE > |TTGCOM|$

    THEN Assign an INVALID to KVAL

    ELSE

        BEGIN

$K = (TTGNOM * KSCALE) / TTGCOM$

            KVAL = VALID

        END

END    ...TTGCOM Valid Block.

IF VCOMIF EQL IASVALID    ...Computations for VCOMI and TIMERR only valid if To-Event  
                                 has a defined IAS.

THEN

BEGIN    ...VCOMIF Valid Block

    IF KVAL EQL VALID    ...Test for validity of K before updating VCOMI.

    THEN

        BEGIN    ...Update VCOMI Block

Calculate Commanded TAS, I.E.,

$$VCOMT = (K * VGNO!) / KSCALE - WATKTO.$$

Convert VCOMT to IAS for display purposes, I.E.,

$$VCOMI = \frac{1.0 - KALTTO * ACALT}{KALTSCALE} * VCOMT$$

Limit VCOMI to upper limit of IAS Instrument.

END ...Update VCOMI Block

Calculate the expected time error for arrival at the Time-Fix, I.E.,

IF TIMERF EQL VALID

THEN

BEGIN ...Update TIMERR

$$EARLY = (TTGNOM * VGNO!) / (ACTAS + WATKTO) - TTGCOM.$$

$$TIMERR = |EARLY|.$$

END ...Update TIMERR

END ...VCOMIF Valid Block

RETURN to Calling Program

## 2.5 ASC Software Modifications

This section describes the 3D/4D modifications to the ANS-70A version of the Aircraft Systems Coupler (ASC) software. One version of this software has been constructed for use by all three of the Task II systems. In addition to changes implemented for the Base and 2D Plus Time Control Systems, this section will describe ASC software modifications that have been added for the 3D/4D Localizer/Glideslope System.

Table 2-3 lists the sensor data inputs that require additional processing by the ASC Input software. The first three items are required for the Localizer/Glideslope System. Each input has an associated high-level flag which is used to indicate current hardware status for the given sensor input. This status serves as one of the criteria used to determine validity of the sensor input.

Due to radio receiver limitations, localizer frequency is input in the same sensor slot normally used for the secondary VOR frequency. In addition to processing localizer frequency, this requires the ASC software to suppress system usage of the secondary navaid during the localizer mode of navigation. Use of this navaid is inhibited by setting a flag that is normally used to indicate a frequency mismatch.

A software switch whose value is specified for the Link Edit Computer run is used to determine which of two sets of computations are required for processing of IAS Airspeed Error. Computations for the G-I instrument are linear for the range of speeds that have been defined for the instrument. A Least-Squares approximation on the data furnished for the C-880 instrument has resulted in the use of a fourth-degree polynomial to determine IAS error.



The sensor word reserved for the HSI Input for Selected Course is processed every cycle by the ASC Input Program. The 2D Plus Time Control System version of the Flight Plan Monitor is the only program for the three systems that monitors this processed data. The net result is that the ASC software is allowed to process the input for all three Task II systems.

Current status of the "Engaged" discretes is recorded for system usage. The Lateral Navigation program suppresses waypoint passage whenever the Area Navigation System is disengaged from the auto-pilot. The other two discretes are used by the Localizer/Glideslope System.

Table 2-4 provides a summary of sensor data outputs that require additional processing by the ASC Output Program. IAS Command is the only output that is required for all three systems. As with the input for IAS error, conversions for the C-880 instrument are straight-forward. A fourth-degree polynomial is used to convert IAS in knots to degrees for the C-880 instrument.

Remaining outputs are required for the Localizer/Glideslope system. Deviation displays are sent to the HSI and ADI instruments. The ASC Output Program monitors internal flags to determine which navigation modes are controlling the instrument displays.

The Localizer Enable discrete is used to activate tuning the VOR/LOC receiver to localizer frequencies. Once again, internal flags are used to determine the setting of this discrete.

The "Arm" and "Capture/Track" discretes are used to control displays on the Mode Annunciator that has been implemented for Localizer/Glideslope usage. Internal flags are monitored each cycle to determine the settings of these discretes.

One additional feature has been added to the ASC Software that is unique to the 3D/4D systems. The Air Data Computer input for True Air Speed is flagged as invalid whenever TAS falls below 150 knots. 3D/4D usage in terminal area operations will require Time Control and Localizer/Glideslope modes at slow speeds. For this reason, a scheme has been implemented that uses IAS to approximate TAS whenever the latter speed reaches its limit of 150 knots.

INPUT SENSOR DATA

Localizer Frequency + High-Level Flag  
Localizer Deviation + High-Level Flag  
Glideslope Deviation + High-Level Flag  
IAS Airspeed Error + High-Level Flag  
HSI Input for Selected Course  
Auto-Pilot Engaged Discrete  
RNAV-Engaged Discrete  
VNAV-Engaged Discrete

TABLE 2-3

Sensor Data Inputs that have been added for the 3D/4D systems

OUTPUT SENSOR DATA

Commanded Localizer Frequency + Localizer Enable discrete

Localizer Deviation

Glideslope Deviation

Localizer Track Angle Error

IAS Command

Localizer Arm Discrete

Localizer Capture/Track Discrete

Glideslope Arm Discrete

Glideslope Capture/Track Discrete

Flight Director Computer Flag

TABLE 2-4

Sensor Data Outputs that have been added for the 3D/4D systems



## 2.6 Navigation Software Modifications

All of the ANS-70A Navigation software programs were modified for 3D/4D usage. Functional modifications were only implemented for the Lateral Navigation program. Remaining changes were the result of the core reduction effort discussed in Section 2.0. Tasks implemented for the Lateral Navigation software consisted of modifying the ANS-70A criterions for waypoint passage and the Distance-To-Go computation.

The 3D/4D geometry for waypoint passage is illustrated in Figure 2-11. Geometry is shown for the case where the flight plan includes an offset, POFS. Passage of the T0-waypoint occurs whenever both of the following conditions are true:

- 1) The Lateral-Distance-Along-Track (LDAT) to the offset waypoint defined for the T0-waypoint is less than the calculated Leg-Switch-Distance (SWD).

When flying legs without offsets, the offset waypoint is defined to be coincidental with the parent waypoint of the T0-event.

- 2) The bisector defined at this same leg intersection has been crossed.

Referring to figure 2-11, the bisector is given by

$$\text{BISECTOR} = \text{CRS0} - 1/2 (\text{CRS0} - \text{CRS1}) + \pi / 2 \text{ SIGN } (\text{CRS0} - \text{CRS1})$$

The bisector is passed once the expressions  $(\text{BFLEG} - \text{BISECTOR})$  and  $(\text{CRS1} + \pi - \text{BISECTOR})$  have opposite signs.

Geometry for the Distance-To-Go computation is shown in Figure 2-11. The ANS-70A system always uses the parent waypoint for the Lateral To-Event as a reference point for this computation. This is considered to be undesirable

for Time Control procedures when flying offset legs. The 3D/4D system uses the offset waypoint as a reference point for the Distance-To-Go computation.

The ANS-70A system records the coordinates of the parent waypoint in the Flight Plan Table. This was left unchanged for the 3D/4D systems. Coordinates of the offset waypoint are calculated by the Flight Plan Monitor whenever revisions are made to the flight plan.

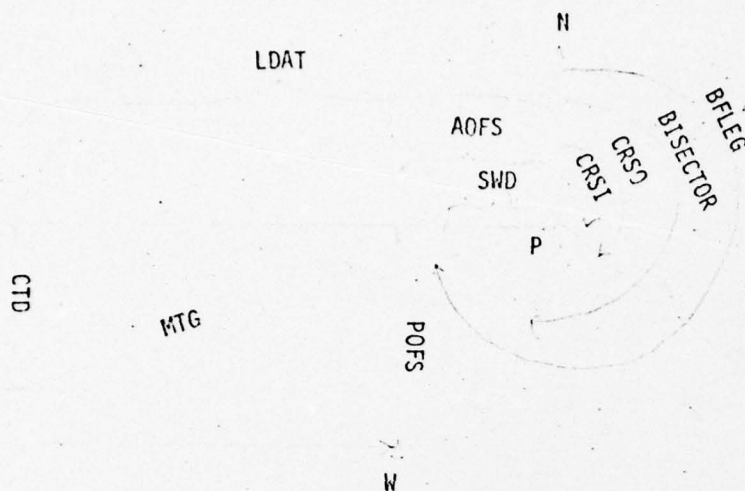


FIGURE 2-11  
Geometry for Waypoint Passage

<u>PARAMETER</u>	<u>DESCRIPTION</u>
W	Parent Waypoint of Lateral To-Event
P	Offset Waypoint of Lateral To-Event
SWD	Switching Distance
LDATA	Lateral-Distance-Along-Track to the Offset Waypoint
CTD	Cross-Track Distance
MTG	Miles-To-Go from Aircraft to the Offset Waypoint
POFS	Offset (Base or Parallel) that has been defined for W
AOF	Along-Path-Offset that must be flown beyond W to reach P
CRSI	Course Into P as determined by Flight Plan
CRSO	Course Out of P as determined by Flight Plan
BISECTOR	Bisector constructed at P
BFLEG	Course (True) from P to the Aircraft

### Section 3 2D PLUS TIME CONTROL SYSTEM

The 2D Plus Time Control System provides the Task II capability of simulating Time Control for non automatic RNAV systems. Major software tasks for this system include the following items:

- 1) Implementation of CDU software for the revised Progress page. Software implementation for this task is described in Section 3.2.

In addition to the Progress page, CDU software allows pilot access to the Flight Plan and Present Position pages. The Flight Plan page is required for data assemblies. The Present Position page is to be used for pilot updates of aircraft present position.

- 2) Maintenance of RNAV waypoint parameters in an array structure that is maintained by the CDU software. The Flight Plan Editor is not used for maintenance of the Flight Plan Table. The pilot has the capability of specifying waypoint parameters for ten waypoints at any given time. Ten 3-word arrays are maintained to record entries for waypoint identifier, bearing, and distance. Two additional arrays are maintained as CDU work areas. A description of the array components used to identify the waypoint parameters is given in Section 3.1.

- 3) Use of HSI analog input for Desired Course. A description of the software implementation for this task is given in Section 3.3.

- 4) Implementation of a Time Control Algorithm that is unique to the 2D Plus Time Control System. All Time Control computations reference the leg presently being flown. A software description of this algorithm is given in Section 3.4.



An additional task consists of suppressing the ANS-70A computations for leg switching and waypoint passage. This has been achieved by constructing a version of the Lateral Navigation program that is unique to this System. This program was constructed by modifying the Base System version of Lateral Navigation. The only other change to this module consisted of implementing a 20-second Waypoint Alert criterion to replace the 15-second criterion used for the other systems.

## 1 External Data Structure

Data parameters unique to the 2D Plus Time Control System have been assigned to a separate module. Data definition for this set of parameters are given below. With the exception of FP.EDIT and NLTOCHG, all parameters are completely maintained by the CDU software.

<u>DATA TYPE</u>	<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
Integer	Display.Wypt	Waypoint Number currently being displayed.
Integer	Use.Wypt	Waypoint Number for waypoint currently being used for navigation.
Integer	FP.Edit	Validity flag that is assigned a VALID status by the CDU software whenever a CDU edit has been made that affects the current navigation leg. FP.EDIT is assigned an INVALID status by the Flight Plan Monitor after the Navigation Event Table (NLTO array) is updated to reflect the edit.
Integer	NLTOCHG	Validity flag that is assigned a VALID status by the Flight Plan Monitor whenever an input (via either the CDU or the HSI Course knob) has been processed that affects the current navigation leg. NLTOCHG is assigned an invalid status by the Speed and Time Control Procedure after the Time and Speed Control computations are updated.

<u>DATA TYPE</u>	<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
Integer	OFFSTF	Validity flag for OFFSET. OFFSTF = valid whenever a lateral offset is commanded, invalid otherwise.
Real	OFFSET	Lateral Offset currently being flown.
Real Array	ARR0, ARR1 ARR9, ARRA, ARRC	Waypoint arrays used to record Ident, Bearing, and Distance information for the IRNAV waypoints.
Pointer Array	PTR.ARRAY	Array of 12 pointers used to reference the waypoint arrays.
Integer Component	WYPT.IDENT	Component used to record ASCII identifier Waypoint Number. Assigned a component position of 0.
Real Component	WYPT.BRG	Component used to record True Bearing from navaid to waypoint. Assigned a component position of 1.
Real Component	WYPT.DIST	Component used to record distance from navaid to waypoint. Assigned a component position of 2.



### 3.2 Functional Description of Revised Progress Page

Display formats for the Progress page are illustrated in Figures 3-1 and 3-2. A functional description of data fields for the Progress page is given below.

#### I) [STATION]

This field provides the pilot with a means of specifying the navaid that is to be used for navigation and tuning purposes. Allowable entries consist of three-character station identifiers that are stored in the data base. The scratchpad message "NOT STORED" is annunciated for attempts to enter invalid identifiers.

#### II) [MODE]

This field provides a CDU display of the current navigation mode. Current usage of VOR, DME, and Air Data/Heading information for navigation purposes is indicated by displaying V, D, and A respectively. The absence of a given mode is indicated by displaying a dash (-) for the corresponding letter. A downgrade of mode will result in the annunciation of the data field. The annunciation may be cancelled via a line-select entry of a single minus sign (-).

#### III) [OFST]

Parallel offsets are commanded by means of the OFST field. The initial character of an offset entry must be either an "L" or "R." The magnitude portion of the entry is allowed to have a range of 0.0 to 50.0 (NM). Thus, an entry of L5.1 would be used to indicate a left offset of 5.1 NM. An existing offset is cancelled via a L0 (L followed by a zero) or R0 entry.

#### IV) [WIND]

The data field for Wind serves as a display field only. Bearing information is displayed as magnetic bearing from the station. Dashes are displayed whenever Air Data or Heading Information is invalid.

#### V) [WPT/BRG/DIST]

The third pair of CDU lines has been reserved for waypoint information. Waypoint parameters consist of Identifier, Bearing (Magnetic) from navaid, and distance from navaid. Allowable entries consist of editing all three fields with one entry or revising any field with a single edit.



A total of 10 waypoints may be designated at any given time. Digits 0 through 9 are used to designate waypoint identifiers. Display of a waypoint other than the USE-waypoint is indicated by blinking the identifier field. A waypoint may be deleted via an entry of a single minus sign for Line-Pair No. 3. Waypoint deletion will result in a display of dashes for the BRG and DIST data fields. Navigation computations reference the navaid presently being used whenever the USE-waypoint is deleted. Deletion of a waypoint will result in the software assignment of 0.0 to the Bearing and Distance fields associated with the given waypoint.

A description of allowable edits for the WPT/BRG/DIST fields is given below:

Entry for Waypoint Identifier:

Acceptable entries consist of a single scratch pad digit (0 through 9)

Entry for Bearing:

Entries must be preceded by a single slash (/).

Range: 0.0 to 360.0 degrees

Increment: 0.1 degrees

Examples: /5.1  
          /05.1  
          /005.1

Entry for Distance:

Entries must be preceded by two slashes (//).

Range: 0.0 to 200.0 NM

Increment: 0.1 NM

Examples: //2.9  
          //02.9  
          // 002.9

VI) TTW

The Time-to-Waypoint field serves as a display field only. The value displayed represents the current estimate of time required to reach the waypoint specified by the Use-waypoint, HSI input for desired course, and current parallel offset.

Range: .0 to 99.9 minutes (values exceeding 99.9 minutes will be displayed as 99.9 minutes).

Resolution: 0.1 minutes

VII) DIST

This field is used to display Distance to the present To-waypoint.

Edits are not allowed.

Range: .0 to 999.9 NM

Resolution: 0.1 NM

VIII) GS

This field is used to display the Present estimate for Ground Speed.

Range: 0 to 999 knots

Resolution: 1 knot

IX) [DTA]

Desired Time of Arrival (GMT units) is to be entered for this field. DTA may be revised or deleted at any time. DTA deletion is accomplished by an entry of a single minus sign. Software is required to invalidate an existing DTA entry upon selection of a new USE waypoint, or revision to any of the WYPT, BRG, or DIST fields of the USE-Waypoint.

Range: .0 to 2359.9 where modulo arithmetic of 60.0 minutes is applied to the last three digits.

Resolution: 0.1 minute

X) GMT

A GMT entry must be preceded by a slash mark (/). Rules for range, resolution, and display format are the same as those for the DTA field.

XI) IAS CMD

This field is used to display Commanded IAS as calculated by the Time and Speed Control Algorithm. Line-Select entries are not allowed.

Line Pair 6 is used for the Early/Late Display. Display formats for the label and data fields are identical to those used for the Base System.



BRT

[STATION]										MODE									
---										---									
[OFST]										WIND									
---										°/---									
[WPT / PRG / DIST]																			
---										---									
[TW]										[DIST]									
---										---									
[DATA]										[GMT]									
---										---									
										IAS									
										CMD									

FIGURE 3-1. Display of Revised Progress Page Prior to Data Entries

1	2	3	A	B	C	D	
4	5	6	F	G	H	I	J
7	8	9	K	L	M	N	O
IND	Ø	CR	P	Q	R	S	T
			U	V	W	X	Y
			.	-	+	/	Z



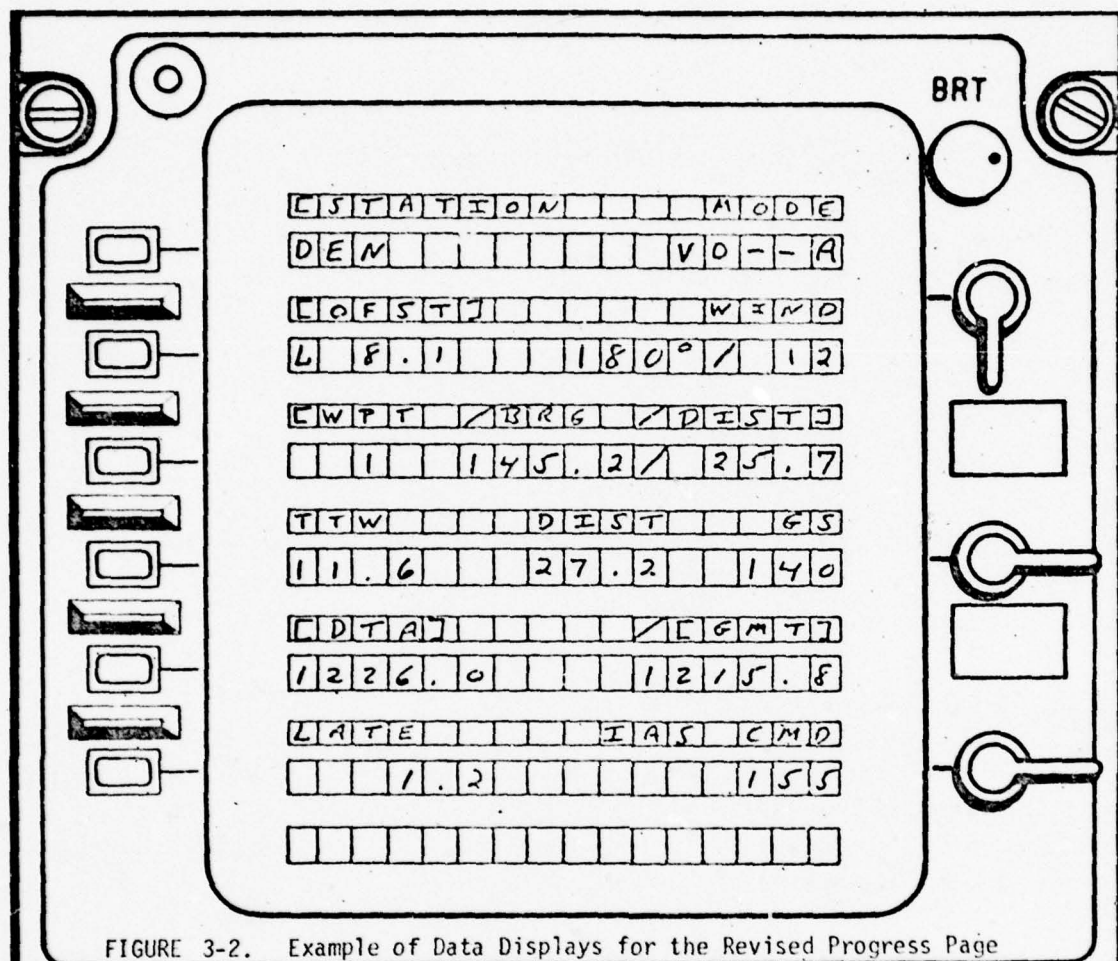
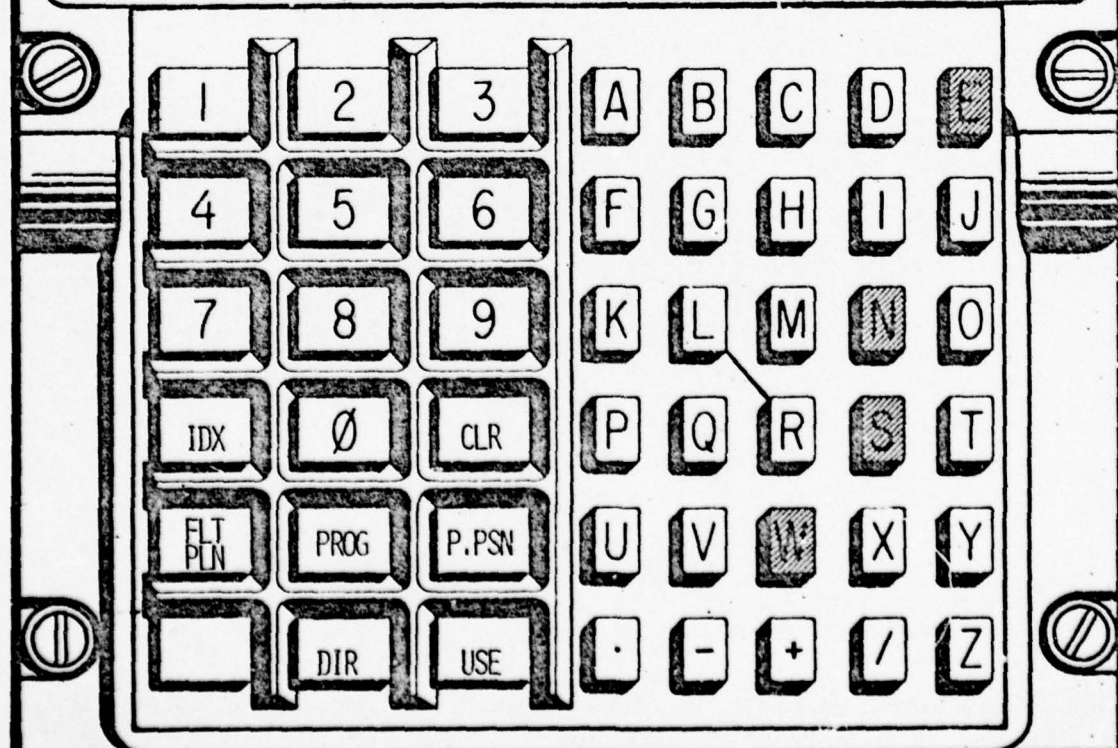


FIGURE 3-2. Example of Data Displays for the Revised Progress Page



### 3.3 HSI Input for Selected Course

Figure 3-3 illustrates software interfaces for programs that require access to the HSI Input for Selected Course. The final objective is to pass the Selected Course input to the Lateral Navigation program as a course command for the present leg.

Initial processing of the input is performed by the ASC Input Program. Converted data is recorded in the ADHD data structure. The Flight Plan Monitor uses the Course input to determine the coordinates of the T0-waypoint. The Selected Course Input is then passed to the Navigation Channel as the flight plan parameter for Course-Into-the-Waypoint (CRSI Component).

Geometry for computation of the T0-Waypoint is given in Figure 3-4.

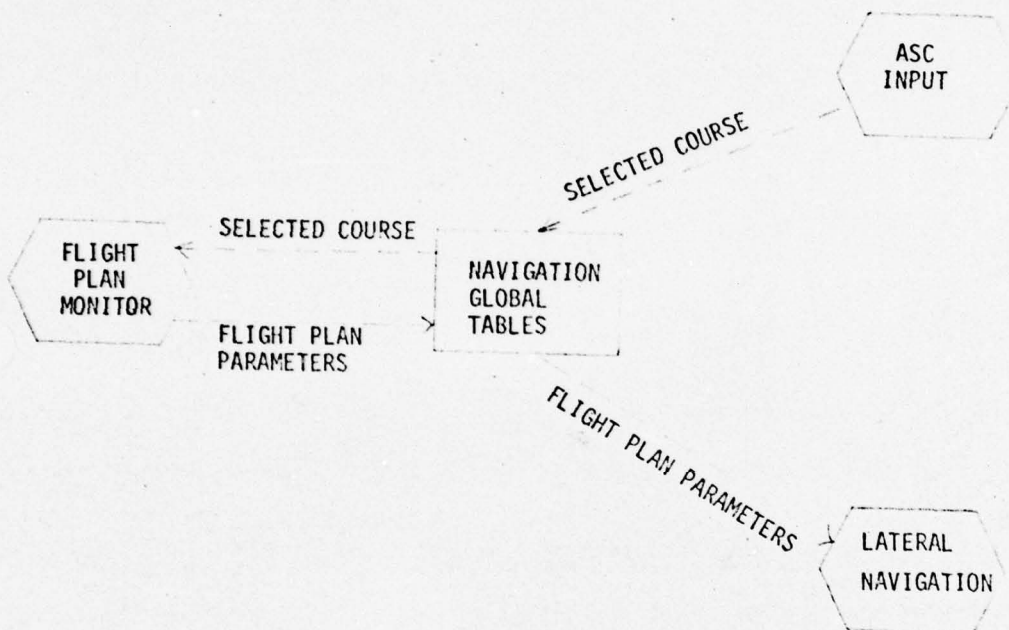


FIGURE 3-3

Software Interfaces used to implement HSI Input for Selected Course



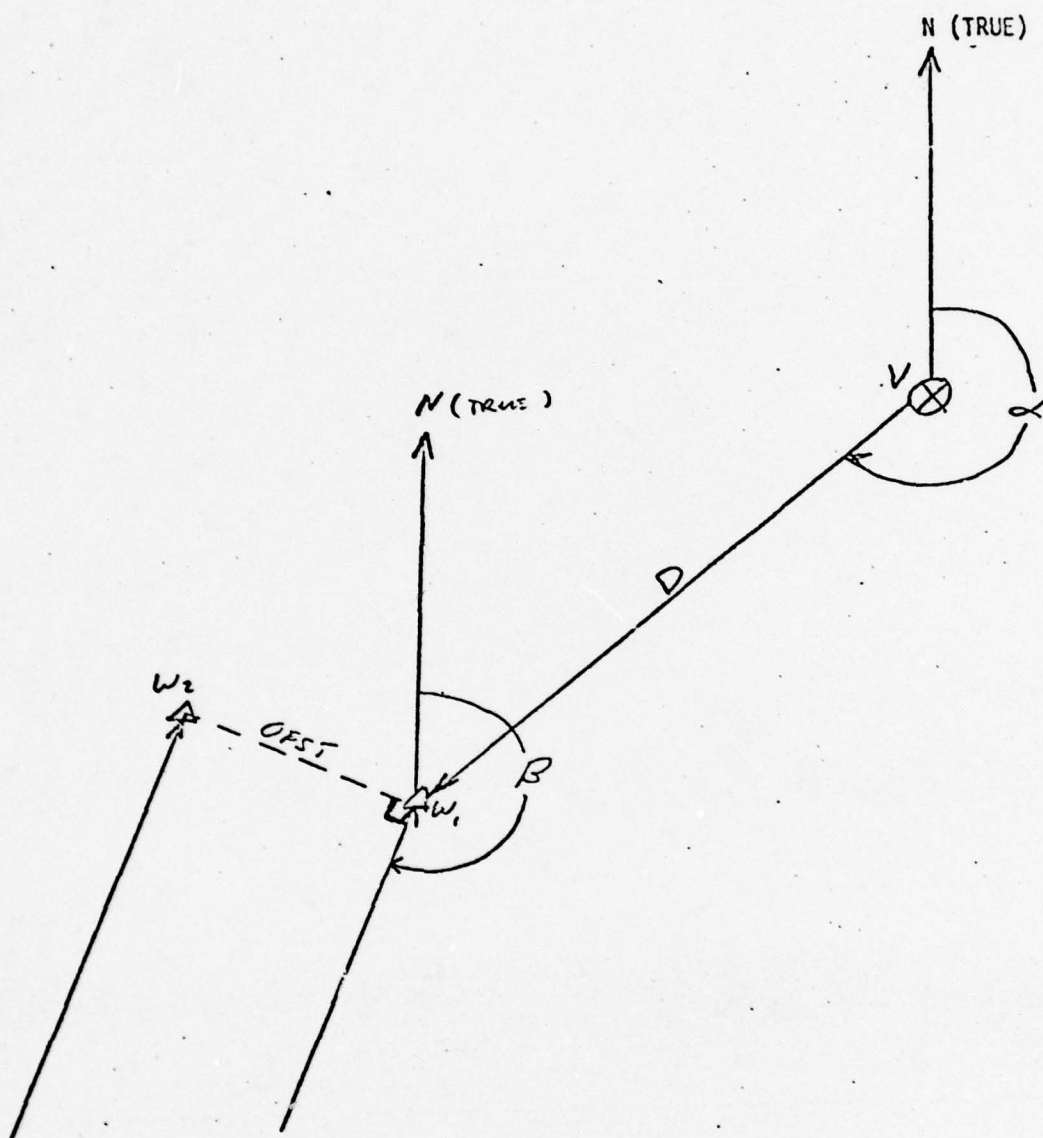


FIGURE 3-4

Geometry for Computation of Waypoint Referenced for Navigation Purposes

- V: Navaid specified on Progress page
- $\alpha$ : Bearing specified as Waypoint Parameter on Progress page
- D: Distance specified as Waypoint Parameter on Progress page
- W<sub>1</sub>: Coordinates of Use Waypoint
- B: HSI Input for Desired Course
- OFST: Parallel Offset as specified on Progress page
- W<sub>2</sub>: Coordinates of Waypoint referenced for Navigation



### 3.4 Time Control Algorithm

The 2D Plus Time Control System computations for Time Control are only applicable to the leg presently being flown. Maximum use is made of existing data declarations for the Base System. Software interfaces are similar to those defined for the Base System, i.e., control is given to a procedure called TIMCNTRL every cycle by the CDU Main Control Program. Procedure TIMCNTRL will monitor the system clock and status of flight plan revisions to determine the necessity of executing the Time Control Algorithm for the given cycle. A task description for TIMCNTRL is given below.

A program listing of the TIMCNTRL routine is given in Appendix D.

#### Task Description for the 2D Plus Time Control System

##### Time Control Algorithm

##### Task Specification for 2D

##### System TIMCNTRL Procedure

##### Procedure Type

Procedure TIMCNTRL ( )

##### Module

2D Plus Time Control System Version of Time and Speed Control

##### Task Summary

Time Control computations for the system are only valid for the present leg. Computations are performed whenever either 1) ten seconds have elapsed since the last execution of the Time Control Algorithm, or 2) a Flight Plan Revision has occurred since the last cycle. The latter condition is determined by monitoring NLTOCHG for a value of VALID.

Computations required for the display of Time Control parameters are recorded in VCOMI, VCOMIF, EARLY, TIMERR, and TIMERF. Declarations for this set of parameters are defined by the Base System insert file DATAZ611.

## Internal Data Structure

### Synonym Declarations:

CYCLE.TIME      Minimum time allowed between Time-Control computations.  
CYCLE.TIME is to be assigned a value of 10 seconds, i.e.,  
                  (10 sec) (1000000 us/sec)  
CYCLE.TIME =  $\frac{\quad}{\quad}$   
                  (409.6 us/count)

### Integer Declarations:

<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
TALCLOCK	Own record of last time that the Time Control Computations were executed.
GMTI	Own copy of GMTS expressed in terms of GMT units (12 hours).

### Real Declarations:

<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
ACTAS	Own snapshot of Aircraft True Air Speed.
ACALT	Own snapshot of Aircraft Baro Altitude.
ACIASERR	Own snapshot of IAS error as recorded by the IAS Instrument.
ACNWND	Own snapshot of the North Component for Wind.
ACEWND	Own snapshot of the East Component for Wind.
DESIRED.CRS	Own snapshot of the HSI course input.
WATK	Along-track component of wind for the vector whose origin and direction are given as present aircraft coordinates and DESIRED.CRS, respectively.
KALT	Altitude Proportionality factor required for the conversion from TAS to IAS.
KALTSKALE	Scale Factor required to prevent overflow for the TAS to IAS computation.
GMTR	Own copy of GMTS expressed in terms of Navigation Time Units.
GMTCONV	Conversion factor used to convert GMT to Navigation Time Units. GMTCONV = 10.8039624/12.
TTU.COM	Commanded Time-to-Go to arrive at the To-Waypoint.

Data Declarations External to Procedure TIMCNTRL;

Synonym Declarations assigned to VCOMIF:

<u>SYMBOLIC NAME</u>	<u>ASSIGNED VALUE</u>	<u>INSERT FILE</u>	<u>DESCRIPTION</u>
IASVALID	15	DATAZ6I1	A valid commanded IAS has been calculated by TIMCNTRL.
IVGMT	14	DATAZ6I1	Either 1) GMT has not been entered via the CDU, or 2) a power interrupt of duration exceeding two seconds has invalidated GMT.
IVTAS	13	DATAZ6I1	The Air Data Sensor input for TAS is invalid.
IVALT	11	DATAZ6I1	The Altimeter sensor input for Baro Altitude is invalid.

Integer Declarations:

<u>SYMBOLIC NAME</u>	<u>INSERT FILE</u>	<u>DESCRIPTION</u>
TCOM	DATAZ6I1	Commanded Arrival Time for the To-Waypoint.
TCOMF	DATAZ6I1	Validity flag (full word) for TCOM.
VCOMIF	DATAZ6I1	Validity flag (full word) for VCOMI.
TIMERF	DATAZ6I1	Validity flag (full word) for TIMEFRA and EARLY.
GMTS		Present value of GMT in seconds.
DMTGF	NTABN6I1	Validity flag (Byte) for DMTG.
DTTGF	NTABN6I1	Validity flag (Byte) for DTTG.
TASF	NTABN6I1	Validity flag (Byte) for TAS. TASF is declared as a component for pointer ADHD.
BALF	NTABN6I1	Validity flag (Byte) for Baro Altitude. BALF is declared as a component for pointer ADHD.



Real Declarations:

<u>SYMBOLIC NAME</u>	<u>INSERT FILE</u>	<u>DESCRIPTION</u>
VCOMI	DATAZ6I1	Commanded IAS displayed on the CDU and IAS instrument. VCOMI is a fraction of 1000 kts.
VCOMT	DATAZ6I1	Commanded TAS calculated by TIMCNTRL.
EARLY	DATAZ6I1	Early/Late indicator calculated by TIMCNTRL and used to control the EARLY and Late displays on the CDU. A positive value is used to indicate a late status.
TIMERR	DATAZ6I1	Expected arrival time error for the To-Waypoint. TIMERR is expressed in lateral navigation time units.
MINR	DATAZ6I1	Minimum magnitude that REAL numbers may be assigned on the U-1108.
MAX64		Maximum magnitude that Real numbers may be assigned on the U-1108.
DMTG	NTABN6I1	Distance between the aircraft and the To-Waypoint.
DTTG	NTABN6I1	Estimated time required to arrive at the To-waypoint.
TAS	NTABN6I1	Sensor input for True Air Speed. TAS is declared as a component for the ADHD structure.
BALT	NTABN6I1	Sensor input for Baro Altitude. BALT is declared as a component for the ADHD structure.
DELV	NTABN6I1	IAS Instrument Error. DELV is declared as a component for the ADHD structure.
HSICRS	NTABN6I1	Desired course as input via the HSI. HSICRS is declared as a component for the ADHD structure.
NWWD	NTABN6I1	North Component of Wind.
EWWD	NTABN6I1	East Component of Wind.



# Task Description

IF Ten seconds have elapsed since the last execution of the Time Control Algorithm

OR A flight plan revision has occurred since the last cycle (i.e., NLTOCHG EQL VALID)

THEN BEGIN ... Computations Required

Update own clock reading.

Assign an INVALID status to TIMERF, the validity flag for arrival time error.

Record the status of VCOMI i.e.,

VCOMIF = IF invalid GMT THEN IVGMT  
ELSE IF invalid aircraft true air speed THEN IVTAS  
ELSE IF invalid aircraft altitude THEN IVALT  
ELSE IASVALID

IF VCOMIF has a status of IASVALID

THEN BEGIN ... VCOMI VALID

After yielding channel time, record a snapshot of sensor data needed for own computations, i.e.,

ACTAS = Aircraft True Air Speed,  
ACALT = Aircraft Baro Altitude,  
ACIASERR = IAS Instrument Error,  
ACNWND = North Component of Wind,  
ACEWND = East Component of Wind,  
DESIRED.CRS = HSI Course Input.

Calculate the along-track component of wind for the course presently input via the HSI, i.e.,

WATK =  $-[ACNWND * \text{NCOS}(\text{DESIRED.CRS})$   
 $+ ACEWND * \text{NSIN}(\text{DESIRED.CRS})]$ .

Calculate KALT, the Altitude Proportionality constant, i.e.,

KALT =  $\text{RLMTF}[\text{ACTAS} - \text{VCOMI} - \text{ACIASERR}] * \text{KALTSCALE}, \text{ACALT} * \text{ACTAS} - \text{MINR}]$   
...Limit function used to protect against overflow in KALT computation.

KALT = KALT / (ACALT \* ACTAS).

Limit KALT to the interval (.10, .15), i.e.,

KALT =  $\text{RMAXF}[\text{RMINF}(\text{KALT}, .15), .1]$ .

IF a commanded arrival time has been entered via the CDU,

THEN BEGIN ... Valid Arrival Time

Calculate VCOMT, the commanded True Air Speed, i.e.,

$VCOMT = RLMTF(DMTG, DTTG - MINR) / DTTG - WATK.$

Convert Commanded TAS to Commanded IAS, i.e.,

$VCOMI = [MAX64 - (KALT * ACALT) / KALTSCALE] * VCOMT.$

Limit VCOMI to upper limit of IAS instrument (300 kts for G-I,  
410 kts for C-880).

Determine commanded Time-To-Go, i.e.,

$GMTI = TCOM - GMTS$  ...Integer arithmetic required as GMTS is  
declared an Integer.

$TTGCOM = GMTR / GMTCONV$  ...Convert to Lateral Nav Time Units.

$EARLY = TTGCOM - DTTG.$  ...Sign of EARLY provides EARLY/LATE  
indication for CDU Display.

$TIMERR = ABS(EARLY)$  ...Record magnitude of arrival time  
error for CDU display.

END ...Valid Arrival Time.

END ...VCOMI VALID.

Assign an INVALID status to NLTOCHG to indicate computations are not required  
next cycle.

END ...Computations Required.

Section 4  
RNAV/ILS INTERFACE DESIGN

4.1 Introduction

The ILS program is managed by a main or executive routine. This routine is an interface between the ILS program and the navigation program. This section describes operations which transition the boundary between the ILS executive program and the 3D/4D main program. A description of the executive program is contained in Appendix E.

4.2 Operation

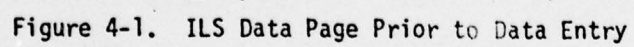
4.2.1 Mode Selection

The overall view of the ILS mode is achieved by selecting the ILS page. This is done by pushing the ILS line select key with the INDEX page on the CDU. After pushing this key, the ILS page will appear on the CDU. Refer to Figure 1 for a diagram of the ILS CDU page. If the localizer programs are not in core, the ILS page will indicate dashed lines under the STATUS label. At any time the parameters ILS FREQ, TD WPT (touchdown waypoint), RWY CRS (runway course), LENGTH (runway length) can be entered for data storage to be used for the ILS computations. Allowable ranges for these parameters are as follows:

- |                       |   |   |
|-----------------------|---|---|
| a. Runway courses     | 0-360 degrees                                 | error message on scratchpad if not within these bounds -- will not accept further commands until error message removed. |
| b. Runway length      | 5-16 thousand feet                            | error message if not within these bounds -- defaults to 9,000 feet  |
| c. ILS frequency      | a valid ILS frequency                         | error message if non-ILS frequency -- cannot accept further commands  |
| d. Touchdown waypoint | A waypoint already entered in the flight plan | error message if cannot be found -- cannot accept other commands until message has been cleared.                        |

The ILS program tape will be loaded when the ILS page is "up" and when mode is selected for the first time. The three modes available are LOC, APPR AUTO, and RNAV. LOC is an ILS mode using only localizer guidance. APPR AUTO is an ILS mode using localizer and glideslope guidance. The operation of the ILS modes will be discussed in a later paragraph.







When the program is loaded, a message will indicate that a "DATA SEARCH" is in effect. The ILS computations will not be accessed until the program is completely loaded. The mode selected will be checked for validities and if the mode is not generated, an INVALID message will be displayed near the mode selector (on the same line). If at any time the mode becomes valid, INVALID will be extinguished. If the mode is again selected, LOC or APPR AUTO will be displayed under STATUS and it will become engaged. If during the engagement of LOC a capture has not been effected and APPR AUTO is selected, and if the validities are checked and approved for APPR AUTO, then APPR AUTO will replace LOC under STATUS. If the validities do not check, INVALID will be displayed by APPR AUTO mode. Once the INVALID extinguishes, if it does, the mode must be reselected before it will take. Before any attempt to use either mode, the INVALID will not appear. In other words, the INVALID can occur only after a request has been checked and refused. Notice that the refusal of APPR AUTO does not discontinue the present use of LOC. The program tape will be loaded if R-NAV is selected. The program tape will also be loaded with the selection of the LOC or APPR AUTO modes. When R-NAV is used to load the program tape, R-NAV remains as the STATUS or selected mode.

To discontinue the use of ILS modes, R-NAV is selected. If AP is disengaged, R-NAV will appear under STATUS and R-NAV will be engaged and a message will appear in the scratchpad: PUSH TO RELOAD R-NAV DATA. Upon the second selection of R-NAV, the R-NAV data base will be overlaid, removing the ILS program. DATA SEARCH will be displayed on the scratchpad while the transition is occurring. ILS will not be used or serviced in any manner during the transition. If localizer is in progress and the autopilot is engaged, R-NAV will not become engaged with the selections of R-NAV. A message will appear on the scratchpad indicating that "DISENGAGE A/P BEFORE SELECTING R-NAV." The re-loading of the R-NAV data will also be prevented until A/P disengage.

#### 4.2.2

##### Annunciators

An ILS ANNUNCIATOR panel will be mounted on the glareshield. The annunciator panel will display messages as shown in Figure 2. LAT NAV will be annunciated when the autopilot is engaged (APENG) or the flight director is engaged (FDENG), the R-NAV system is engaged and the system is not ignoring conventional R-NAV steering outputs (i.e., not during localizer capture/tracking). LOC ARM is annunciated during localizer arm. LOC is annunciated during localizer capture.

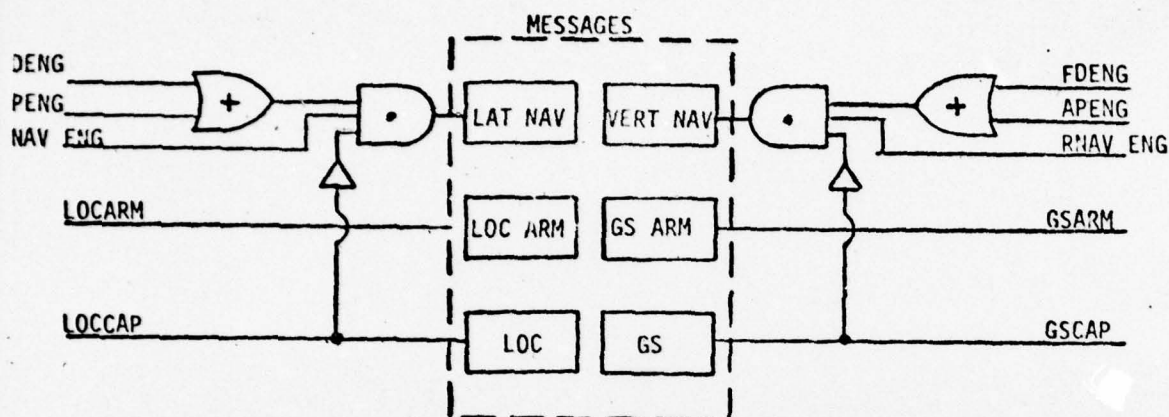


Figure 4-2. RNAV/ILS Annunciator Panel Messages

Similar logic holds for V-NAV. VNAV is annunciated when the auto-pilot is engaged, (APENG) or the flight director is engaged (FDENG), the VNAV system is engaged and the system is not in glideslope capture/tracking. G/S ARM is annunciated during glideslope arm. G/S is annunciated during glideslope capture.

#### 4.2.3 Mode Description

##### LOC (LOCALIZER) MODE

Selection of the LOC mode will automatically inhibit the glideslope computations. Only a localizer capture and/or track will then result. If the capture conditions or logics have not been satisfied and the processor is in a valid R-NAV submode it will continue to fly the submode until the capture conditions are satisfied. If capture conditions are satisfied and exceeded (track conditions exist) the computations will automatically compute track computations. At the time of LOC mode selection, all validities or parameters monitored must be valid to engage the mode. Once engaged, loss of any validity will cause the computer flag output to drive the computer flag in the ADI.

Signals monitored: LOC SUPER FLAG, LOC FREQ, COMPASS.

Annunciator sequencing: LAT NAV, LAT NAV and LOC ARM, LOC

#### APPR AUTO (APPROACH AUTOMATIC) MODE

APPR AUTO mode is much like LOC mode except automatic glideslope captures can be effected. The computer will sense and switch both localizer and glideslope computations according to the level of the logics. That is, if localizer and glideslope capture conditions are not satisfied, the submodes will continue to be used. Upon proper detection of the necessary conditions to effect captures, the captures will occur automatically. If the capture conditions have been satisfied by either or both channels, either or both will start computing the track computations. Glideslope capture is inhibited from occurring before LOC capture.

Signals monitored: ALL OF THOSE IN 4.2.3 and G/S SUPER FLAG, ALTITUDE.

Annunciator sequencing: LAT NAV AND VERT NAV, LAT NAV AND VERT NAV and G/S ARM and LOC ARM, LOC and G/S.

#### 4.2.4 Display Control

The ILS maneuver will be performed using an ADI and HSI much as is done with existing conventional systems. Steering commands for the flight director will be supplied to the flight director computer for display on the ADI. Deviation indicators will be driven by the 3D/4D ILS computations during the ILS approach.

The HSI will be controlled whenever a valid LOC ARM is annunciated or latched. Control over the course pointer, deviation indicators and distance readout will be effected by the 3D/4D main program at that time.

#### 4.3 ILS EXECUTIVE PROGRAM OPERATION

The ILS executive program interfaces the ILS approach computations with the overall 3D/4D main computational program. The executive program converts data passed to it from the main 3D/4D program for use in the glideslope and localizer computational routines. In the ILS executive program decisions are also made on validities and mode selection logic. Basically the ILS executive program provides overall administration to the computational routines. The operation as described in the previous sections of this paper are partly accomplished by the ILS executive program. The other part is accomplished by the 3D/4D main program. Figure 4-3 is the flow diagram for the ILS executive program. AED coding of ILS executive program is included in Appendix E. From Figure 4-3, when the ILS page has been selected and the ILS program has been loaded from tape, the ILS executive program is serviced by transferring data to the ILS executive program. This is followed by a preset (initial conditions operation).

From data passed from the 3D/4D program and ILS page, the distance to touch-



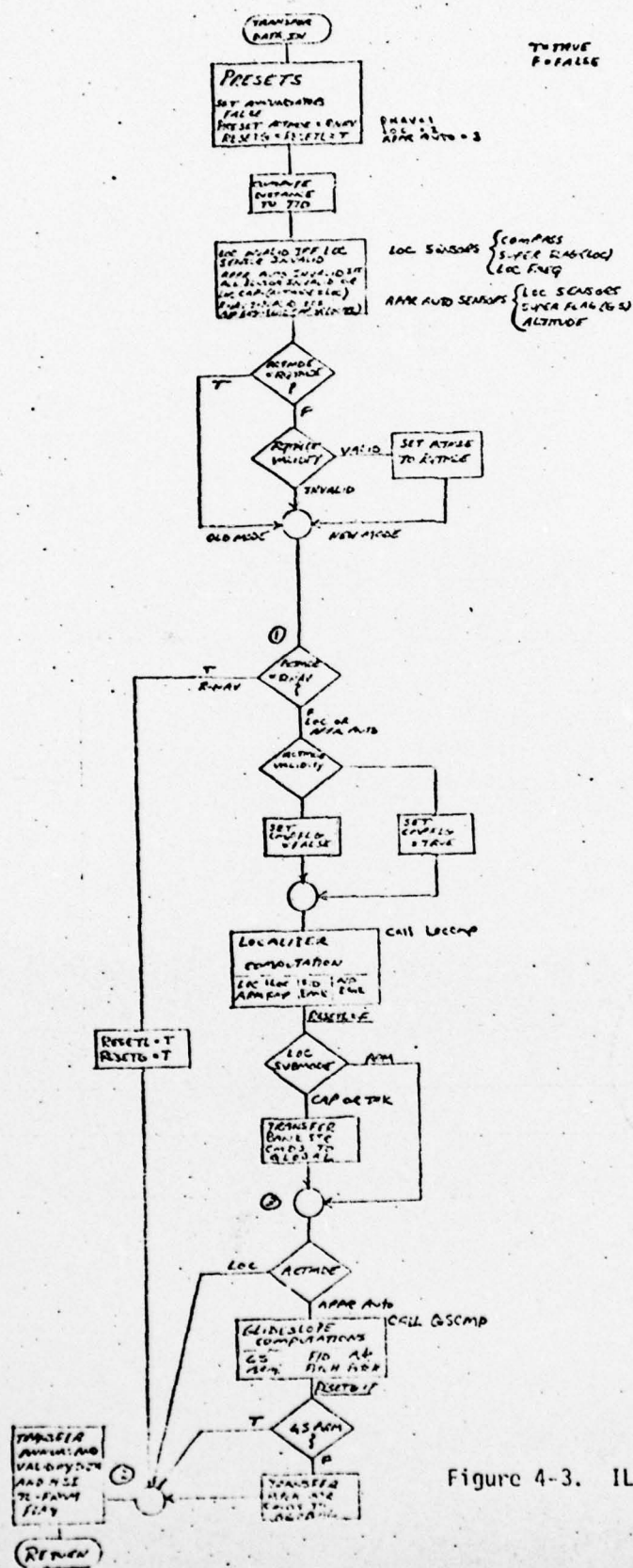


Figure 4-3. ILS Executive Program Flow



down is now computed. Next in sequence, the mode validities are update to establish the validity of each mode serviced by the ILS executive program.

At this point, the present requested mode is compared to the mode now considered active by the ILS executive program. If the requested and active mode are the same, program flow is routed to point 1.

If the requested mode is not the same as the active mode, the validity of the requested mode is checked. If the requested mode validity is true (mode valid) then the active mode is set to the requested mode. If the requested mode is false (mode checked invalid), the previous active mode is retained (requested mode denied).

Program flow now proceeds to point 1. If the active mode is R-NAV, program flow is routed directly to point 2. R-NAV pitch and roll steering data is transferred back to the 3D/4D main program unaltered. Notice also before control is transferred back to the 3D/4D main program, annunciator and mode validity updates are transferred back to the 3D/4D main program. This is true every computational cycle.

The parameter RESETL and RESETG was set true when program flow was routed control from point 1 directly to point 2. These parameters are always maintained true until after the first time either the localizer computation or glideslope computation is executed. The resets will be further treated below.

At point 1, should the active mode be either localizer (LOC) or approach auto (APPR AUTO), then the next action is to check the validity of the active mode. The computer flag is next set depending upon whether the active mode validity is true or false. If the validity is true (mode determined valid), the computer flag is set true (not displayed). If the validity is false, the computer flag is set false (the computer flag on the ADI is displayed).

At this point the localizer computations (localizer control laws for determining roll steering commands) are serviced. When control returns to the ILS executive routine RESETL is set false. RESETL has been used to establish that the localizer computations have been serviced for the first time. This is used as a key for setting initial conditions. Notice that RESETL will now be false unless R-NAV mode is re-established.

From information passed to the executive program from the localizer computation, the ILS main program passes bank steering commands to the 3D/4D main program if the localizer mode has been determined to be in a capture or track submode. If in the arm submode, bank steering commands are not passed to the 3D/4D main program. Control is essentially achieved therefore by the ILS main program overwriting the R-NAV steering commands. Notice that no overwriting will occur if the arm submode is the present status. R-NAV continues to be flown during the arm submode.

After passing through the localizer routines, a decision is made based upon whether the active mode is localizer or approach auto. If localizer mode is the active mode program flow proceeds directly to point 2. Otherwise the glideslope computations are serviced. The operation of the ILS executive program in regard to the glideslope computations is almost identical to that described above for the localizer computation. RESETG is used in an identical manner to the use described for RESETL above.

Once point 2 has been reached independent of the route, annunciator and validity data is transferred to the 3D/4D main program. The HSI to-from flag information is also passed at this point. The ILS executive program is now exited and program flow moves to the 3D/4D main program.

The flow graph of Figure 4-3 describes one computational cycle of the ILS executive program. The ILS computation is processed five times a second and its throughput time is in the order of milliseconds.

Section 5  
LATERAL ILS CONTROL LAW  
DESCRIPTION AND ANALYSIS

5.1 Introduction

There has been interest for some time in using area navigation system derived data to aid in localizer captures. Reference 1 describes one preliminary Collins' study that investigated this technique. Localizer capture algorithms in general suffer from two important disadvantages. Range information is not generally available, hence the capture law is usually optimized for a given range and performance degradation occurs on either side of the optimum range. Reference 2 describes an attempt to overcome some of this deficiency by estimating range from beam and air data. This approach showed promise but if an area navigation system were available, range information would be inherently present. The second difficulty in localizer captures is that the localizer beam provides angular deviation from a reference centerline. Hence as one moves closer to the localizer antenna, the "beamwidth" of the localizer beam in distance units (e.g. ft.) grows smaller. Thus the available space to execute a turn onto final course once the beam is intercepted shrinks rapidly. As an example, the turn radius associated with  $30^\circ$  of bank at an airspeed of 200 ft/sec implies that for a 90 degree beam intercept, centerline overshoot will occur at ranges shorter than 7.5 nm assuming capture starts (with instantaneous  $30^\circ$  of bank) at 200 ft/sec deviation. At higher airspeeds, the minimum range without overshoot will increase. An area navigation system offers potential alleviation of this situation by permitting the initiation of captures prior to beam intercept, thus avoiding the geometry limits described above. The R-NAV aided approach also has problems, however. The inherent errors in the R-NAV estimates of position and velocity are such that if care is not exercised, a capture initiated on R-NAV data may turn short missing the beam entirely or such a capture may turn late resulting in gross overshoots. Reference 1 described two approaches to overcoming these problems. The first approach involved never turning to a lesser course cut than  $45^\circ$  before intercepting the beam. This worked well in terms of localizer overshoot but resulted in two distinct "up-down" bank commands or a "double bank" characteristic which was considered by some to be objectionable. The second approach studied in Reference 1 was to always initiate the R-NAV aided capture with  $30^\circ$  of bank command, but to start fading the bank command almost immediately so that hopefully a smooth blend with beam based bank commands at localizer intercept resulted. This approach had a more desirable bank characteristic but appeared to pose formidable difficulties in properly programming the bank command fade in general. The approach to be discussed in this section avoids the double bank characteristic, uses an adaptable initial bank command (i.e. not always 30 degrees), and provides a solution to the bank command fade problem in the case where the system is tending to turn short of the beam.



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3D/4D AREA NAVIGATION SYSTEM DESIGN, DEVELOPMENT AND IMPLEMENTA--ETC(U)  
JUN 77 J M BRUCKNER, F B BENSON DOT-FA72WA-3123

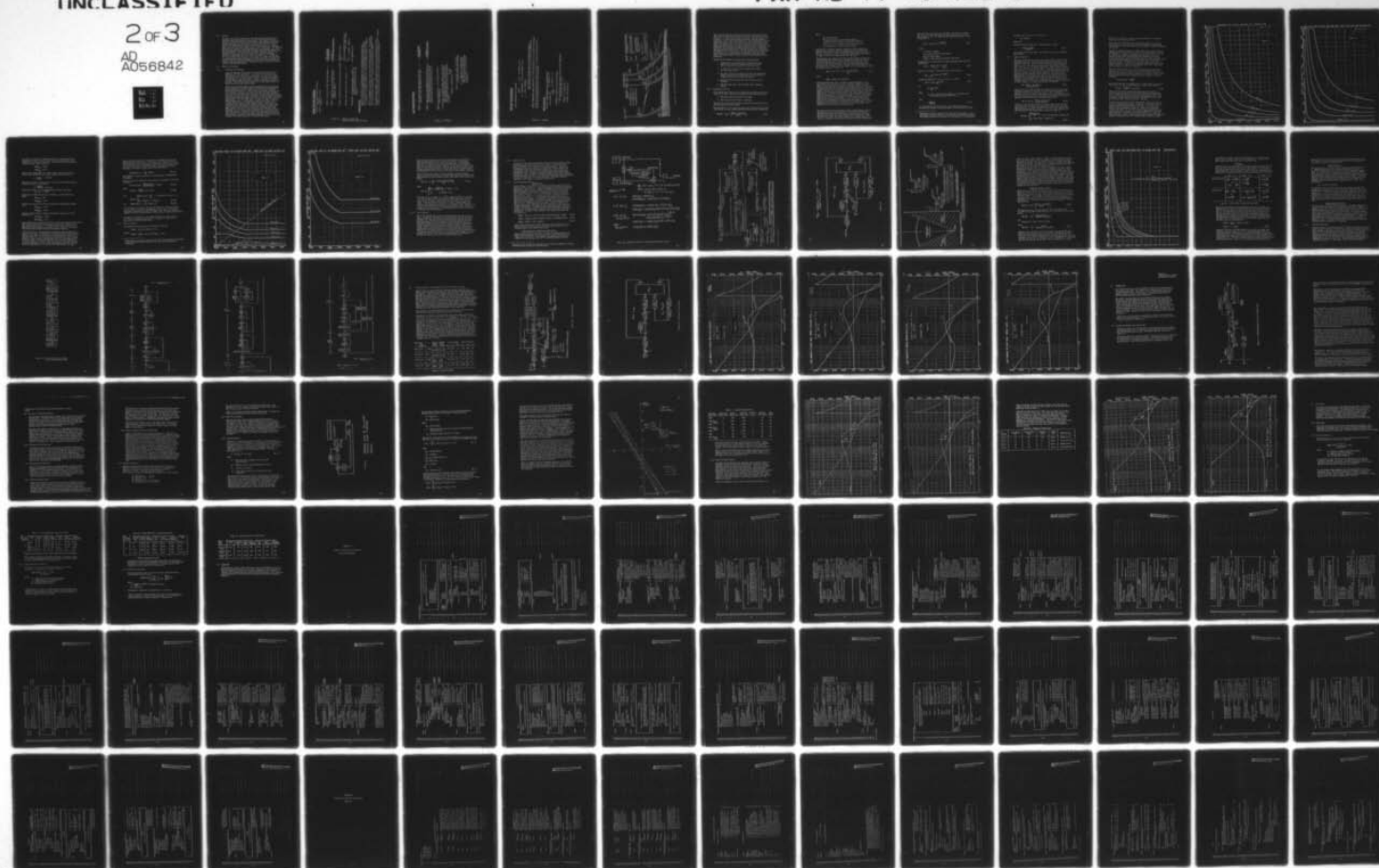
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## 5.2 Summary

An R-NAV aided capture algorithm has been developed which provides good localizer capture performance in the presence of nominal R-NAV errors. The system uses R-NAV aiding only when needed. When geometry constraints permit, the system uses primarily beam data and bank information relying on the R-NAV system only for range as a primary piece of data. Track angle error from the R-NAV system is used in this mode but in a way that makes the system relatively insensitive to errors in this data. The technique developed here assumes an integrated R-NAV/ILS flight computer, but could be readily adapted to separate R-NAV and flight computers with minimal interface requirements. This report does not detail simulation results, but design goals of maximum localizer overshoot less than 30  $\mu$ A and bank activity in established track less than 1° rms with 2.5  $\mu$ A, 1 $\sigma$  beam noise ( $\tau = 4$  sec.) and R-NAV errors of  $\pm 2$  nm in CTD,  $\pm 2^\circ$  in TAE, and  $\pm 40$  ft/sec in ground speed have been demonstrated in hybrid simulation at ranges from 5 nm to 25 nm from localizer antenna and course cuts from 0 to 90 degrees. Simulation results are detailed in Reference 4. Table 5-1 provides a concise summary of the developed system.

## 5.3 Details of the Study

### 5.3.1 Framing of the Strategy

Figure 5-1 illustrates three potential situations that may occur when performing an R-NAV aided capture. For convenience they will be referred to as the "turn short", "good data", and "turn long" cases. For captures with trip point within the beam, as shown in the fourth case of Figure 5-1, no R-NAV aiding is needed. Also shown in Figure 5-1 are the required bank traces for each case if a successful capture is to occur. The following argument serves to validate the selection of these three R-NAV aided cases as basic.

If one is to start the capture based on R-NAV data, he has no choice but to establish a trip point algorithm based on area navigation data and consequently must design a system to be tolerant of trip point shifts due to R-NAV errors. Since capture trip points in general must be a function of velocity, this means not only cross track distance errors but also velocity errors will affect the trip point computation. Assuming a constant bank capture algorithm, the three possible situations that may exist once the capture has begun are shown in Figure 5-1 as discussed above. The "turn long" case is critical in terms of amount of bank command to use. If the system is turning long then a "reserve" of bank command must be available (once beam data is present) to increase the bank command to the required amount. Hence, since the "turn long" case may be present, the nominal bank in an R-NAV aided capture should not be the bank command limit (normally about 30°). Note, however, that this is not an absolute constraint but rather a consequence of the strategy being considered here. One could always force the system to "turn short" (see below) and thus avoid the "turn long" case entirely, but the strategy adopted here seems more natural to the author. In summary, the approach adopted is to leave some room for bank to increase in case the "turn long" case occurs.

### CAPTURE TRIP POINT COMPUTATIONS

CAPTRP = Cross Track Distance Trip Point

CAPTRP =  $\left( \frac{\text{CAPNAV}}{\text{CAPILS}} \right) + \text{CTD.ADJ}$

$$\text{CAPNAV} = \text{Trip Point for RNAV initiated capture} = \frac{V_g^2 (1 - \cos(\text{TAE}))}{g \tan(\text{CAP.BNK})}$$

$$\text{CAPILS} = \text{Trip Point for ILS initiated capture} = \frac{(\text{CTR.BCI})^2}{(g \tan(\text{CAP.BNK})) (1 + \cos(\text{TAE}))}$$

(CTRBCI is cross track rate from the beam data filter)

$$\text{CTD.ADJ} = \text{Compensation for bank rate command limit (RCL)} = \frac{\text{CAP.BNK}}{\text{RCL}} * V_g \sin(\text{TAE})$$

$$\text{CAP.BNK} = \text{Bank (deg) to be used in capture} = \begin{cases} -\text{MAX.CAP.BNK} * \frac{\text{TAE}}{90} & \text{if magnitude of result is } \geq 5^\circ \\ -5 * \text{sign}(\text{TAE}) & \text{otherwise} \end{cases}$$

$$\text{MAX.CAP.BNK} = \text{Programming parameter on CAP.BNK} = \begin{cases} 8^\circ & \text{if } \text{RNGLOC} \leq 25^\circ \\ 17^\circ & \text{otherwise} \end{cases}$$

Corresponds to CAP.BNK at TAE = 90°.  
RNGLOC is distance (nm) to localizer antenna.

### CAPTURE INHIBITS

Capture is inhibited at computed (based on R-NAV data) deviations greater than nominally 7° to guard against decreasing localizer receiver output at wide angles. This computation is sensitive to ANAV errors and could compute a value as low as 4° or as high as 10° with typical A-NAV errors. Applicable software variable is "DEVFLG".

NAVCAP is inhibited if the range is such that R-NAV aiding is not needed. This prevents early trip (NAVCAP) in those cases where CTD errors from the ANAV would initiate (unnecessarily) capture outside the beam edge. Applicable software variable is "ILSLOC".

Localizer deviation (LOCDEV) is rate command limited (limit is programmed with TAE and airspeed) to protect against sudden transients which could cause false captures as well as command transients. Applicable software variable is MXDLDV ("maximum delta in deviation").

Table 5-1. Summary of RNAV Aided Localizer Capture and Track Laws



# BANK COMMAND DURING CAPTURE

BCMDNC - Bank command "NAV CAP" based on R-NAV data  
(CTDNAV is cross track distance from R-NAV) ----- =  $\frac{Vg^2(1-\cos(TAE))}{g \text{ CTDNAV}}$

BCMDBC - Bank command "beam capture" based on ILS data  
(CTRBC =  $\text{CTRBCI} \cdot \cos(TAE) + (Vg \sin TAE) \cdot (1 - \cos TAE)$ ) ----- =  $\frac{(\text{CTRBC})^2}{g \text{ CTDBC}(1 + \cos(TAE))}$   
where CTRBCI and CTDBC are cross track rate and distance respectively from the beam data filter.

BCMDNC fades to BCMDBC with a 1 sec exponential fade at beam interception.

If "turn short" is detected BCMDC fades by the algorithm below until beam intercept. Turn short test is  $|TAE| < .95 \cdot TAE_{BE}$  where TAE<sub>BE</sub> is the magnitude of the predicted track angle error at beam intercept (see text)

$$\text{BCMDNC}(t) = \text{BCMDNC}(t_s) * e^{-\left[ \frac{(t-t_s)}{\tau_B} \right]}$$

where  $t_s$  is the time at which "turn short" is detected and the fade is started;

$\tau_B$  is a computed time constant (see text) that fixes the permissible additional heading change in NAVCAP to insure against turning parallel to the beam.

### TRACK TRIP POINT COMPUTATIONS

Track Computations are used when

LOCDEV < 30  $\mu$ A for RINGLOC  $\leq$  13 nm  
 or LOCDEV \* RINGLOC < .091 nm for RINGLOC > 13 nm  
 or |TAE| < .9 \* TAETRK

where TAETRK is the magnitude of the predicted track angle error at track intercept (i.e. 30  $\mu$ A or .091 nm as appropriate)

Capture Computations fade exponentially to track computations with a 5 second time constant.

The TAE test is to prevent turning parallel to the beam in extreme cases and should not normally be the determining factor in initiating Track.

### TRACK COMPUTATIONS

BNK.CMD = RINGPGM(KCTDTRK \* CTDBC + KCTRTRK \* CTRBC)

where RINGPGM =  $\begin{cases} 1 & \text{for RINGLOC} \leq 7 \text{ nm} \\ 7 & \text{for RINGLOC} > 7 \text{ nm} \\ \text{RINGLOC} & \end{cases}$

and RINGLOC is distance to localizer antenna.

CTDBC and CTRBC are cross track distance and rate respectively from the beam data filter.

KCTDTRK = (3.2 deg/70 ft.)

KCTRTRK = (35 deg/70 fps).

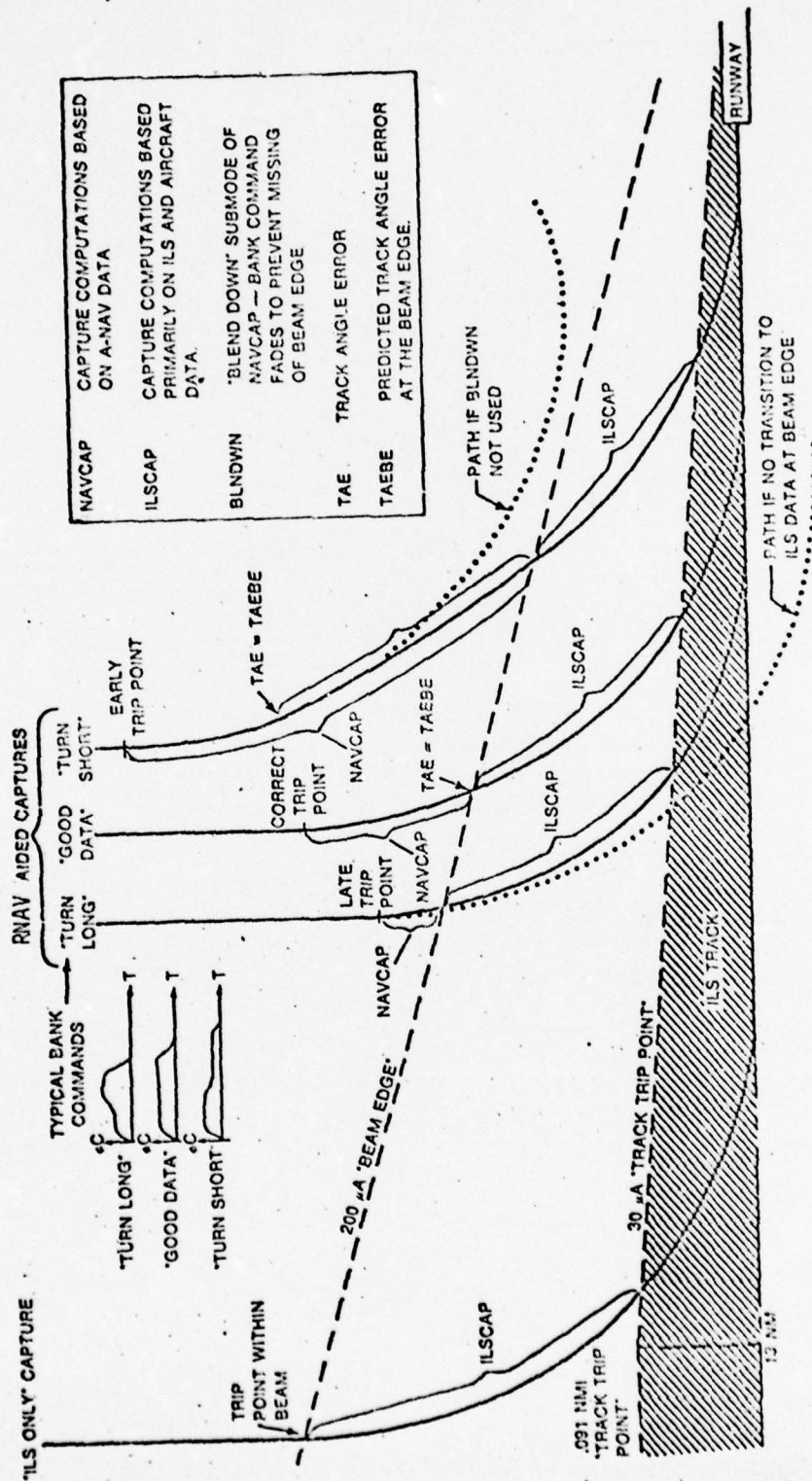


Figure 5-1. Area Nav Aided Localizer Capture.



The other disconcerting situation that can occur is the "turn short" case. Here one must be very careful because the beam could be missed entirely (i.e. beam intercept might not occur). To guard against this situation, some means must be present to detect when the system has turned far enough. Recall that Reference 1 took the approach of never letting the system turn to less than a 45° course cut relative to the beam. The approach here is similar in that it restricts course cut relative to the beam, but is a new development in that it conditions the permissible minimum course cut based on the state of the system and provides a precise bank command fade algorithm which is a function of the computed minimum course cut. This will be discussed in more detail in Section 5.3.2. For the moment, we note that in the "turn short" case a "blend down" algorithm must be provided to prevent turning parallel to the beam and to smoothly transition bank command to beam based data.

Several design problems are posed by the discussion above:

1. A capture trip point algorithm is needed which keeps nominal bank in capture significantly less than the bank command limit to handle the "turn long" case.
2. A "blend down" algorithm must be provided to handle the "turn short" case.
3. Good data filtering is needed to provide noise suppression without excessive lag in order that the real system will closely approximate the theoretical system.
4. Smooth transition between modes and data bases must be provided.
5. The individual pieces must be melded into a composite system.

### 5.3.2 "Blend-Down" Algorithm

As discussed above, the need for a blend-down algorithm arises in the "turn short" case. There are two aspects of the blend-down problem.

1. When should the blend-down be initiated?
2. How should the blend-down be programmed?

The first of these questions requires addressing the problem of "when has the system turned far enough?"

From Reference 2, if the system is executing a constant bank turn onto final course, the bank command (BNK-CMD) should obey the relationship

$$\text{BNK.CMD} = -\tan^{-1} \left( \frac{Vg^2 * (1 - \cos(\text{TAE}))}{g * \text{CTD}} \right) \quad (5.1)$$

where

Vg is ground speed

TAE is track angle error or angle of ground velocity vector relative to the runway centerline

CTD is cross track distance to localizer centerline

g is gravitational constant (32.17 ft/sec<sup>2</sup>)

and consistent units are assumed. Equation 5.1 holds through the entire capture maneuver; and if all assumptions are satisfied, TAE and CTD change in such a way that BNK.CMD remains constant, assuming no wind. If there is a wind, the bank must change during the capture in order to maintain a circular track over the ground.

In particular, for a capture initiated outside the beam on R-NAV data and neglecting wind for the moment, Equation 5.1 should hold at the instant of beam intercept. Now at beam intercept, since one knows range and localizer deviation (LOC.DEV), he can compute cross track distance at the beam edge (CTDBE). Further, since Vg and BNK.CMD are known, one can compute the track angle error at the beam edge (TAE<sub>BE</sub>) by solving Equation 5.1 for TAE as

$$TAE_{BE} = \cos^{-1} \left[ 1 - \frac{g \tan(-BNK.CMD) * CTDBE}{Vg^2} \right] \quad (5.2)$$

where

$$CTDBE = Range * \sin (LOC.DEV)$$

with appropriate units used. If wind is present Equation 5.2 will still hold at any particular instant in the turn. However, in simulation, certain combinations of errors caused BNK.CMD to converge in such a way that the TAE<sub>BE</sub> computation converged toward zero. Since this is highly undesirable it was judged best to compute TAE<sub>BE</sub> once only at capture initiation and accept any resulting anomalies due to wind, which should not be too serious since wind will still be factored correctly into command. Equation 5.2 is basically only used to define the trip point for transition to the blend-down submode. That is, one computes TAE<sub>BE</sub> at the initiation of capture and as the capture proceeds, he continually tests TAE against TAE<sub>BE</sub>. If the condition TAE = TAE<sub>BE</sub> occurs prior to encounter of the beam edge, the system is presumably turning too fast and fading of the bank command should begin. If beam encounter occurs prior to TAE = TAE<sub>BE</sub>, then the system should fade immediately to bank command based on beam data.

The second aspect of the blend-down problem is the question of how to fade the bank. Assuming an exponential fade on bank command, the following development shows that the time constant of the fade can be computed such that for a fade beginning at the point TAE = TAE<sub>BE</sub>, the system will never turn further than to TAE = k\*TAE<sub>BE</sub> where 0 < k < 1. That is, a parameter k can be specified such that under no conditions

will the system turn parallel to the beam. For example, if TAEBE = 30° and k = .5, then the system will always intersect the beam at TAE ≥ k\*TAEBE = 15°. The expression for faded bank command is given in Equation 5.3

$$\phi_c(t) = \phi_c(t_0) \exp \left[ \frac{-(t-t_0)}{\tau} \right] \quad (5.3)$$

where

t is time in seconds

t<sub>0</sub> is time at which the fade begins

φ<sub>c</sub>(t) is bank command

φ<sub>c</sub>(t<sub>0</sub>) is bank command just before fade starts

If the maneuver is coordinated and neglecting lags between bank and bank command

$$\dot{\psi}(t) = \frac{g \tan \phi_c(t)}{U_0} \approx \frac{g \phi_c(t)}{U_0} \quad (5.4)$$

where U<sub>0</sub> is airspeed. Substituting from equation (5.3)

$$\dot{\psi}(t) = \frac{g}{U_0} \phi_c(t_0) \exp \left[ \frac{-(t-t_0)}{\tau} \right] \quad (5.5)$$

Integrating equation 5.5 from t = t<sub>0</sub> to t = ∞ yields

$$\psi(\infty) = \psi(t_0) + \frac{g\tau}{U_0} \phi_c(t_0) \quad (5.6)$$

or

$$\Delta\psi = \frac{g\tau}{U_0} \phi_c(t_0)$$

where

Δψ = ψ(∞) - ψ(t<sub>0</sub>) is the change in ψ that would occur if the fade continued indefinitely.

Thus

$$\tau = \frac{U_0 \Delta\psi}{g\phi_c(t_0)} \quad (5.7)$$

is a relation for the time constant of the fade which permits us to specify the maximum permissible change in heading during the fade\*.

---

\*Admittedly a number of approximations are made here, notably  $\dot{\psi} \approx \tan \dot{\phi}$  and neglecting of bank loop lags, but inclusion of these details would be somewhat gruesome and would not alter the essence of the development.



An appropriate choice for  $\Delta\psi$  seems to be

$$\Delta\psi = k * TAEBE$$

where  $0 < k < 1$ .

Substituting this choice for  $\Delta\psi$  into Equation 5.7 yields

$$\tau = \frac{U_0 (k * TAEBE)}{g \phi(t_0)} \quad (5.8)$$

as an expression for the fader time constant to be used in the blend-down submode.

### 5.3 Capture Trip Point

The basic requirement for capture trip point is that it be such that reasonable banks are used in capture and reasonable overshoots occur under all conditions. Generally bank command is restricted to less than  $30^\circ$  in magnitude and it is highly desirable to keep overshoots less than  $30 \text{ LA} (-.4^\circ)$  of localizer deviation. Other factors may also enter. For example, if no R-NAV system is available, clearly the trip point must be within the beam resulting in geometry limits for certain close-in captures. Pilots often have very definite opinions about how the bank should behave under given conditions. It should also be apparent that the conditions above involve the form of the capture bank command at least implicitly. That is, the capture trip point is obviously not independent of the bank to be used in capture. If one assumes a circular capture (i.e. constant bank), it is interesting to solve Equation 5.1 for CTD to illustrate the CTD required to execute a circular capture as a function of  $V_g$ , TAE, and  $BNK.CMD$

$$CTD = \frac{V_g^2 (1 - \cos(TAE))}{g \tan(BNK.CMD)} \quad (5.9)$$

Equation 5.9 illustrates the generally applicable point that capture trip point expressed in CTD terms is a function of ground speed, TAE, and bank command to be used in the capture. Since it appeared feasible to specify a desired bank during capture, the approach decided on in this study was to specify the capture bank ( $CAP.BNK$ ) and then use Equation 5.9 to determine the trip point, specifically

$$CTD \text{ Trip Point} = \frac{V_g^2 (1 - \cos(TAE))}{g \tan(CAP.BNK)} \quad (5.10)$$

Further, it was felt that  $CAP.BNK$  should be a function of TAE, that is at high angle course cuts more bank should be used than for lower angle course cuts. Further, to prevent very small bank captures, the restriction was added that  $|CAP.BNK| \geq 5^\circ$  in all cases. Summarizing this relationship, the capture bank in degrees is given by

$$CAP.BNK = \begin{cases} \frac{-MAX.CAP.BNK}{90^\circ} * TAE \dots (\text{if magnitude of result} \geq 5^\circ) \\ -5 * \text{Sign}(TAE) \dots (\text{otherwise}) \end{cases} \quad (5.11)$$

where TAE is in degrees. Before choosing MAX.CAP.BNK it is important to consider the following factors.

Recall from the earlier discussion of the "turn long" case that one must leave room for the bank to increase once the beam is encountered. The question is, "How much increase space is needed?" Figure 5-2 provides some insight.

Figure 5-2, based on Equation 5.1, shows (assuming a circular capture) CAP.BNK versus CTD with TAE as a parameter for a ground speed of 200 fps. For example, if a capture is begun at .5 nmi and TAE is 90°, then 22.3° of bank must be applied instantaneously and held through the turn. Consider, however, the situation when CTD from RNAV is in error by .2 nmi such that the capture in reality begins at .3 nmi instead of .5 nmi. The required instantaneous bank for this case is 34.3° to execute a no overshoot capture. Obviously, with a 30° bank command limit, this cannot be achieved. Further, the inclusion of rate command limits and inherent system lags will make this situation worse (i.e., bank cannot step instantaneously from 0° to CAP.BNK).

Two things are important here. First, the trip point should be such that .2 nmi errors do not cause the required CAP.BNK to exceed 30°. Secondly, the rate command limit turns out to be rather significant and the trip point should be moved to account for its effect. This is most simply done by noting that the approximate time required to build to CAP.BNK is

$$\text{Time-to-CAP.BNK} = \frac{\text{CAP.BNK}}{\text{RCL}}$$

where RCL is the bank rate command limit. Further the CTD traversed in this interval of time is (neglecting any turning in this interval)

$$\text{CTD.ADJ} = \frac{\text{CAP.BNK}}{\text{RCL}} * Vg \sin(\text{TAE}) \quad (5.12)$$

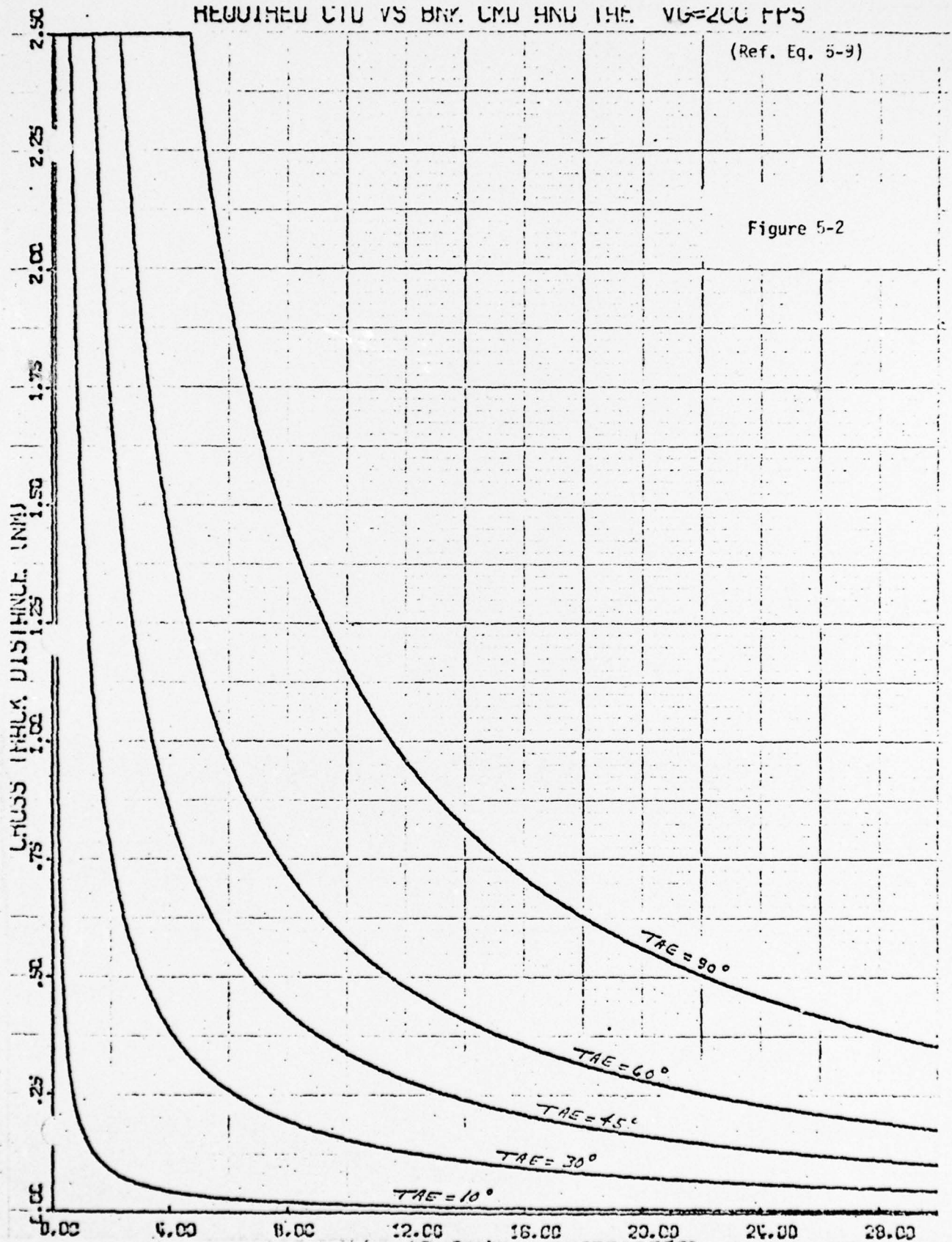
Hence the trip point as computed from Equation (5.10) should be incremented by Equation (5.12) with CAP.BNK determined from Equation (5.11). Figure 5-3 represents Figure 5-2 corrected by equation 5.12 to account for the time to build to the required capture bank. Given the value of CAP.BNK and TAE, therefore, the CAPTURE trip point may be read from Figure 5-3 for the case  $Vg = 200$  fps.

The only item as yet unresolved is MAX.CAP.BNK., the maximum bank to be used in capture which as shown in Equation 5.11 becomes one of the significant programming parameters on CAP.BNK. In the event one is doing an RNAV aided capture and the "turn long" case arises, the required "room to increase" on bank once the beam is encountered is a function of range. To see this, consider captures beginning at the same CTD and course cut but at varying range (RNAV data is used until beam intercept). Intuitively, the further out one is in range, the more beam width in feet is available after beam intercept to correct the problem or conversely less time is spent using an erroneous command.

REQUIRED LTD VS BRK LTD AND THE  $VG=200$  FPS

(Ref. Eq. 5-9)

Figure 5-2

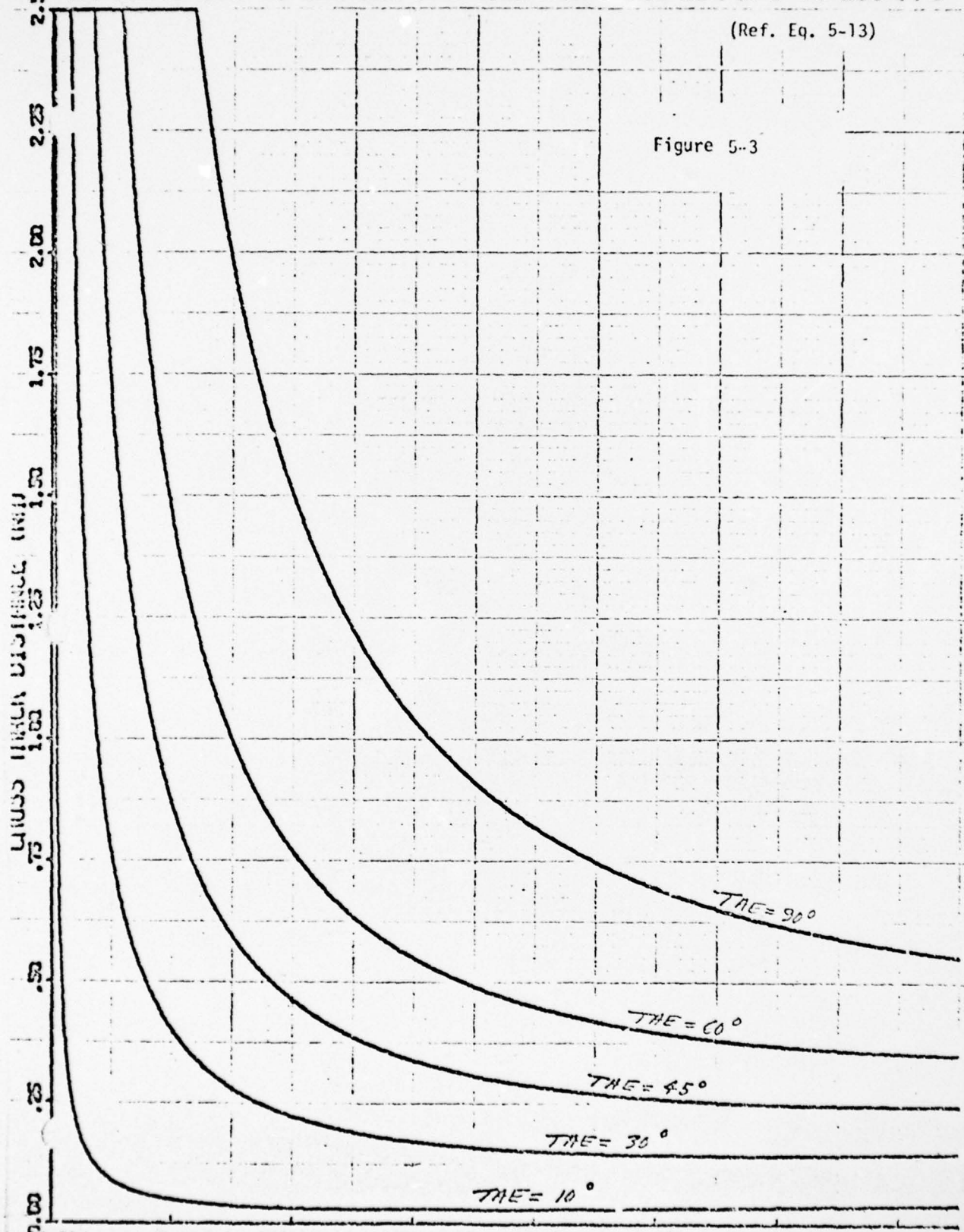




# REQUIRED CTD VS BNK CMD AND TAE..RATE CMD LHM AND VG=200 FPS

(Ref. Eq. 5-13)

Figure 5-3



For example, consider 90° captures at 5 nm and 8 nm respectively at a groundspeed of 200 fps and using -20° of bank in the capture. From Equation 5.2, if there are no errors, the respective track angle errors at the beam edge (TAEBE) should be

$$\text{TAEBE}_{8\text{nm}} = 70.25^\circ$$

$$\text{TAEBE}_{5\text{nm}} = 54.11^\circ$$

where a 200  $\mu\text{A}$  "beam edge" is assumed. Now in either case at 20° of constant bank the rate of turn is also constant and has the value

$$\dot{\psi} = \frac{g \tan \phi}{Vg} = -3.35^\circ/\text{sec}$$

Now if the trip point in each case is .2 nm late, the capture starts  $\tau_D$  seconds late where  $\tau_D$  is given by

$$\tau_D = \frac{.2 \text{ nm}}{200 \text{ fps}} = 6.076 \text{ sec.}$$

Therefore in each case  $\Delta\tau$  of heading change would be lost where

$$\Delta\psi = \tau_D * \dot{\psi} = 20.35^\circ$$

Hence the real TAEBE in each case is (adding  $\Delta\psi$  to the TAEBE values above)

$$\text{TAEBE}_{8\text{nm}} = 90^\circ$$

$$\text{TAEBE}_{5\text{nm}} = 74.46^\circ$$

Further, the respective cross track distances at the beam edge (CTDBE) are

$$\text{CTDBE}_{8\text{nm}} = .37 \text{ nm}$$

$$\text{CTDBE}_{5\text{nm}} = .23 \text{ nm}$$

Thus the required bank to complete the capture in each case is (from Equation 5.1)

$$\text{CAP.BNK}_{8\text{nm}} = -28.9^\circ$$

$$\text{CAP.BNK}_{5\text{nm}} = -33.1^\circ$$

Notice that for the capture at 8 nm with .2 nm of error in CTD,  $(28.9^\circ - 20.0^\circ) = 8.9^\circ$  of bank increase was required while at 5 nm  $(33.1^\circ - 20.0^\circ) = 13.1^\circ$  of bank increase was required. This example supports the contention that MAX.CAP.BNK should decrease as range decreases. Further, it is apparent and desirable that R-NAV aiding be used only when necessary.

If the trip point is within the beam, then capture will not begin until beam data is present. If MAX.BNK.CAP is made sufficiently large at longer ranges, it will force the capture to be within the beam in those cases (see Equation 5.10). It was decided to make MAX.CAP.BNK = 25° at longer ranges to insure localizer based captures there and to decrease the value at shorter ranges. From the example above, at 5 nm a bank increase of 13.1° was required in the "turn long" case while at 8 nm a bank increase of 8.9° was required. Further, it can be shown that for a 90° intercept at 200 fps, MAX.CAP.BNK = 25° implies R-NAV aided captures at ranges

shorter than 13 nm range; hence this seems a reasonable point to start programming MAX.CAP.BNK. down. Simulation results supported the 5 nm conclusions above and indicated that slightly more increase was required for the case of a 20% ground velocity error in the slow direction. For this reason, provision of about 15° possible increase at 5 nm seemed advisable. The resulting range program for MAX.CAP.BNK is

$$\text{MAX.CAP.BNK} = 8. + \frac{17.}{13.} * \text{RNGLOC} \quad (3.13)$$

where RNGLOC is range to localizer in nm and the units on MAX.CAP.BNK are degrees.

Collecting the above discussion, the trip point computation is performed as follows

$$\text{CTD Trip Point} = \frac{Vg^2(1-\text{COSTAE})}{9 \tan(\text{CAP.BNK})} + \text{CTD.ADJ} \quad (3.13a)$$

where

$$\text{CTD.ADJ} = \frac{\text{CAP.BNK}}{\text{RCL}} * Vg \sin(\text{TAE}) \quad (3.13b)$$

and

$$\text{CAP.BNK} = \begin{cases} -\text{MAX.CAP.BNK} * \frac{\text{TAE}}{90} \dots \text{if magnitude of result is } \geq 5^\circ \\ -5 * \text{SIGN}(\text{TAE}) \dots \text{otherwise} \end{cases} \quad (3.13c)$$

$$\text{and} \quad \text{MAX.CAP.BNK} = 8. + \frac{17}{13} * \text{RNGLOC} \leq 25^\circ \quad (3.13d)$$

CTD trip point as a function of range and course cut is shown in Figures 5-4 for a speed of 200 fps. Superimposed are lines for 200  $\mu$ A (ILS CAP "beam-edge") localizer deviation and "track trip". These are significant boundaries for they delineate NAVCAP, ILSCAP, and track regions respectively.\*

An alternate presentation of trip point information is shown in Figure 5-5. Here, for constant course cuts of 90 degrees, CTD trip point is plotted versus ground speed and range.

#### 5.3.4 Track Trip Point

The transition from capture to track normally occurs when

$$\text{LOCDEV} < 30 \mu\text{A for } \text{RNGLOC} \leq 13 \text{ nm}$$

and for

$$\text{LOCDEV} * \text{RNGLOC} < .091 \text{ nm for } \text{RNGLOC} > 13 \text{ nm}$$

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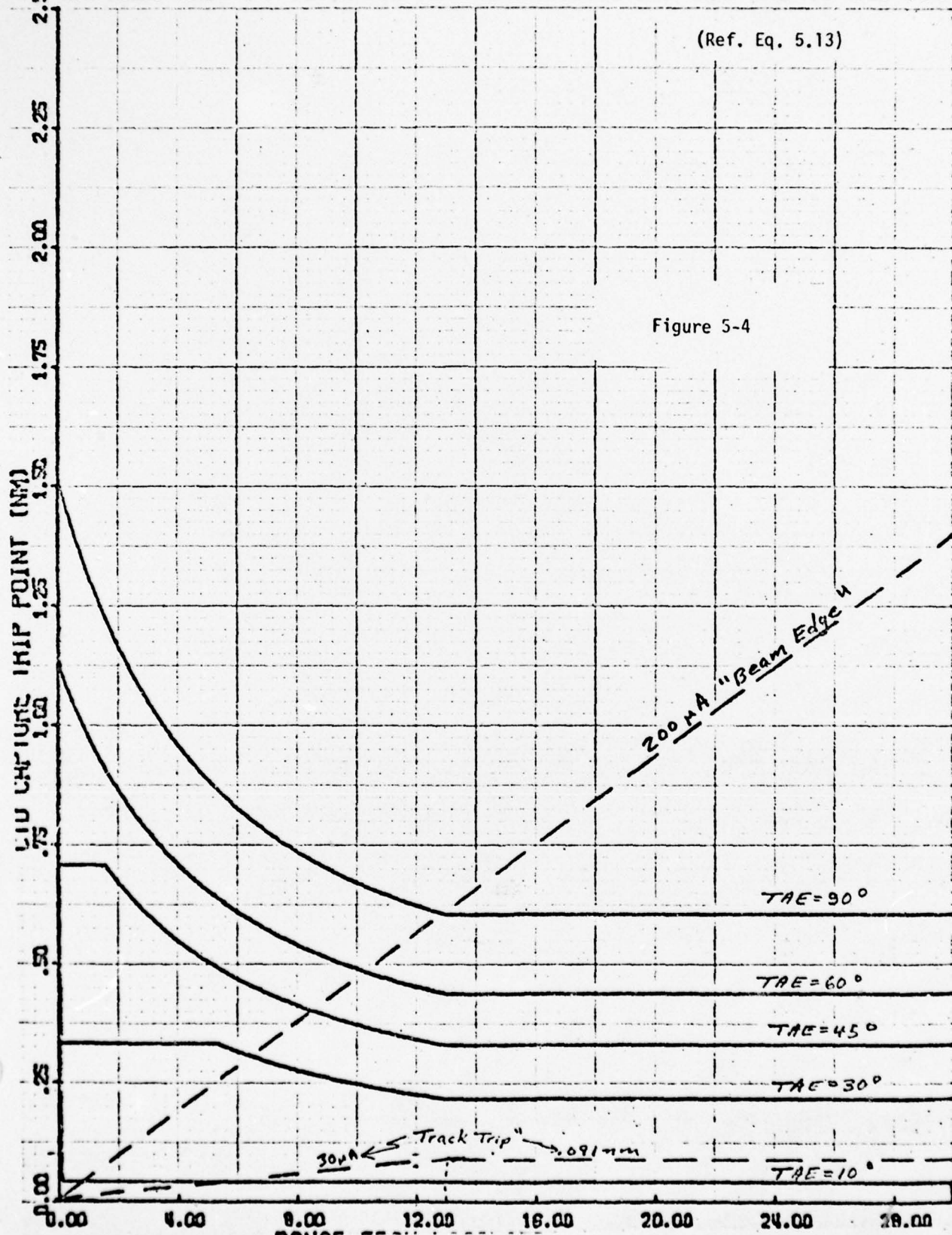
\*If the capture trip point lies within the "Track Trip" boundary, capture mode is deleted and the system transitions directly from heading mode to track mode.



# CAPTURE TRIP PT VS RANGE AND TAE...RATE CMD LIM AND VG=200 FPS

(Ref. Eq. 5.13)

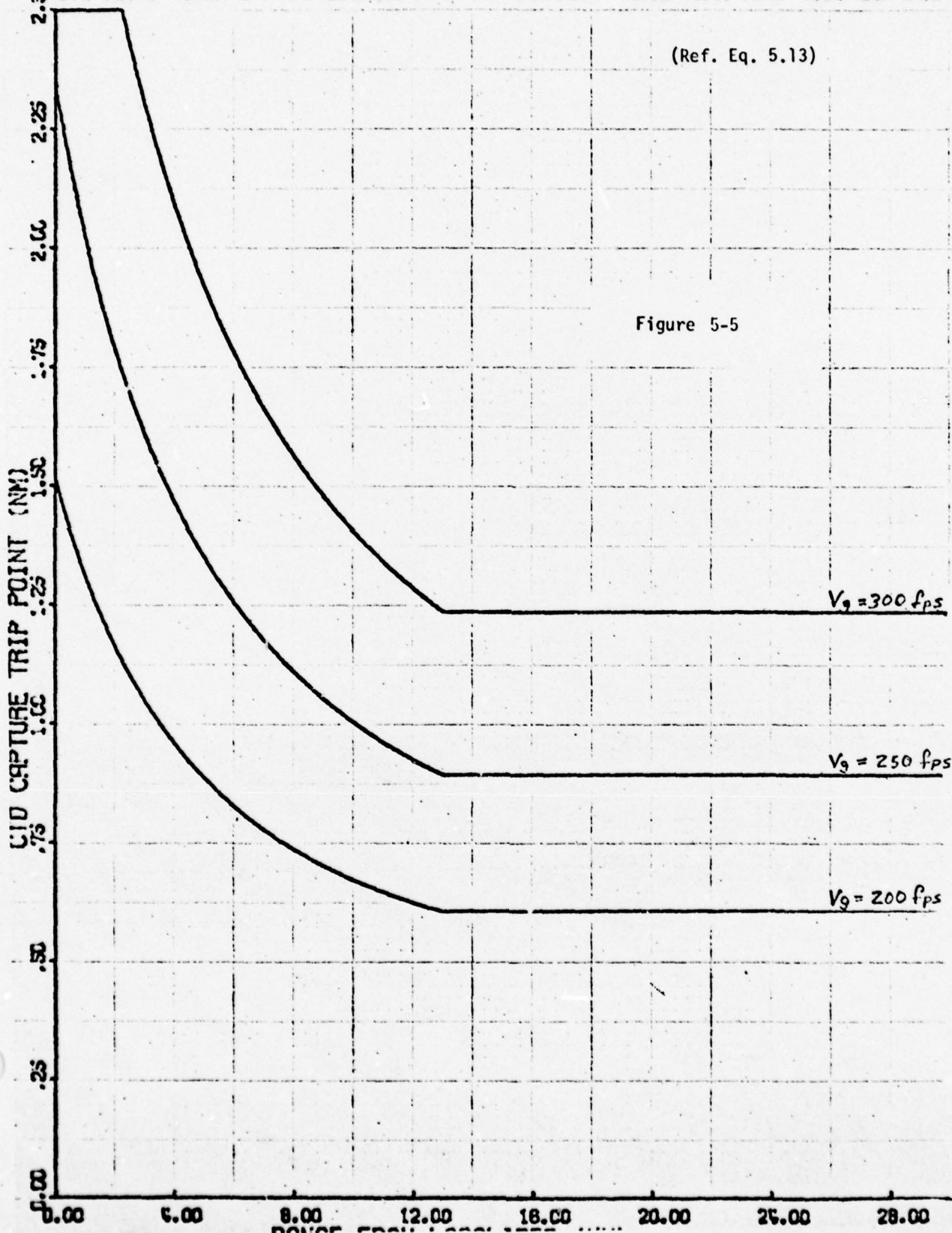
Figure 5-4



CAPTURE TRIP PT VS RANGE AND VG ... RATE CMD LIM AND TAE=90 DEG

(Ref. Eq. 5.13)

Figure 5-5



The transition from angular to linear CTD criterion for transition to track prevents going to track at high values of TAE at long ranges where 30  $\mu$ A represents significant linear deviation. The advantage here lies in maintaining capture mode and hence the circular nature of the capture as long as possible. However, in the event of severe crosswinds or unusually bad initialization the possibility of turning parallel to the beam during ILSCAP exists. To provide a final safeguard against turning parallel the following override trip to track feature is provided.

Since in ILSCAP the system is still performing a circular capture a slight derivative of Equation 5.2 for the TAEBE (track angle error at the beam edge) can be used to compute TAETRK (track angle error at track trip point).

$$\text{TAE TRK} = \cos^{-1} \left[ 1 - \frac{g \cdot \tan(-\text{BNKCMD}) \cdot \text{CTDTRK}}{v_g^2} \right] \quad (5.14)$$

where

$$\text{CTD TRK} = \begin{cases} \left( 30 \mu\text{A} \cdot \frac{\text{RNGLOC}}{(75)(57.3)} \right) \text{ nm, RNGLOC} \leq 13 \text{ nm} \\ .091 \text{ nm, RNGLOC} > 13 \text{ nm} \end{cases}$$

The system tests for ( $|\text{TAE}| < .9 \cdot \text{TAETRK}$ ), computing TAETRK via Equation 5.14; and if this condition occurs during ILSCAP, generates an override trip into the TRK mode. The flattening of the TAETRK curves at long ranges is due to the fixed CTD track trip point at ranges greater than 13 nmi. The flattening at short ranges is due to a bottom limit of 7° imposed on the computation (actually 7.73° on TAETRK so that  $.9 \cdot \text{TAETRK} > 7^\circ$ ) to ensure that this final test never drops below that value. That is, the system is constrained under all circumstances to go to track from ILSCAP if TAE drops less than 7 degrees.

### 5.3.5 Data Filtering

All of the foregoing discussion has neglected noise and lags on sensor data. In order for the conclusions and predictions above to be accurate, the data filtering, particularly on localizer data, must not introduce excessive lag. The often used system of about one second lag on radio and a complementary filter using radio and bank or heading to derive beam rate introduces lags that significantly compromise the performance of the system described here based on simulation results. For this reason a second order data filter for radio was developed which employs a bank input to provide complementing for both beam rate and position. With this filter, better performance in capture resulted and bank activity in track due to beam noise was very significantly decreased. This filter is described in detail in Reference 3 and performance is documented in Reference 4, hence it will not be discussed further here.



### 5.3.6 Mode Transition

As implied in the preceeding discussion, there are several distinct modes in the system that have evolved from this study. It is assumed that there is a heading select mode which is controlling the aircraft to a fixed heading (or course) prior to initiation of capture. Capture may be initiated either on R-NAV data or on beam data. In the former case, a blend-down submode may occur, and eventual transition to beam based capture must occur. Finally, a track mode assumes control once capture is completed. The transitions from mode to mode must be handled smoothly with no switching transients. The general mode switching smoothing technique is shown in Figure 5-6. The fade is basically a digitized exponential fade with 1 to 5 second time constants being typical.

### 5.3.7 Final System Description

#### Capture Modes

A block diagram of the total R-NAV aided ILS localizer capture and track system is shown in Figure 5-7. It should be noted that there are basically two potential capture modes. Capture computations are based on R-NAV data (NAVCAP) or based on ILS data (ILSCAP). Further there is a blend-down submode (BLNDWN) of NAVCAP which is provided to fade the bank command down in the "turn short" case. If R-NAV aiding is needed, the NAVCAP mode will occur first, transitioning to ILSCAP when localizer deviation becomes less than 200  $\mu$ A. If during NAVCAP the system turns too far [determined by continually comparing TAE with predicted TAE at the beam edge (TAEBE) during NAVCAP], the BLNDWN submode is automatically selected and fades the bank command according to the fade algorithm discussed in Section 5.3.2. ILSCAP can occur in two ways. First, if NAVCAP is in progress and localizer deviation decreases below 200  $\mu$ A, then ILSCAP is selected immediately. The other case occurs when the capture trip point is such that localizer deviation at that point will be less than 200  $\mu$ A. In this case no R-NAV aiding is needed and the ILSCAP mode is selected immediately. In terms of logic equations, the capture conditions may be expressed as

$$\text{NAVCAP} = [(\text{LOC DEV} > 200 \mu\text{A}) \cdot (\text{CTDNAV} < \text{CAPTRP})] \cdot (\text{RNGLOC} < \text{ILSLOK}) \quad (5.15)$$

$$\text{ILSCAP} = [(\text{LOCDEV} \leq 200 \mu\text{A}) \cdot (\text{NAVCAP} + (\text{CTDILS} < \text{CAPTRIP}))] \cdot (\text{DEVFLG}) \quad (5.16)$$

$$\text{BLNDWN} = \text{NAVCAP} : (|\text{TAE}| \leq |\text{TAEBE}|) \quad (5.17)$$

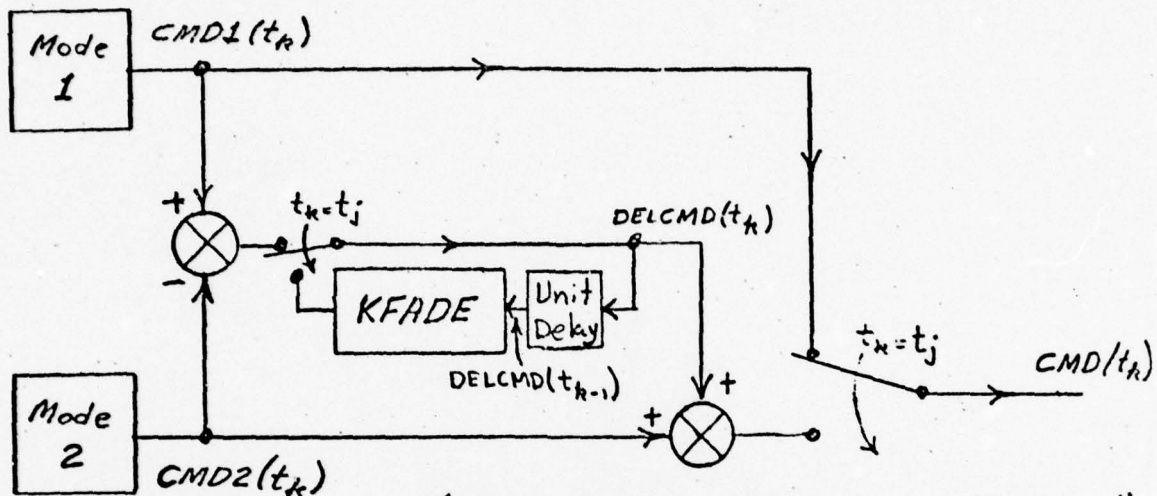
where ILSLOK and DEVFLG are added protections against R-NAV trip at excessive range due to CTDNAV errors and false ILSCAP trips due to decreasing LOCDEV at wide angle\* respectively.

#### False Trip Guards and Deviation Rate Limit

Both of these protections are shown in Figure 5-8. DEVFLG basically inhibits localizer computations at greater than a nominal deviation of 7° from the beam centerline. Seven degrees was chosen so that even with R-NAV errors the computed value will lie reliably between 4° and 10°.

---

\*Localizer signal strength in a +10 degree sector should be adequate to saturate the receiver but may drop off at wider angles.



( $t_k = kT$  where  $T$  is the sample period)

(Mode changes from Mode 1 to Mode 2 at time  $t_k = t_j$ )

$$KFADE = e^{-T/\tau}$$

1. For  $t_k < t_j$

$$CMD(t_k) = CMD1(t_k)$$

$$DELCMD(t_k) = CMD1(t_k) - CMD2(t_k)$$

2. At  $t_k = t_j$

$$DELCMD(t_j) = CMD1(t_j) - CMD2(t_j)$$

$$CMD(t_j) = CMD2(t_j) + DELCMD(t_j) = CMD1(t_j)$$

3. For  $t_k > t_j$

$$t_k - t_j = (k-j)T$$

$$DELCMD(t_k) = DELCMD(t_j) * (KFADE)^{(k-j)}$$

$$= DELCMD(t_j) * e^{-\frac{(t_k - t_j)}{\tau}}$$

$$CMD(t_k) = CMD2(t_k) + DELCMD(t_k)$$

4. For

$$(t_k - t_j) \gg \tau$$

$$CMD(t_k) \approx CMD2(t_k)$$

Figure 5-6. Smoothing Technique For Mode Switching (Digital System)

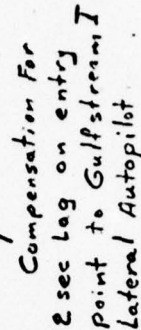


Figure 5-7a 30/40 Lateral Axis Control Laws

```

1. WMIN = 'LST-10' * 10 SEC.
2. KYOBLN = COS(TAE)
3. RNGPCM = { 1 if RNGLOC ≤ 7m
               7/RNGLOC if RNGLOC > 7m

```

4.  $\tau_{\phi} = 22.5 + 1.5 * R_{UGLO}$

5.  $RCL \geq 9\sqrt{\frac{\sigma^2}{n}}$  (See Fig 13).



30/40 Gulfstream I Inner Loops  
(SP20 Autopilot)

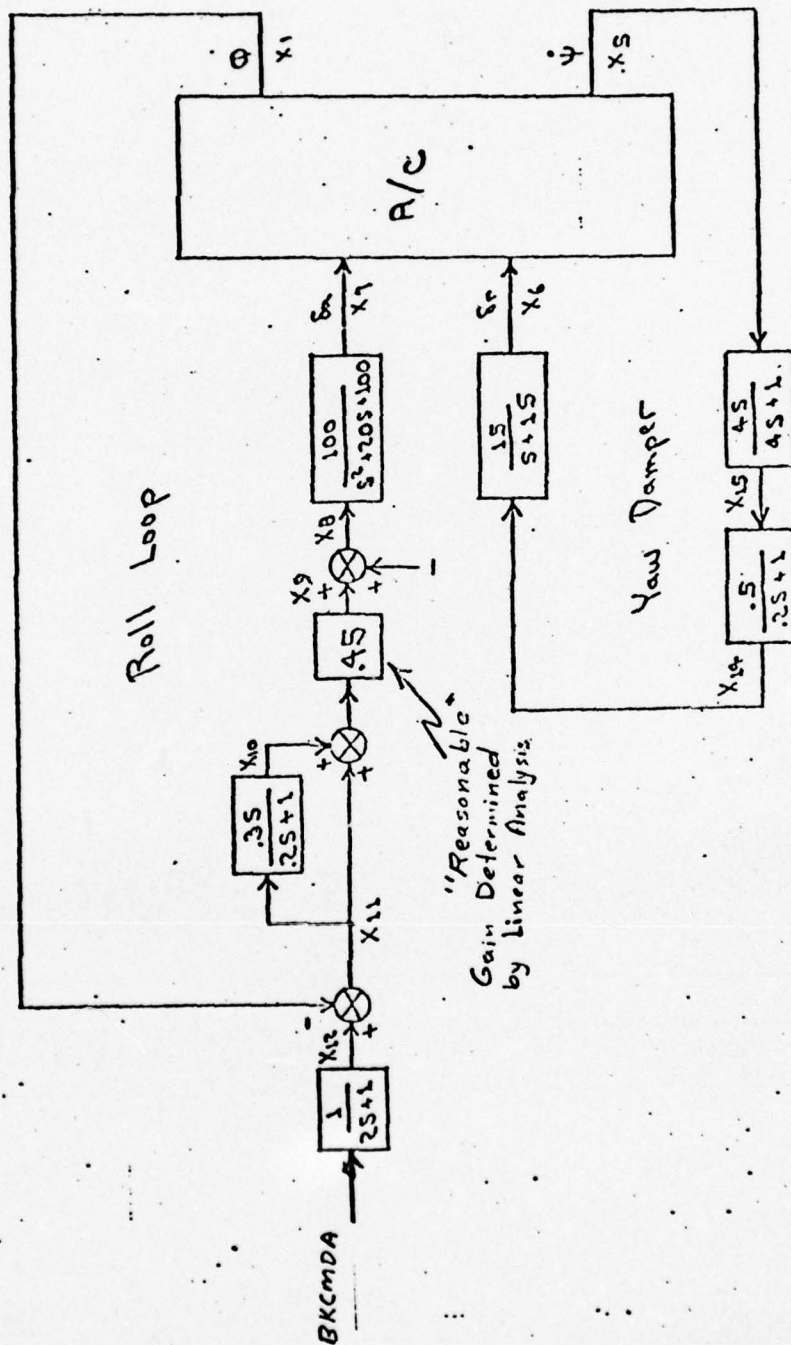
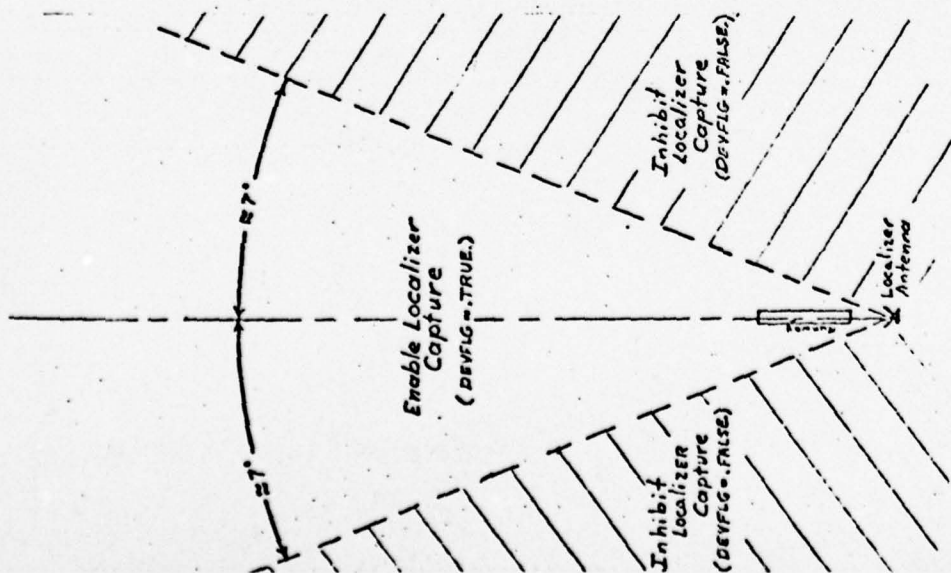
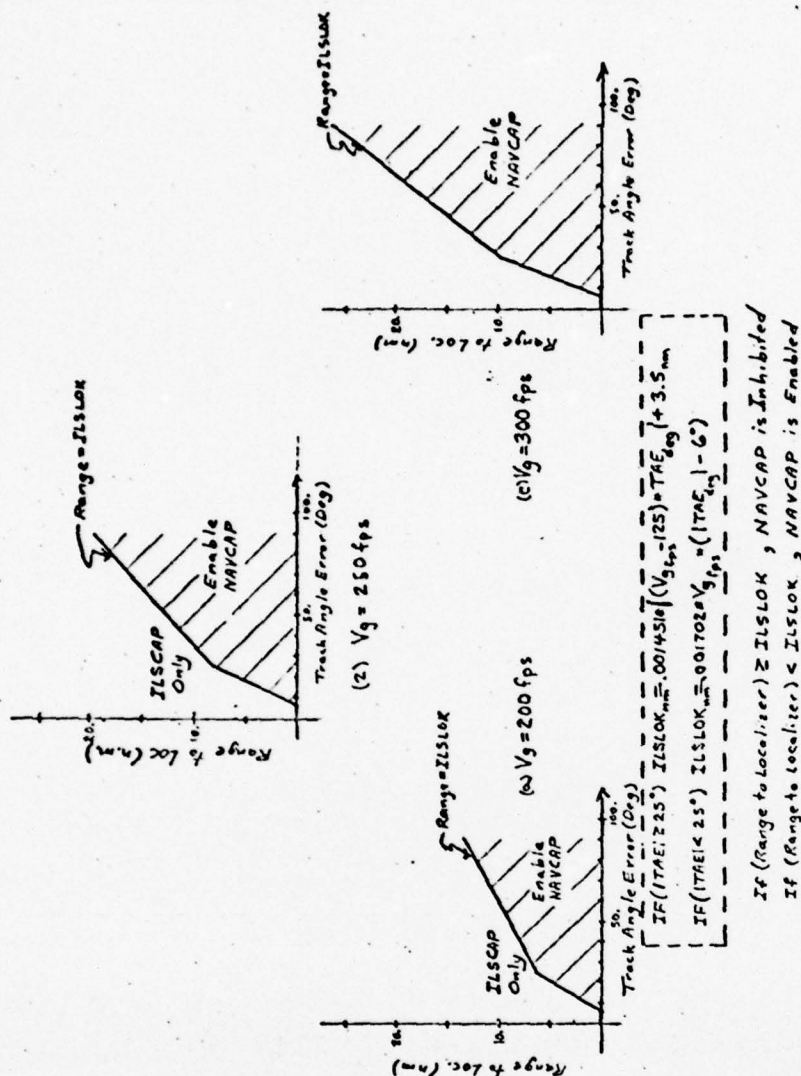


Figure 5-7b



(a) Guard Against Decreasing Localizer Deviation At Wide Angles



If (Range to Localizer)  $\geq$  ILSLOK, NAVCAP is Inhibited  
If (Range to Localizer)  $<$  ILSLOK, NAVCAP is Enabled

(b) Guard Against A-NV Aiding At Excessive Range Due to A-NV Cross-Track Distance Errors

Figure 5-8. Capture Trip Point Guards

ILSLOK basically inhibits NAVCAP if RNGLOC and TAE and VG data indicate that a non-R-NAV aided capture can be made. The only protection really is against early capture due to R-NAV CTD errors in regions where RNAV aiding is not needed. The equation for ILSLOK was generated by tabulating the ranges at which various TAE capture trip points intercept the beam edge (200  $\mu$ A) at 200, 250, and 300 fps and then curve fitting to this data. It should be noted that if LOCDEV  $> 200 \mu$ A, then CAPTRP is based on R-NAV data, but if LOCDEV  $\leq 200 \mu$ A, it is based on beam data. This feature is necessary to prevent R-NAV errors from corrupting the trip point of an ILS data only capture. To protect against decreasing LOCDEV at wide angles, DEVFLG, as discussed above, is used and to prevent false trips due to momentary interference as well as to guard against sudden transients a rate limit on LOCDEV is included. This rate limit is programmed with TAE and speed but lower limited at 9  $\mu$ A/sec under all conditions. Figure 5-9 shows the programming on the rate limit which is basically determined by dividing the cross track rate of the aircraft by range and then increasing this value by 30% to provide a conservative estimate of deviation rate.

#### Fade From NAVCAP to ILSCAP

Notice that during NAVCAP a fader circuit like the one of Figure 5-6 is prepared to fade from NAVCAP to ILSCAP when the need arises. Similarly during ILSCAP a companion fader stands ready to blend to the track mode. The bank command in either NAVCAP or ILSCAP is the proper one to generate a circular capture and both are essentially the same as Equation 5.1 although the form used in ILSCAP is modified to more appropriately use beam based data. This form is easily derived from Equation 5.1 which is repeated below

$$\text{BNK.CMD} = -\tan^{-1} \left( \frac{Vg^2 * (1 - \cos(\text{TAE}))}{g * \text{CTD}} \right) \quad (5.18)$$

Multiplying numerator and denominator of the arctan argument by  $(1 + \cos \text{TAE})$  and substituting  $\sin^2(\text{TAE})$  for  $1 - \cos^2(\text{TAE})$  in the numerator yields

$$\text{BNK.CMD} = -\tan^{-1} \frac{(Vg * \sin(\text{TAE}))^2}{g * \text{CTD} * (1 + \cos(\text{TAE}))}$$

But

$$Vg * \sin(\text{TAE}) = \text{Cross Track Rate (CTR)}$$

Hence

$$\text{BNK.CMD} = -\tan^{-1} \frac{(\text{CTR})^2}{g * (\text{CTD}) * (1 + \cos(\text{TAE}))} \quad (5.19)$$

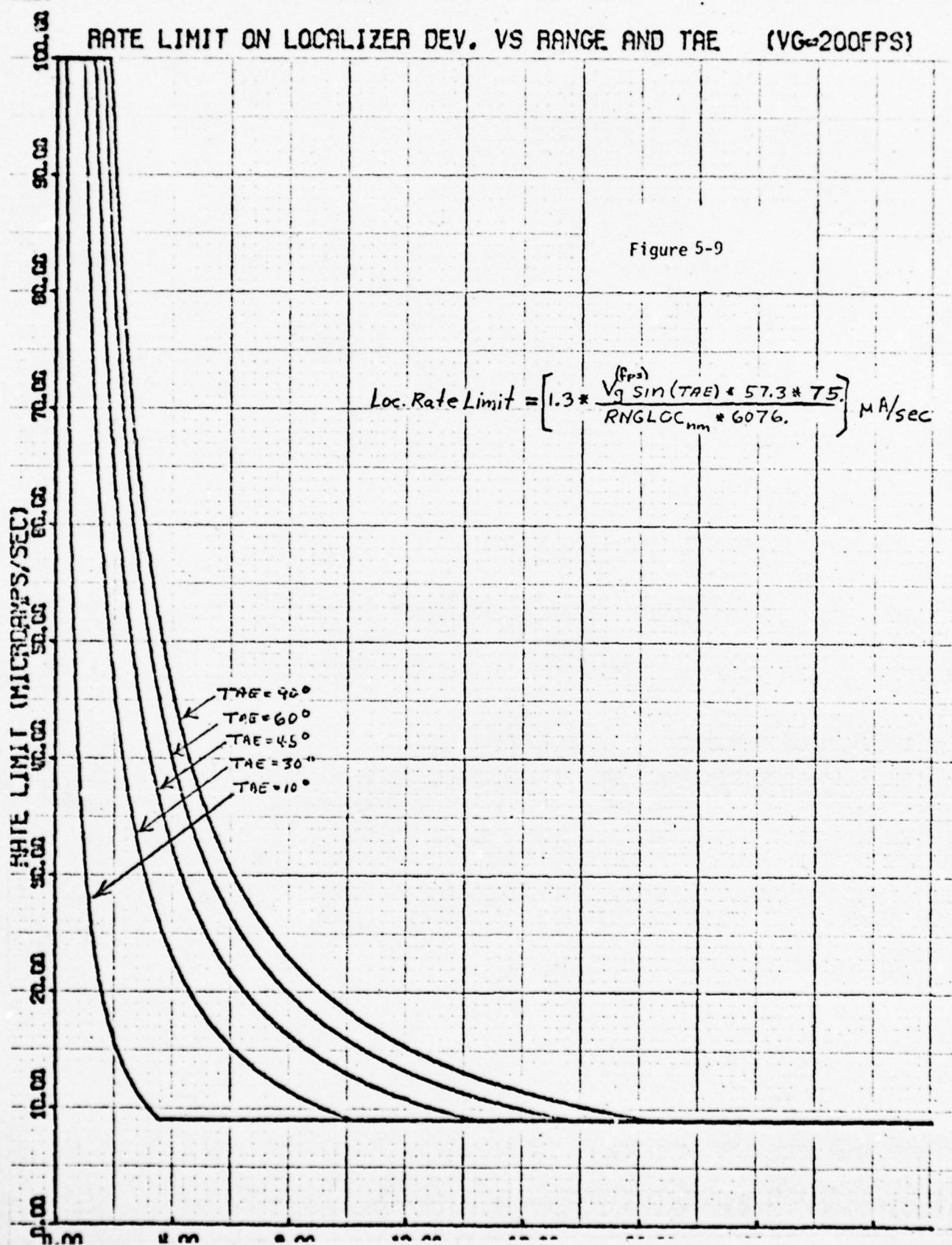
Equation (5.19) uses CTR as well as CTD explicitly and can thus make effective use of the beam data filter output. Groundspeed estimate errors will not influence Equation (5.18) directly and TAE errors will not have a large effect, particularly as the system approaches transition to track since as  $\text{TAE} \rightarrow 0$ ,  $\cos(\text{TAE}) \rightarrow 1$ , and  $(1 + \cos(\text{TAE})) \rightarrow 2$ . Thus, this term does not have the effect that it does in Equation (5.13), where



# RATE LIMIT ON LOCALIZER DEV. VS RANGE AND TAE (VG=200FPS)

Figure 5-9

$$\text{Loc. Rate Limit} = \left[ 1.3 * \frac{V_g^{(FPS)} \sin(TAE) * 57.3 * 75}{RNGLOC_{nm} * 6076} \right] \text{ mA/sec}$$



$(1 - \cos(\text{TAE})) \rightarrow 0$  as  $\text{TAE} \rightarrow 0$ . The form of Equation 5.19 is no better than that of 5.18 in NAVCAP, however, since in NAVCAP,  $\text{CTR} = -V_g \sin(\text{TAE})$  which simply would bring back TAE in a different form.

#### Track Mode

The track mode is a conventional proportional combination of position and rate relative to the beam center to form bank command. The trip point for going to track mode was discussed in Section 5.3.4. Track gains are given in Table 5-2 in several different forms for ease of correlation with other work. A stability analysis of the track mode appears in Section 5.4.

	Range < 7 nm	Range $\geq$ 7 nm	Range = 8 nm
Gain on Position	$\left(\frac{3.2}{70} = .046\right) \frac{\text{deg}}{\text{ft}}$ or $\left(\frac{1}{279.5}\right) \frac{\text{deg}}{\text{nm}}$	$(.45) \frac{\text{deg}}{\mu\text{A}}$ or $(13.6) \frac{\text{deg}}{\text{dot}}$	$(.45) \frac{\text{deg}}{\mu\text{A}}$ or $(13.6) \frac{\text{deg}}{\text{dot}}$
Gain on Rate	$\left(\frac{35}{70} = .5\right) \frac{\text{deg}}{\text{fps}}$ or $(.844) \frac{\text{deg}}{\text{kt}}$	$.5 * \frac{7}{\text{RNGLOC}} \frac{\text{deg}}{\text{fps}}$ or $\left(.844 * \frac{7}{\text{RNGLOC}}\right) \frac{\text{deg}}{\text{kt}}$	$(.438) \frac{\text{deg}}{\text{fps}}$ or $(.739) \frac{\text{deg}}{\text{kt}}$

Table 5-2. Rate & Position Gains for Track Mode

Notice that the output of the data processing filter is position and position rate to provide the requisite data to the capture computations. This is also the appropriate form for the track mode at close ranges. However, at longer ranges the effects of beam noise, particularly excessive bank activity, require that gains be softened, usually such that the track law becomes angularly based rather than position based. The RNGPGM block of Figure 5-7 may be seen to provide this feature since at ranges beyond 7 nm (neglecting the filter for the moment since its parameters are not range dependent),

$$\text{CTDTRK} = \frac{7}{\text{RNGLOC}} * \text{RNGLOC} * \text{LOCDEV}$$

$$\text{CTDTRK} = 7 * \text{LOCDEV} \quad (5.20)$$

Equation 5.20 shows that CTDTRK beyond 7 nm is really in angular units with the 7 being the required factor for blending properly with the linearized portion. Alternately, the combination of RNGPGM programming downstream of the filter and RNGLOC programming of LOCDEV upstream of the filter provides linearization of LOCDEV out to 7 nm and a constant gain beyond that range. The rate is treated similarly to take care of the radio contribution to rate. There is no real necessity to program the bank

contribution to rate and in fact stability would be aided by not doing so. However, in order to maintain system simplicity, no separate provision was made for bank contributed rate.

#### Data Processing

The data processing portion of the block diagram consists primarily of a double complementing filter (DCF) as described in Reference 3. Since in this application roll or bank is used for generating acceleration, it is termed the roll radio double complementing filter (RRDCF). The proportional combination of RRDCF rate and R-NAV based rate using the function KYDBLN provides slightly improved rate for capture. The basic idea here is that although bank provides information about acceleration orthogonal to the aircraft fuselage reference line, the RRDCF filter requires acceleration relative to the beam centerline. Hence bank is processed as

$$\ddot{y}_{\phi} = -g \tan(\phi) \cos(\text{TAE})$$

At high course cuts, therefore, bank does not provide very good information about acceleration relative to the beam. The necessity of complementing RRDCF filter rate against R-NAV rate in capture is not firmly established. R-NAV rate is used to initialize RRDCF and low frequency updates by radio rate might then provide sufficiently good rate. The function used for KYDBLN is  $\cos(\text{TAE})$  so that as the system turns onto the final course, the influence of R-NAV rate is removed. A washout on bank is used during track to prevent beam tracking standoff due to bank bias.

#### Output Command Processing

The final aspect of the system block diagram is the output command processing shown at the right side of Figure 5-7a. Basically a 5 degree per second rate command limit and a 30 degree command limit are imposed. The lead-lag compensation is necessary for the specific Gulfstream I autopilot interface provided for in this application. The system interface to the Sperry SP40 autopilot interposes a 2 second lag between the available heading error port and the bank command summing point. Figure 11b shows the equivalent block diagram of the SP40 autopilot. It should be noted that this is a somewhat sluggish autopilot having particularly large servo lags. This factor necessitates running somewhat lower outer loop gains than one might prefer in approach.

### 5.3.8 Software Organization

The basic software organization required to implement the system described above is shown in Figure 5-10. The localizer capture and track computation are a submode to the ILS main program which interfaces with the R-NAV main software. The chosen approach is to process the data in one software block, determine the proper mode in another, and then perform control computations based on the determined mode. Finally, the output control processing does the rate and amplitude command limiting and the lead-lag compensation as shown in Figure 5-7a. A more detailed block diagram is provided in Figure 5-11. The program listing is given in Appendix F.



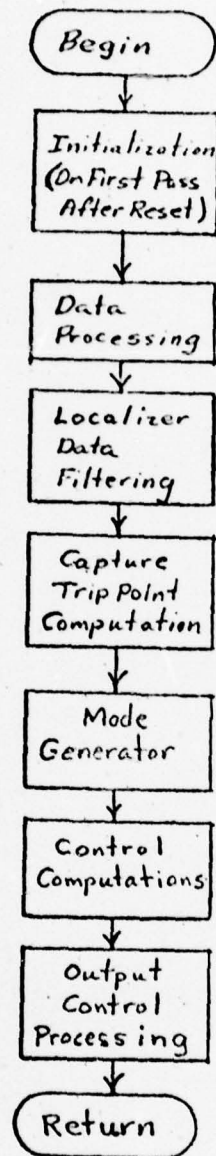
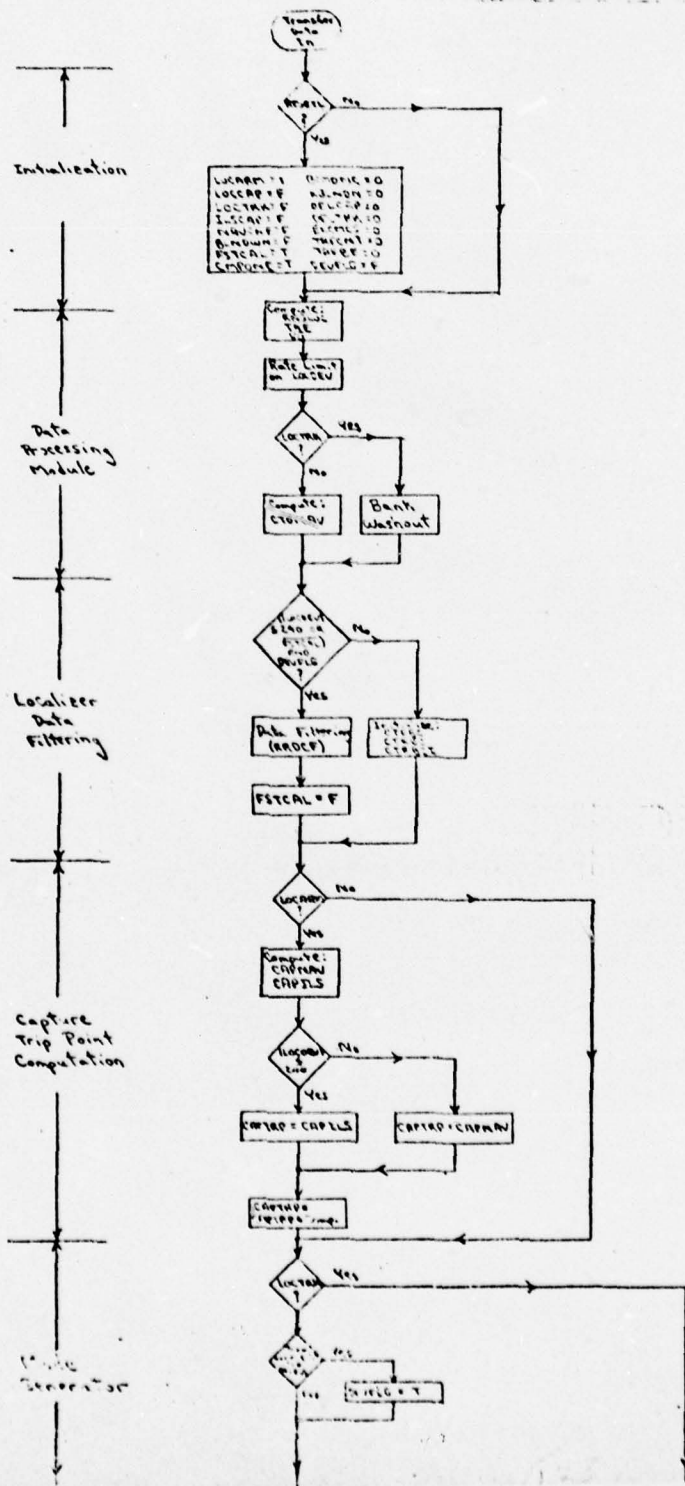
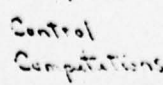


Figure 5-10. Basic Software Organization  
Lateral Computational Module

Figure 5-11. Detailed Lateral Flow Chart  
Section 1 out of 3









## Stability Analysis of the 3D/4D Lateral ILS Localizer Track Laws

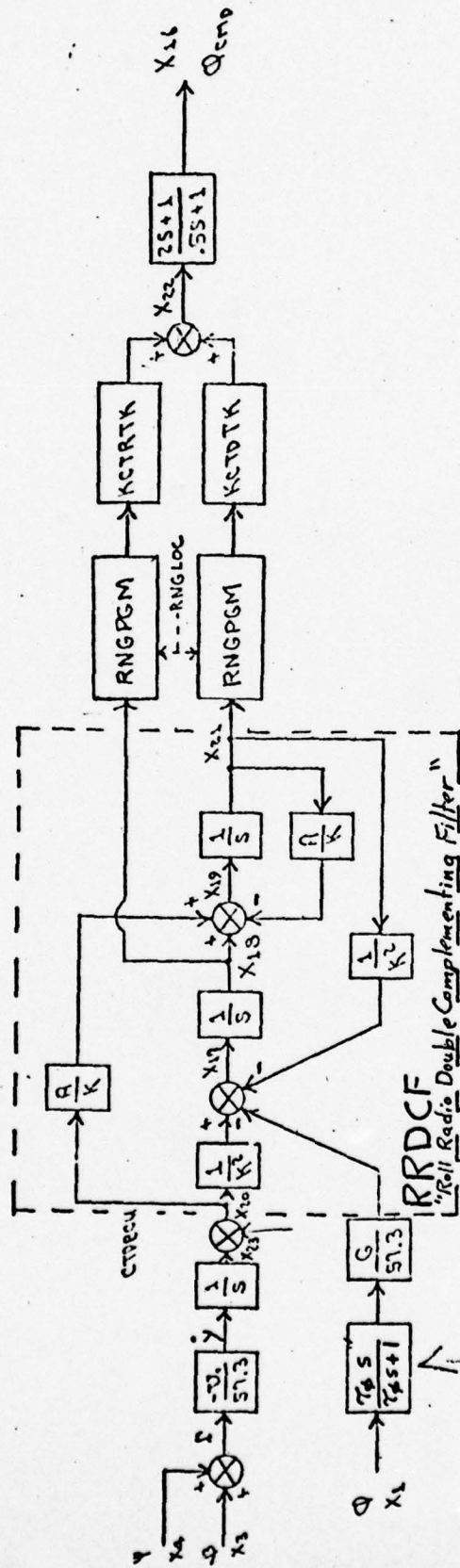
Figure 5-12 shows a block diagram of the track control laws from sensor inputs to bank command while Figure 5-13 shows the block diagram for autopilot and aircraft. (Note the rather sluggish aileron servo.) From Reference 3 the pole-zero parameter A in the RRDCF filter (see Figure 5-12) was set at 2 with the bandwidth parameter K fading from 3.036 (the capture value) to 10 once track was well established. Stability and PSD data was therefore computed for both extreme values of K recognizing that the results for K=3.036 will be applicable early in track while those for K=10.0 apply for well established track. Loops were broken at radio and at bank command. The loop at radio plots must be interpreted carefully particularly for K=10, because the complementing effect of the bank feed through to position (see Reference 3) permits somewhat lower than conventional bandwidths in the radio loop.

The system was linearized (RNGPGM) only to 7 nm from the localizer antenna since linearizing further produced excessive bank activity.

At long ranges, therefore, the bandwidth of the system both at radio and bank command decreases considerably ( $-20 \log \left( \frac{7 \text{ nm}}{25 \text{ nm}} \right) = -11.06 \text{ db}$ ). Stability was checked carefully, therefore, at the assumed extreme range of 25 nm. Figures 5-14 to 5-17 show gain/phase plots for loops broken at radio and bank command for K=3.036 and K=10 respectively, all at 25 nm. Note on Figures 5.14 and 5-15 the phase dip below  $180^\circ$  at low frequency. This dip is due to the bank washout shown in Figure 5-12. The magnitude of the dip is greater for shorter than for longer washout time constants. For this reason a 60 second washout is used at 25 nm programmed down to 30 seconds at 50 nm. The long washout at near range is undesirable due to the long charging time required to remove bank biases which are more troublesome at near than at far ranges. Bank biases, if not washed out, result in both position and rate biases out of RRDCF (see Reference 3). Table 5-3 tabulates the stability margin and crossover data from Figures 5-14 through 5-17. Also shown in Table 5-3 is the analogous data for 5 nm range.

Range	W/O Time Const.	K	RNGPGM* KCTDTK deg/ft	RNGPGM* KCTRTK deg/fps	Loop at Radio			Loop at Bank Cmd		
					Wc.o.	P.M.	G.M.	Wc.o.	P.M.	G.M.
25 nm	60	3.036	$7 \left( \frac{3.2}{25} \right) \left( \frac{35}{70} \right)$	$7 \left( \frac{35}{25} \right) \left( \frac{35}{70} \right)$	.092	25°	11	.101	38°	24
25 nm	60	10.0	$7 \left( \frac{3.2}{25} \right) \left( \frac{35}{70} \right)$	$7 \left( \frac{35}{25} \right) \left( \frac{35}{70} \right)$	.070	20°	7	.092	42°	24
<7 nm	30	3.036	$\left( \frac{3.2}{70} \right)$	$\left( \frac{35}{70} \right)$	.155	31°	8	.26	57°	13
<7 nm	30	10.0	$\left( \frac{3.2}{70} \right)$	$\left( \frac{35}{70} \right)$	.09	24°	10	.295	60°	13

Table 5-3. Stability Margins



$$\text{RNGPGM} = \begin{cases} 1 & \text{if } \text{RNGLOC} < 7\text{nm} \\ \frac{1}{\text{RNGLOC}} & \text{if } \text{RNGLOC} > 7\text{nm} \end{cases}$$

$$\begin{aligned} \text{KCTDTK} &= .0(4/10) = .0457 \\ \text{KCTRTK} &= (35/10) = .50 \\ A &= 2.0 \\ K &= 3.036 \\ U_0 &= 200 \end{aligned}$$

$$\tau_\phi = (22.5 + 1.5 * \text{RNGLOC}_{\text{nm}}) \text{sec}$$

Figure 5-12. 3D.4D Track Laws



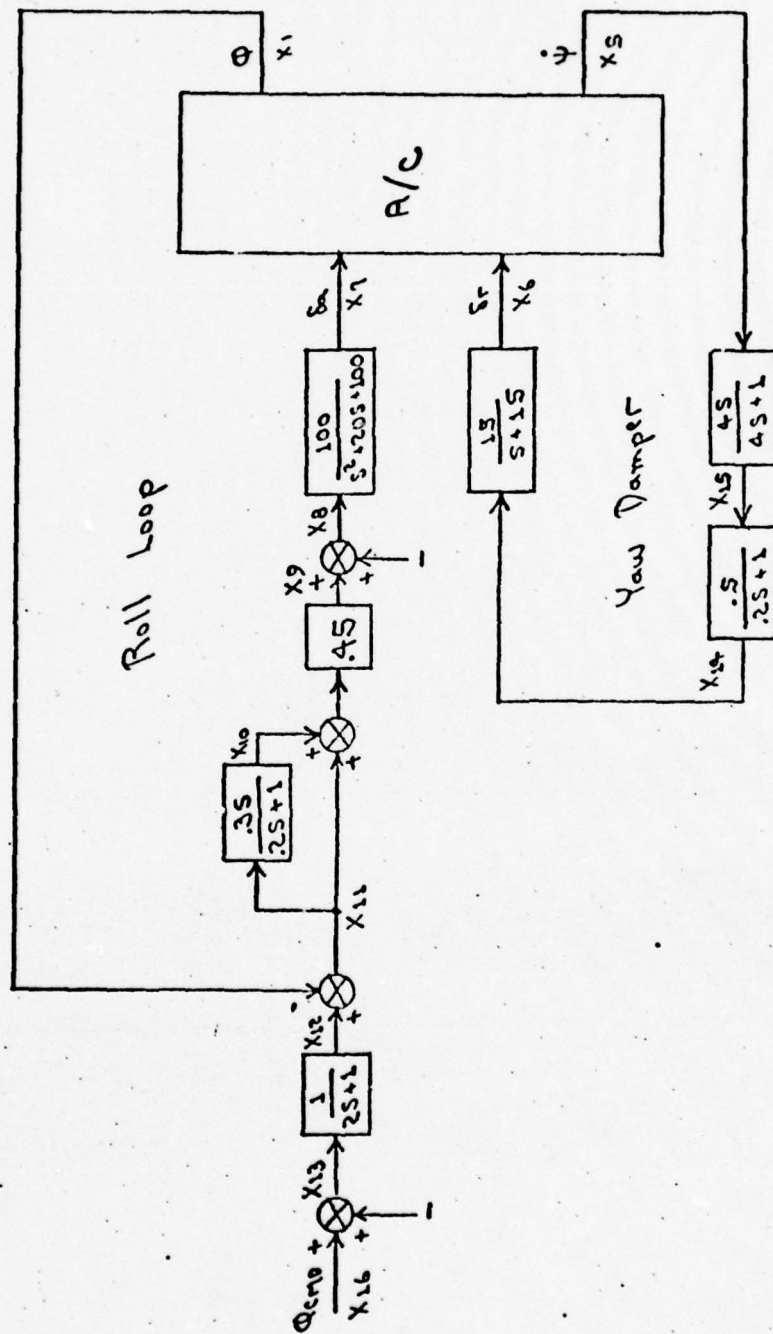


Figure 5-13. Gulfstream I Inner Loops

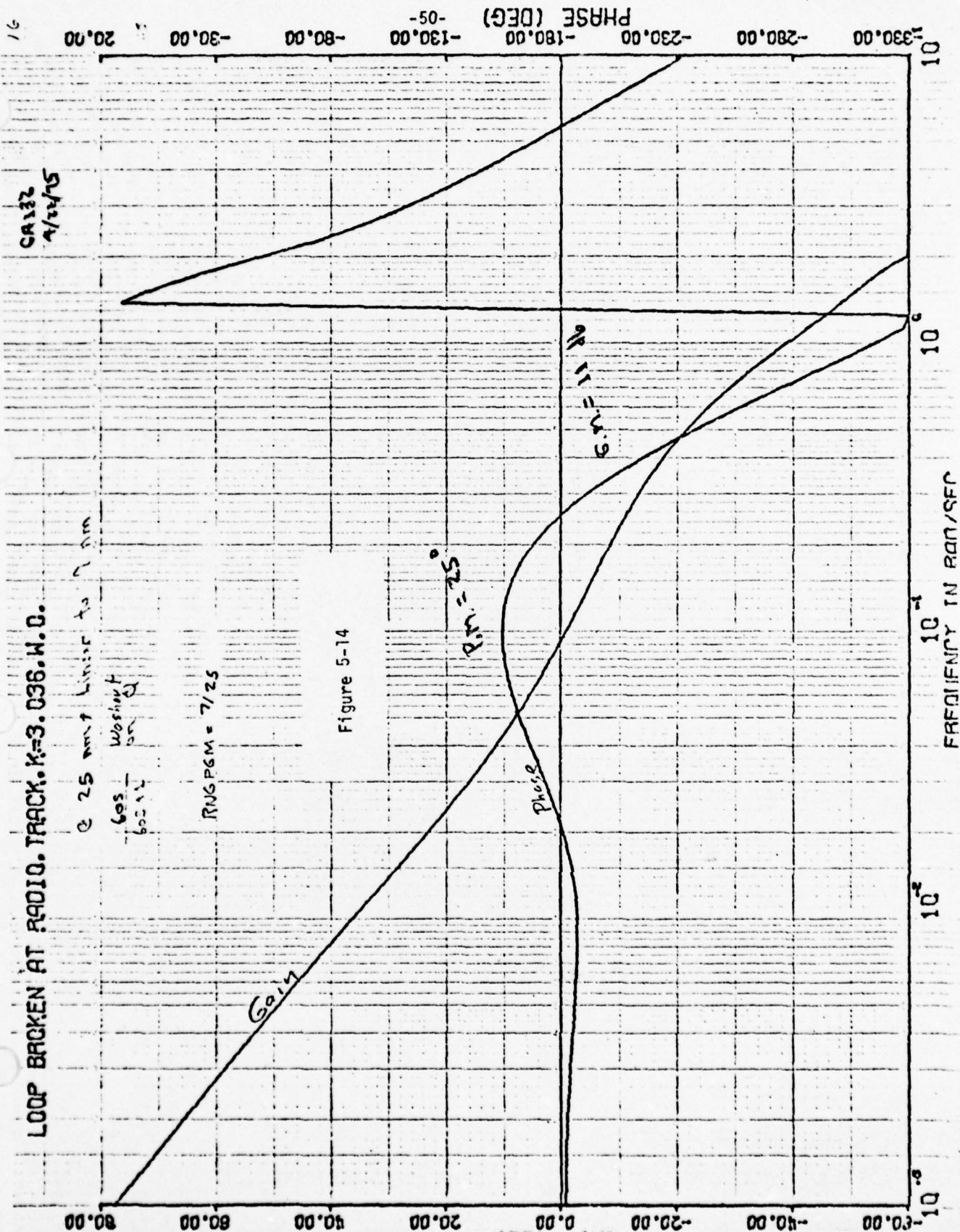
LOOP BACKEN AT RADIO. TRACK. K=3.036. H.O.

Q 25 mmf limit to 7 mm

603 - Washburn  
605 12

RNG PGM = 7/25

Figure 5-14

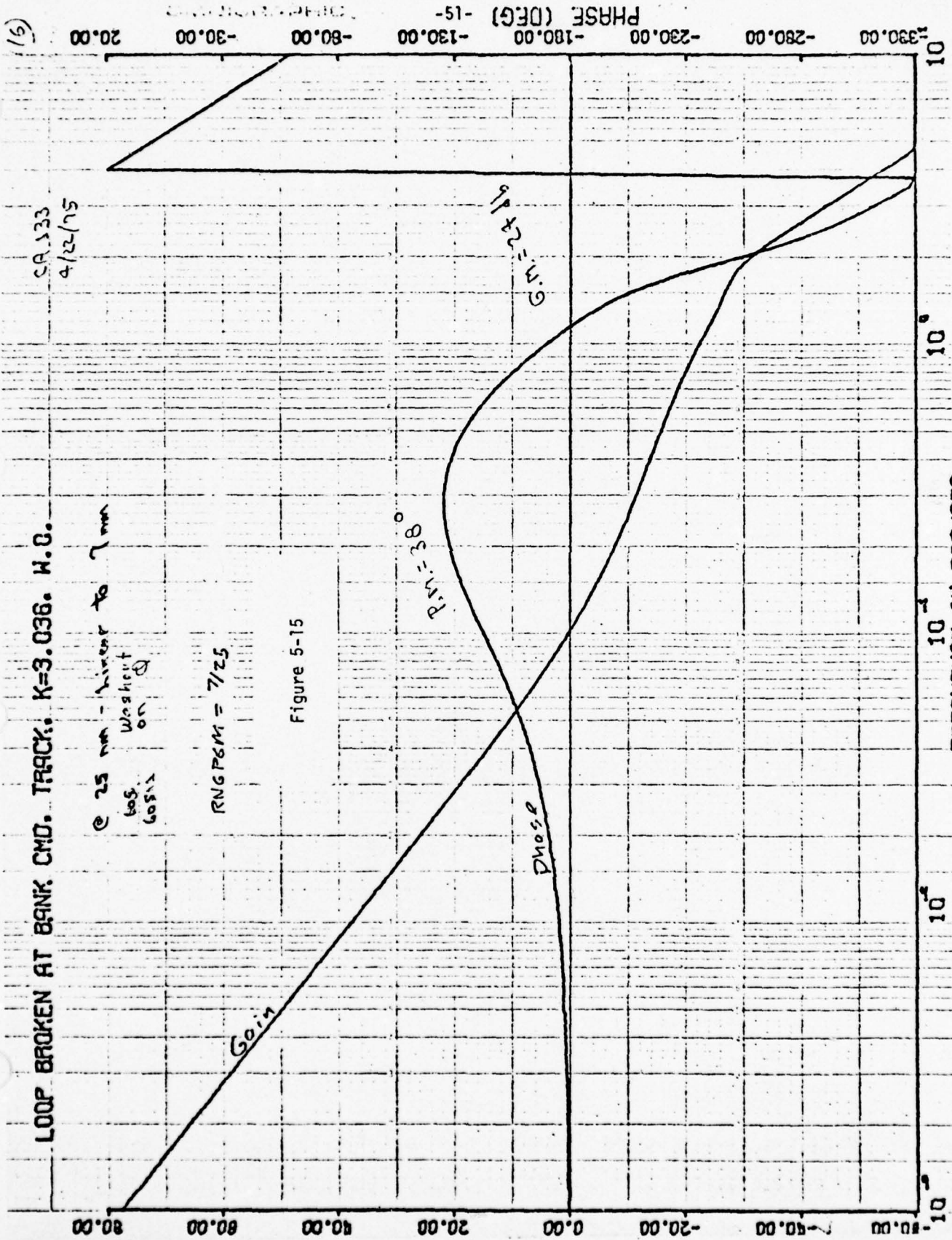


LOOP BROKEN AT BANK CMD. TRACK. K=3.036. W.O.

@ 25 mm - direct to 7 mm  
605. Washout on 605.2

RNGP6M = 7/25

Figure 5-15



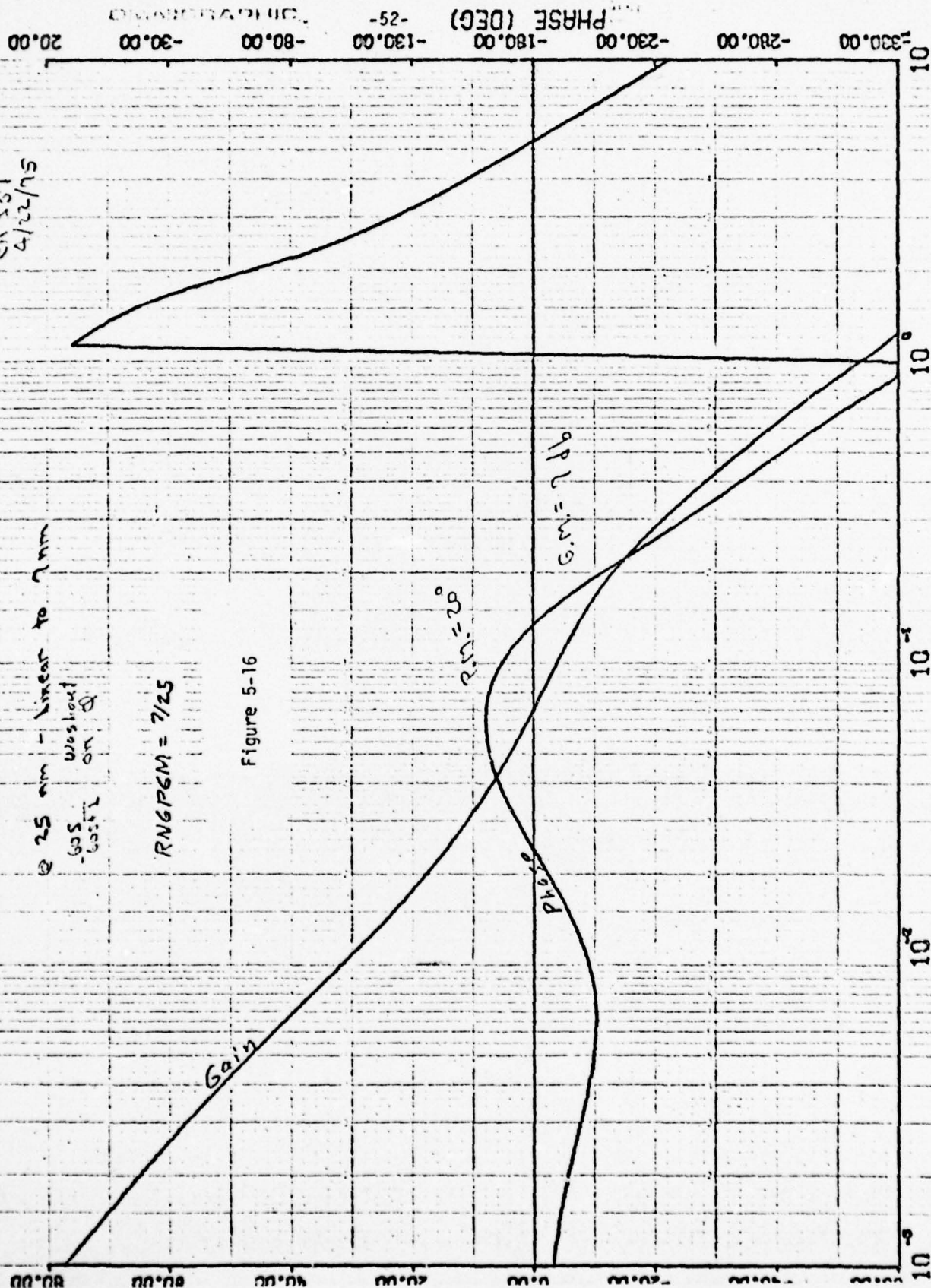


LOOP BROKEN AT RADIO. TRACK. K=10...W.O.

@ 25 mm - linear to 7mm  
-60S without  
-60S on 0

RNGPEM = 7/25

Figure 5-16

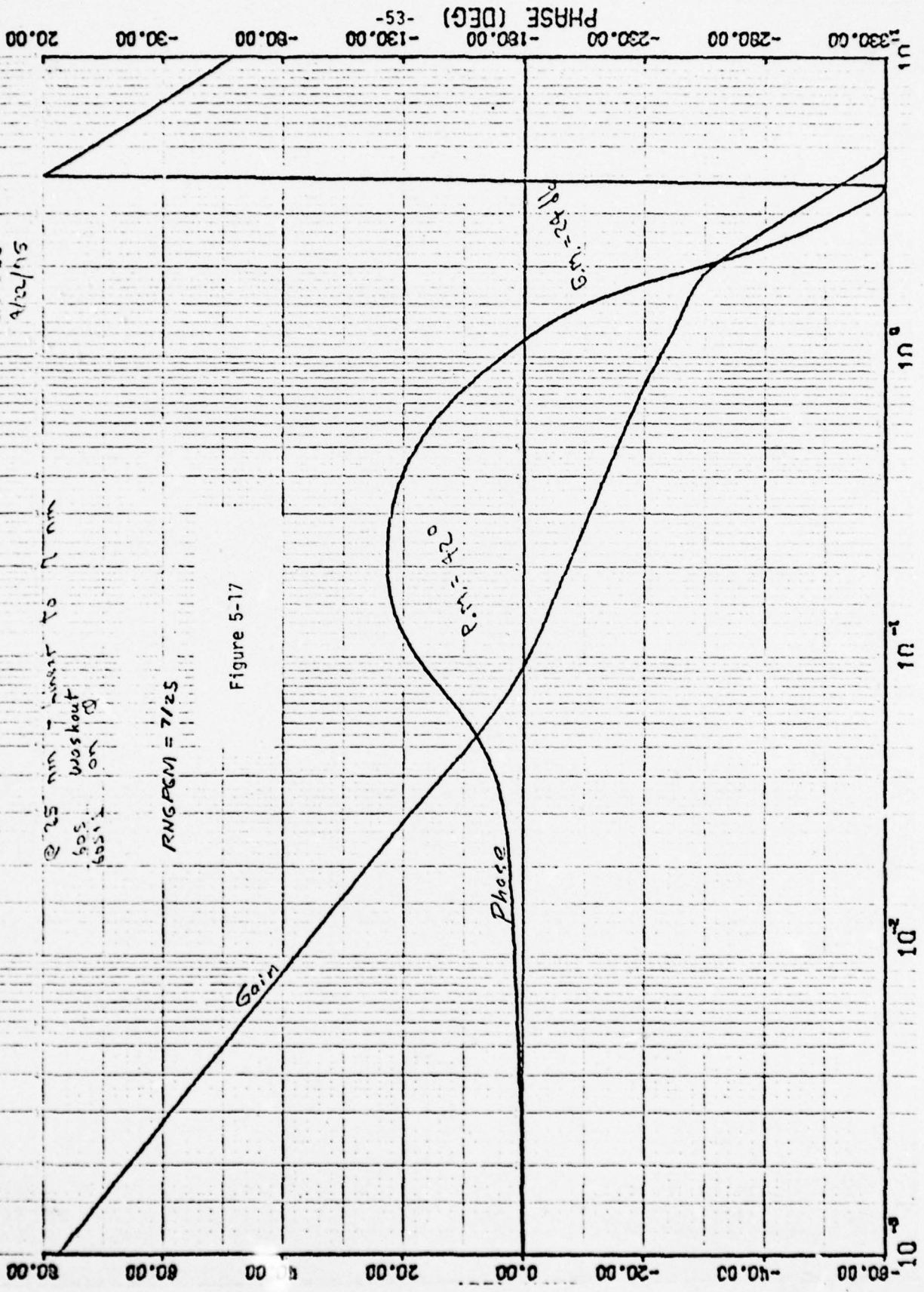


LOOP BROKEN AT BANK CMD. TRACK. K=10.. H.O.

@ 25 mm - limit to 7 mm  
 60% Washout  
 60% on 10

RNG PCM = 7125

Figure 5-17



Section 6  
LONGITUDINAL ILS CONTROL  
LAW DESIGN AND ANALYSIS

6.1 INTRODUCTION

The glideslope portion of the ILS approach control laws are presented by this report. The control laws provide for a smooth, transientless capture of the glideslope beam. The control laws will automatically adapt for varying airspeed, wind and beam angles. In addition, both above and below the beam intercepts can be accommodated.

The control laws developed rely upon derived vertical rate to enhance the adaptive capture capabilities and to supplement basic autopilot and flight director path dampening and gust alleviation. The autopilot and flight director both accept pitch commands from the glideslope control laws in the 3D/4D processor to an altitude hold port. Once attitude is closed in a glideslope control loop, it has been found that vertical rate is of some benefit for gust alleviation, but it cannot be used to its fullest advantage. The control laws, therefore, have some advantages over conventional pitch implemented controls while exhibiting similar tracking performance.

A description of the glideslope computations, stability and performance analyses are contained herein. The glideslope control laws digital program listing is contained in Appendix G.

6.2 GLIDESLOPE OPERATION AND DESCRIPTION

Glideslope control laws are provided for vertical navigation of an RNAV/ILS approach capability. An adaptive capture capability has been designed into the glideslope control laws. The control laws are illustrated in Figure 6-1.

Glideslope operation is performed with the 3D/4D system just as is done with any conventional flight guidance computer. Basically glideslope capture is initiated from a flight path which has been set up to intercept the glideslope beam. Most often the glideslope is intercepted from a zero





flight path angle or altitude hold maneuver. Unlike some glideslope operations the control laws in the 3D/4D system will also allow the user to capture from above.

Operationally, glideslope capture and tracking can be accomplished in the approach auto mode (APPR AUTO) of the ILS portion of the 3D/4D system. Once an intercept has been established so that the aircraft will intercept the glideslope beam, capture is completely automatic. The system compares beam and vertical rates with beam deviation and polarity to establish a capture trip point. Figure 6-1 also includes the capture logic which dictates when capture occurs. When pitch command is sensed to go through zero in the correct direction as determined by comparing its polarity with that of beam deviation, capture is initiated.

Since the capture is a function of both beam closure rate and vertical rate, capture is a function of ground speed and flight path angle. Ground speed in turn makes the capture a function of aircraft speed and wind. If a capture is initiated from altitude hold, the capture trip point will vary as a function of how fast the glideslope beam is approached. The trip point will move further from the glideslope beam center as the closure rate increases no matter what reason. Similarly, if the aircraft has a vertical rate established, capture will be adjusted to compensate for the vertical rate. As an example, when capturing from above, capture will be initiated further from the glideslope for a greater vertical rate or flight path intercept. Of course, beam rate alone can also sense this higher closure rate, but the addition of vertical rate has proved to be more accurate in adjusting the trip point especially in above the beam captures.

Once capture has been initiated, the beam rate is held by a track/store operation. Also notice that at the instant of capture a fader or washout is initiated on both stored beam rate and vertical rate. The action is such that at the instant of capture, pitch command is zero, and the aircraft proceeds toward the glideslope beam. Deviation therefore decreases while the rate signals (which are being slowly faded out) provide a nose up or nose down pitch command, whichever is appropriate to transition the aircraft to the glideslope path. The fader washes out all of the beam rate and initial vertical rate as the aircraft acquires the beam centerline. In this manner the control laws smoothly and transientlessly transition the aircraft from its intercept flight path to the beam center.

After capture, tracking is provided by glideslope deviation and washed out vertical rate. The capture bias provided by the stored beam rate is completely removed. Vertical rate is washed out to prevent the vertical rate or descent rate from causing a deviation standoff in the control laws.

The control laws developed for the 3D/4D use vertical rate to good advantage as was explained in the introduction. It should also be pointed out that for autopilot operation, vertical rate is required to dampen the deviation path. Pitch attitude used for deviation path dampening in the autopilot is washed out (by the 5 sec forward integration) faster than can normally be done to provide stability with stiff glideslope tracking.

A breakdown of the glideslope operation and details is given below:

#### 6.2.1 Overview of Glideslope Operation

The glideslope computation may be entered via a transition from the LOC or the RNAV mode. The RNAV computation will request the ILS main program to perform this transition. If all system validities are acceptable, the ILS main program will activate the localizer and glideslope computations. Each time a transition is requested, the ILS main program will initialize the glideslope computation by setting the logical variable RESETG true for one program cycle.

As long as the localizer computation is in the LOCARM condition, the RNAV steering commands are used to control both the lateral and longitudinal axes. The transition to LOCCAP terminates RNAV control of the lateral steering commands only. ILS control of longitudinal steering command will occur when the glideslope capture mode is entered (GSCAP) subsequent to LOCCAP. However, deactivation of the ILS computation, after LOCCAP, can only be achieved by disengaging the autopilot and reselecting the RNAV mode. Re-entry of the ILS computation is possible and will be treated as an initial request by the ILS main program.

#### 6.2.2 Glideslope Arm (GSARM) Logic

The glideslope control law will be set to the GSARM mode whenever the logic signal RESETG from the ILS main program is true. The computation will remain in this mode as long as the localizer computation is in the arm condition (LOCARM). While in this mode, the computation will estimate the distance to and the approach rate of the glideslope beam. Following LOCCAP that information will be used to select an appropriate point to transition into the capture mode (GSCAP). The transition will occur at the first opportunity following the termination of LOCARM and prior to the intercept of the glideslope.

#### 6.2.3 Glideslope Arm Computation

While in the arm mode, external steering commands are passed directly through the computation without modification. The radio deviation is passed through a gain programmer to estimate linear distance to the glideslope. A rate deriver estimates the approach rate of the glideslope and these two signals are combined with derived barometric altitude rate to generate a pitch command. That command signal is routed to the capture logic rather than the steering command.

#### 6.2.4 Glideslope Capture Logic

Assuming the localizer computation is not in the arm mode and the aircraft is on a course which will at some future time intersect the glideslope, radio deviation will establish the major portion of the pitch command and the rate signal will contribute a portion in opposition to the radio signal. As the glideslope is approached the closure rate will cancel and then exceed the radio signal. When this occurs the pitch command will initially be zero and then of a polarity which directs a flight path away from the



glideslope beam. The capture detector monitors the localizer computation status, the polarity of radio deviation and that of the pitch command. When the condition described above exists, the glideslope computation is switched to the capture mode. Once this mode is enabled the computations are latched in that mode. The GSARM mode can only be reinitiated by the RESETG command generated in the ILS main program. While in the GSCAP mode the VOR/DME/baro altitude based RNAV steering command will be overwritten by the computed pitch command.

Derived barometric rate is used in the capture logic to sense glideslope intercepts from other than a zero flight path. This enables captures to be made from all practical intercept angles, including above the beam captures.

#### 6.2.5 Glideslope Capture and Track Computations

Figure 6-1 also identifies the capture computations. There are two major functions performed by this control law: (1) generate a pitch command which will provide good capture and tracking of the glideslope beam and (2) smoothly transition from external (RNAV) control of the steering command. The first task is accomplished by mixing radio deviation with barometric altitude rate to obtain a pitch command. The radio deviation is gain programmed, and altitude rate is washed out to remove its steady state value. Derived radio rate is held to the value it has when the capture mode is enabled, and since this signal enters pitch command via the same path as altitude rate, it will be smoothly removed by the same washout used to eliminate the steady state value of altitude rate. Notice that the washout is utilized only after capture. The value of the external steering command, at the time of transition to GSCAP, is added to the computed pitch command via a washout. Since pitch command is effectively zero at that time, overwriting the steering command will not cause an unacceptable transient while the previously coupled command is faded out.

#### 6.3. Control Law Analysis

Control law analysis was performed on the system shown in Figure 6-1. Included in the figure is a model of the autopilot. The autopilot model was derived from time response data taken on the NAFEC Gulfstream I aircraft. The gains and time constants were selected to match the following data parameters for a step command:

- a) Time to peak: .42 sec.
- b) Settling time: .92 sec.
- c) Overshoot: 30%
- d) Forward Gain: 4 deg  $\delta$ e/deg  $\theta$
- e) Integration Rate: 1.5°  $\delta$ e/sec.

The only modification was a 4:1 reduction in forward gain. The probable cause of this change is an invalid elevator sensitivity in the aerodynamic data available at Collins.

Figure 6-2 illustrates the manual throttle control loop. The model has shown good correlation with manual pilot performance.

### 6.3.1 Radio Gain Programmer

The gain programmer converts radio deviation (214  $\mu\text{a}/\text{deg}$ ) to linear feet of cross track distance (.496  $\text{ft}/\mu\text{a}-\text{nm}$ ) out to 5.58 nm from the end of the runway. Beyond this point cross track distance is fixed at 2.8  $\text{ft}/\mu\text{a}$ . To extend the range of the programmer beyond this point would invariably result in unacceptable performance due to beam noise. Assuming a shallow 2.5 degree glideslope, the programmer will be effective to an altitude of 1,480 ft. Consequently, normal captures will be performed within the linear range of the programmer. The programmer is a function of distance to touchdown rather than altitude.

### 6.3.2 Capture Detection

Although it is certainly possible to initiate a capture outside the linear range of the gain programmer, the effect of the non-linearity on the capture detector is marginal and the following discussion will therefore be presented assuming linear programmer range. Referring to figure 6-1, an internal pitch command is formed when the glideslope computation is in the arm condition (GSARM). The value of that signal will be

$$\theta = K_h (K_{\Delta h} \Delta h + \dot{h}) + K_{\dot{h}} \Delta h \quad \text{Eq. 6-1}$$

where

$\theta$  = degrees of pitch command (+ directs a pitch down attitude)

$\Delta h$  = approach rate of the glideslope beam (ft/sec)

$\dot{h}$  = ascent rate (ft/sec)

$\Delta h$  = cross track distance (ft), positive above the glideslope

Any flight path intersecting or almost paralleling the glideslope will result in the rate terms having a polarity opposite to that of  $\Delta h$ . When the rate term equals or exceeds the position term, the glideslope capture mode will be enabled (GSCAP). Two conditions exist which will result in a missed capture: (1) transversal of the capture window while LOCARM is active, and (2) a flight path paralleling the glideslope which never established sufficient proximity and/or closure rate to intersect the capture window.

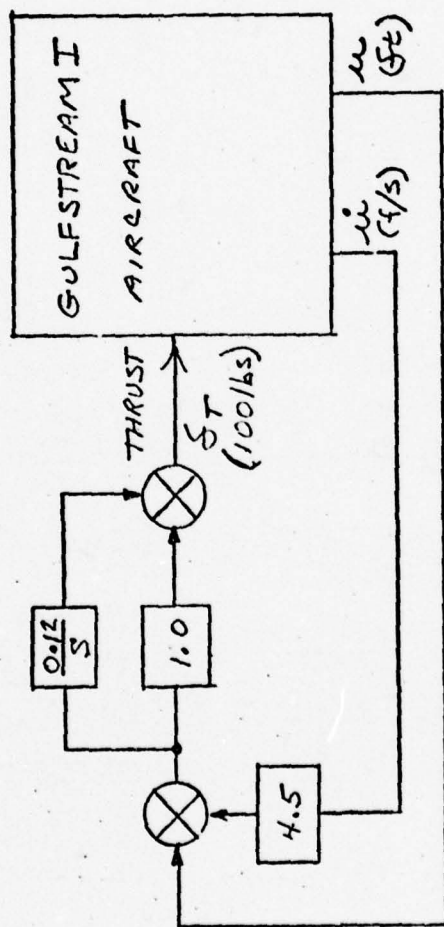


Figure 6-2. AIRSPEED LOOP TO SIMULATE  
MANUAL PILOT AIRSPEED  
CONTROL

Figure 6-2.



The glideslope capture window may be more clearly defined by expressing the rate terms as functions of flight path angle:

$$\dot{h} = U_0 \sin(a)$$

$$\Delta \dot{h} = U_0 \sin(a - a_g)$$

where

$$U_0 = \text{true airspeed}$$

$$a = \text{flight path angle measured as positive counterclockwise from horizontal}$$

$$a_g = \text{glideslope angle (nominally } -2.5 \text{ deg.)}$$

Substituting those expressions into equation 6-1 and setting  $\theta=0$  yields the crosstrack distance at capture as a function of flight path angle:

$$\Delta h_c = - \frac{K_h}{K_{\Delta h}} U_0 [K_{\Delta h} \sin(a - a_g) + \sin a] \quad \text{Eq. 6-2}$$

where

$$K_h = .15 \text{ deg/(ft/sec)}$$

$$K_{\Delta h} = .05 \text{ deg/ft}$$

$$K_{\Delta \dot{h}} = 2.22 \text{ (ft/sec)/(ft/sec)}$$

$$U_0 = 200 \text{ ft/sec}$$

$$a_g = -2.5 \text{ deg.}$$

then

$$\Delta h = -(33.8a + 58.2) \quad \text{Eq. 6-3}$$

Equation 6-3 assumes the flight path angle relative to both the glideslope and the horizontal reference line is small enough to allow the substitution of  $\sin(x)=x$ . The mode logic tests the polarity of equation 6-1 against that of  $\Delta h$ , i.e. if  $(\text{sgn } x) \neq (\text{sgn } \Delta h)$  then capture is initiated. Therefore, the capture window is defined as:

$$0 < \Delta h < - \frac{K_h}{K_{\Delta h}} U_0 [K_{\Delta h} \sin(a - a_g) + \sin a]$$

$$0 < \Delta h < - \frac{K_h}{K_{\Delta h}} U_0 [K_{\Delta h} \sin(a - a_g) + \sin a]$$

Figure G-3 graphically presents the glideslope capture window obtained via equation 6-2. Capture will occur when (1) the aircraft is below the beam and the flight path angle is on or above the line described by equation 6-2, or (2) the aircraft is above the beam and the flight path angle is below the line described by equation 6-2.

Five capture boundary lines are shown to illustrate the effect of longitudinal wind and varying glideslope angles.

Clearly, an RNAV approach paralleling the glideslope must, at some point, close to within 58 feet of the glideslope. Since RNAV errors of 150 feet are not out of the question, there is a possibility of missing the glideslope if capture is attempted with R-NAV assist. However, random variations in the beam as well as the aircraft position will normally result in a capture. A more probable cause of missed capture would be a close-in approach which resulted in a flight path angle in the  $-1.0$  to  $-1.2$  degree range. Here, the capture window can become quite small. Similar arguments apply to captures from below the beam. Although it would be possible to modify the capture laws to encompass parallel RNAV approach configurations additional development will be required.

Since the capture window is actually determined by measured position and rate information, the capture point will be moved to compensate for along track and cross track wind conditions as well as variations in glideslope angle. Simulation data included in this report demonstrate the use of capture point movement to maintain a relatively smooth performance during the capture maneuver. Estimates of distance to and closure rate of the beam in equation 6-3 compensate for environmental variations but cannot distinguish between ascending, descending, or constant altitude capture conditions. The altitude rate term does provide this information and is used to extend the capture point thereby suppressing excessive vertical rates. Examination of simulated captures from above the beam shows the complete absence of overshoot under these conditions.

Table 6-1 summarizes data for simulated approaches. The intercept point is defined as the beam altitude at the intersection of the glideslope and the flight path prior to capture. The approaches were simulated to evaluate system performance capturing and tracking the glideslope.

Figure 6-3  
Capture Boundary

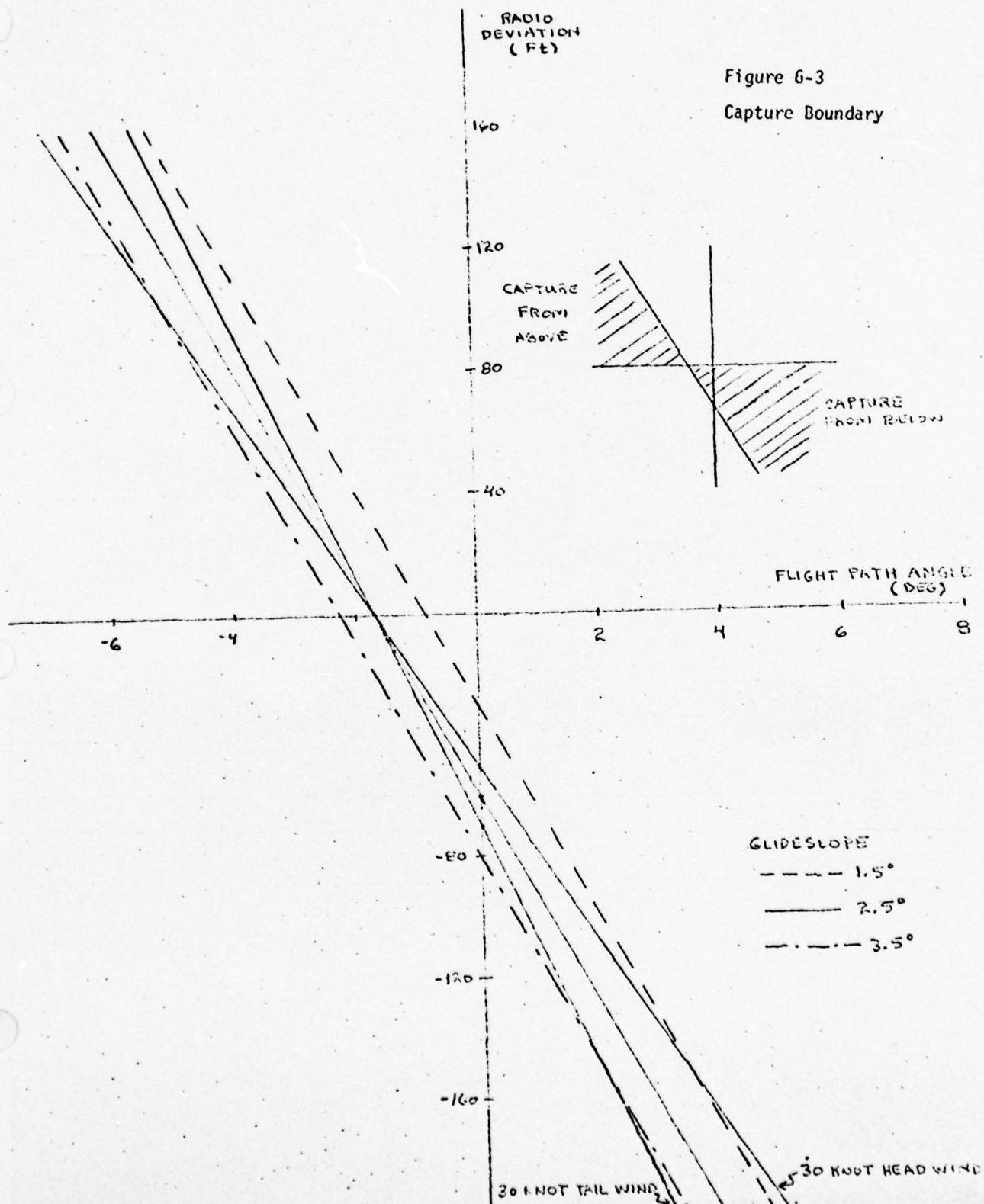




Table 6-1. Simulated Capture Data

Intercept Point (ft)	Flight Path Angle (deg)	Capture Point (ft)	Predicted Value (ft)	Overshoot (ft)	Settling Time (sec)	Strip Chart
1000	0	-50	-58.2	--	8	1A
1000 (From above)	-5	+125	+132	--	45	1B
1300	0	-50	-58.2	--	10	1C
1300 (From above)	-5	+125	+132	--	45	1D
1500	0	-54	>- 58.2	6	20	1E
1800	0	-58	>- 58.2	12	28	2C
1800 (From above)	-5	+90	<132	--	55	2D

As would be expected the data confirms anticipated results. Along with the previously mentioned adaptive behavior, the gain programmer is seen to reduce the capture window as distance to touchdown increases. This is the only non-linear effect in the capture maneuver.

Analog computer simulation results are somewhat different than the predicted values due to a dead zone in the analog capture logic. The predicted values were attained when simulations were performed using the digital version of the control laws.

### 6.3.3 Stability Margin Analysis

To analyze the stability of the glideslope control laws of Figure 6-1 frequency response or Bode plots were obtained. Reference to Autothrottles in this discussion is to Figure 6-2. Figure 6-4 is an open loop bode plot of the radio or deviation loop. This plot indicates the stability of the aircraft when tracking the glideslope beam. Autothrottles were also used for Figure 6-4. The aircraft used to obtain this plot was the Gulfstream I approach flight condition (200 ft/sec airspeed). From Figure 6-4 it can be seen that the bandwidth is sufficient to achieve good Category II tracking performance. The stability margins as summarized in Table 6-2 indicate good stability for the glideslope maneuver.

Figure 6-5 illustrates the outer loop or deviation loop broken as in

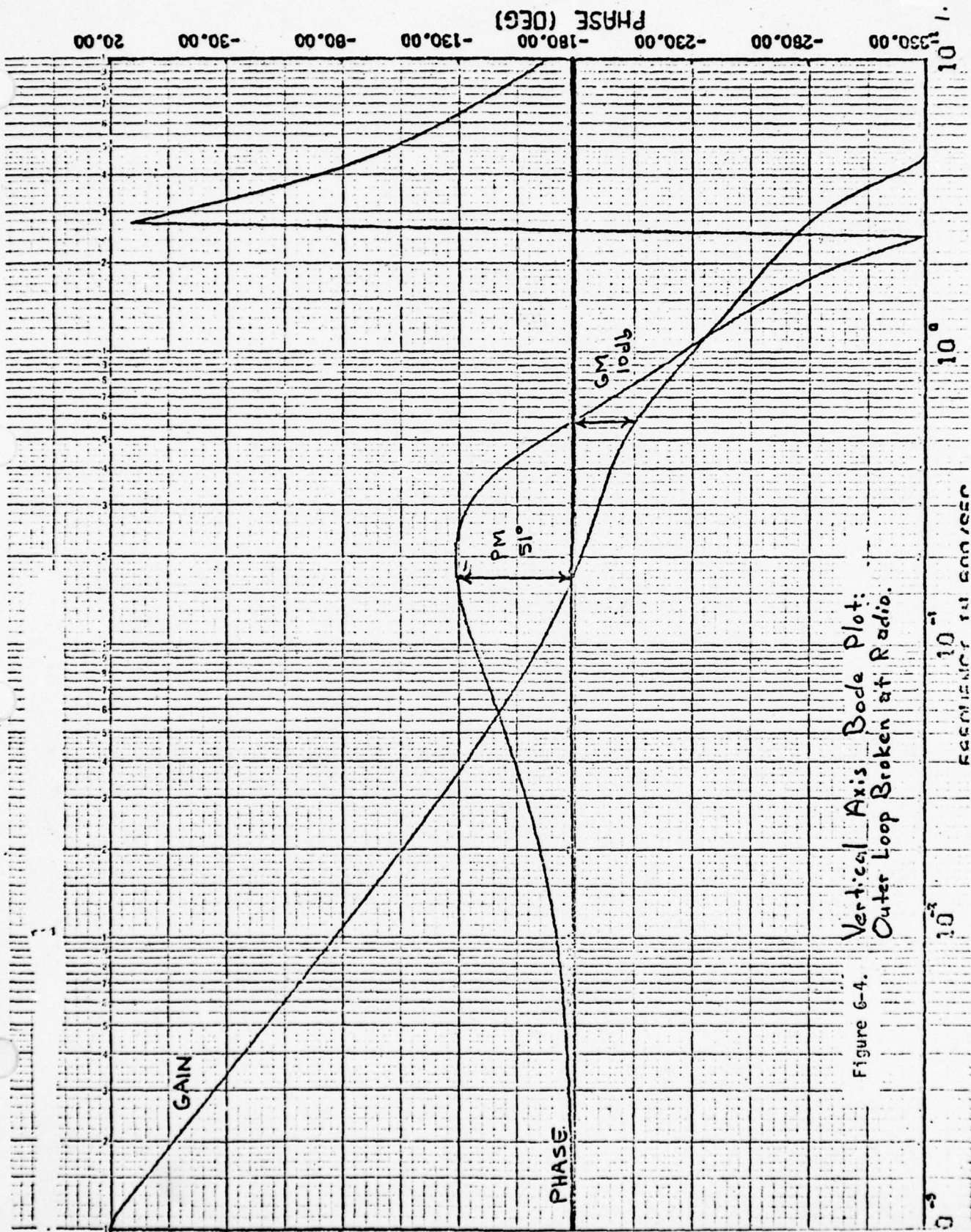


Figure 6-4. Vertical Axis Bode Plot:  
Outer Loop Broken at Radio.



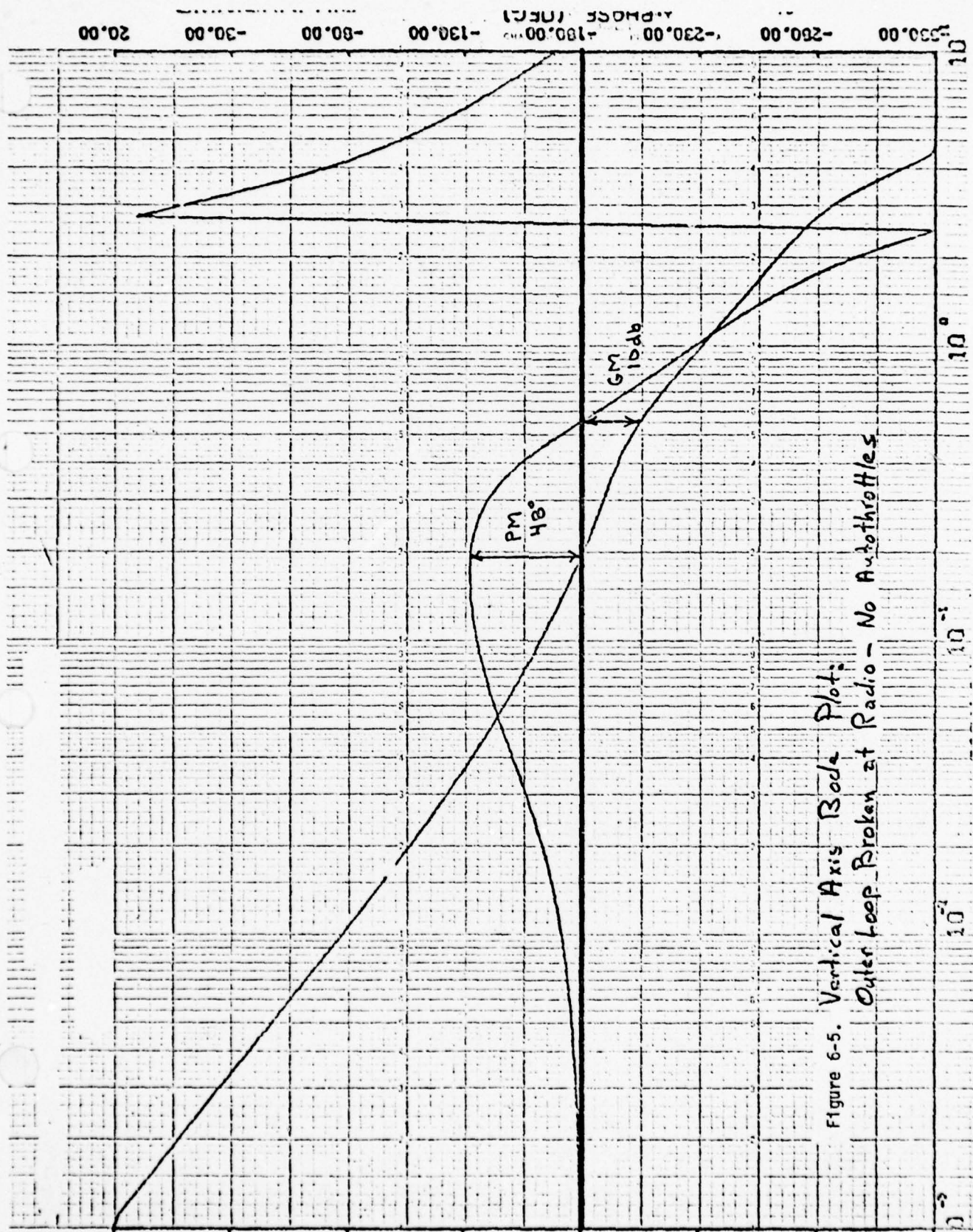


Figure 6-5. Vertical Axis Bode Plot:  
Outer Loop Broken at Radio - No Autothrottles



Figure 6-4, but the autothrottles were removed. As can be seen by comparing the two figures, airspeed control does not greatly effect glideslope tracking stability.

Figure 6-6 is a bode plot of the control laws of Figure 6-1 broken in the inner loop or at the servo. All outer loops are closed. This plot is indicative of the inner loop or elevator activity and stability while the system is tracking the glideslope. The bandwidth and stability indicated by Figure 6-6 is typical of good Category II glideslope computations. The stability margins and bandwidth are summarized in Table 6-2. Figure 6-7 is the same as Figure 6-6 except for the lack of autothrottles. As can be seen airspeed control does not effect the inner loop stability or bandwidth to any great extent.

Table 6-2. Frequency Response Data

FIGURE	GAIN MARGIN (db)	PHASE MARGIN (deg)	BANDWIDTH (rad)	OPENED LOOP	CONFIGURATION
6-4	10	51	.175	Radio	Autothrottles
6-5	10	48	.2	Radio	No autothrottles
6-6	10	75	.7	Servo	Autothrottles
6-7	10	75	.7	Servo	No autothrottles

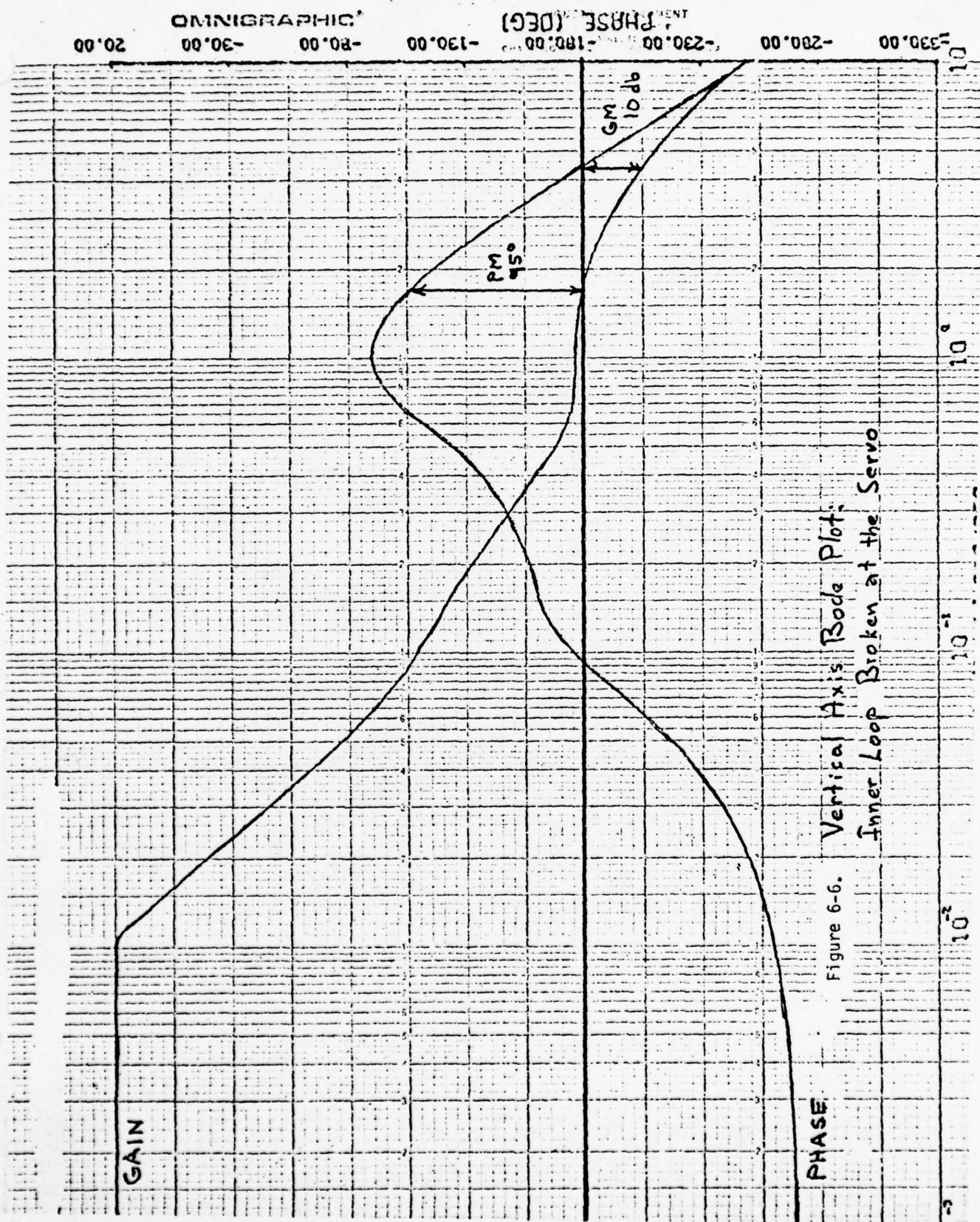


Figure 6-6. Vertical Axis Bode Plot:  
Inner Loop Broken at the Servo

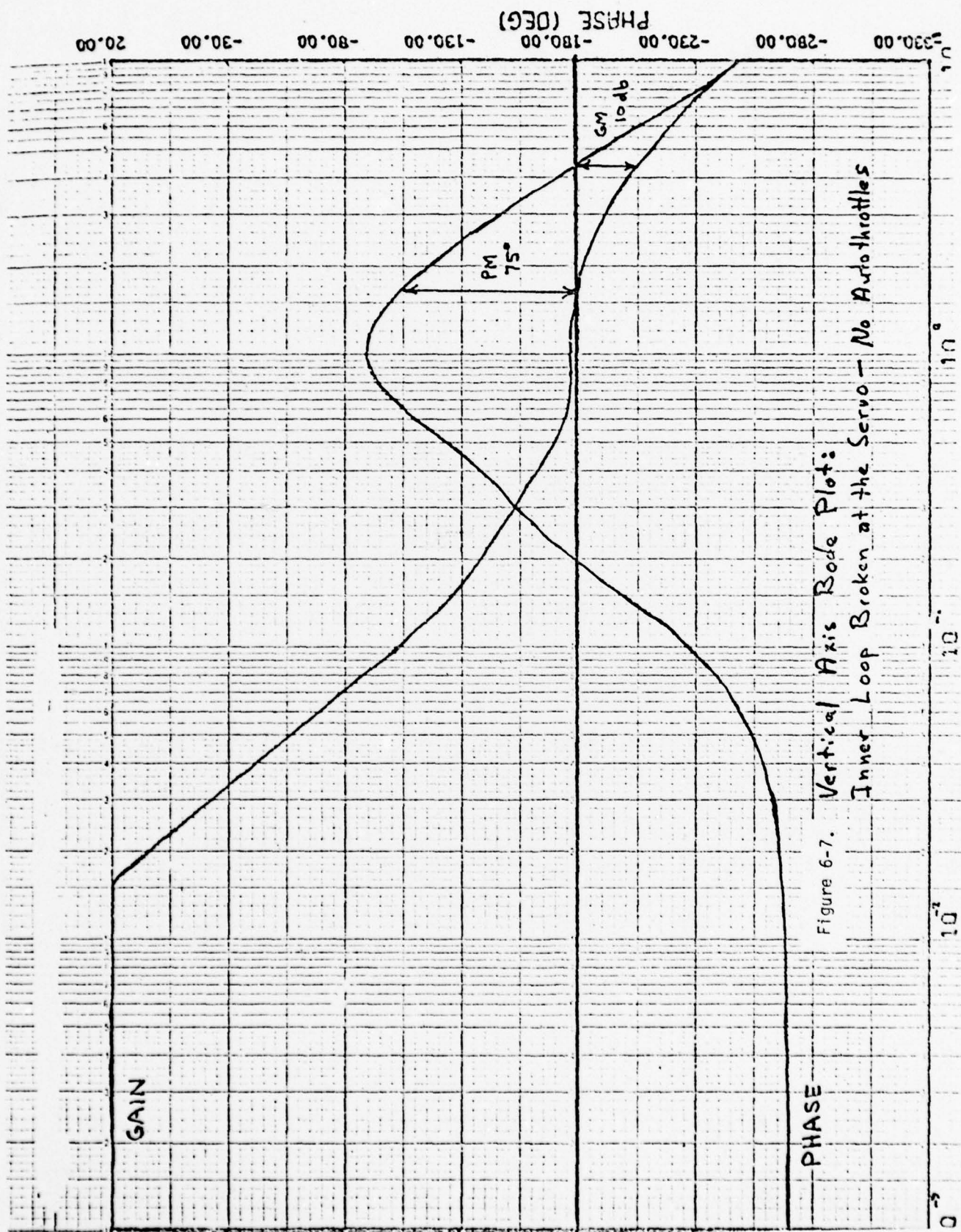


Figure 6-7. Vertical Axis Bode Plot:  
Inner Loop Broken at the Servo - No Autothrottles



## 6.4 Performance

To evaluate the performance of the glideslope computations, the system was simulated on the EAI 680. The system of Figure 6-1 was used with a simulation of the Gulfstream I aircraft (approach flight condition). To simulate manual airspeed control, the autothrottle system shown in Figure 6-2 was used. The autothrottle system was adjusted to give airspeed control similar to what is known to be typical of manual operation. Strip chart recordings were taken using radio noise, vertical wind turbulence, longitudinal wind turbulence and radio steps.

### 6.4.1 Radio Steps

Strip chart recordings were taken for step changes in glideslope. These recordings illustrated the stability of the glideslope computations when tracking the glideslope beam. The glideslope tracking performance had sufficient stability and bandwidth. The responses were smooth and well damped.

### 6.4.2 Vertical Turbulence

The following represents the  $2\sigma$  vertical turbulence transfer function (ref. 5) used for the performance simulation.

$$\text{white noise} \rightarrow \boxed{\frac{K}{1+(L/V)S}} \rightarrow \sigma_{\theta}$$

where

$S$  = complex variable of Laplacian operator  
 $V$  = approach speed (200 ft/sec)  
 $L$  = vertical scale length (30 ft.)  
 $\sigma_{\theta}$  = 1.3 deg RMS ( $2\sigma$  level)

It should be strongly pointed out that the RMS level of vertical turbulence represents a  $2\sigma$  value. In other words, this level of turbulence would be expected on only 5% of the approaches if a random selection were made over a total every day operation.

For the assumed flight condition this model corresponds to .15 sec. correlated noise, and RMS output value of 1.3 degrees was used in the simulation effort. At an airspeed of 200 ft/sec this is equivalent to 5.6 ft/sec (RMS) vertical gusts. System response to wind gusts at fixed distances from the runway is summarized in Table 6-3.

Table 6-3. System Deviations to Vertical Gusts

Gust Strength (deg) RMS	Distance (nm)	Airspeed (f/s) RMS	Pitch (deg) RMS	Pitch Command RMS	Deviation (ft) RMS	Altitude Rate (f/s) RMS	Servo Command (deg) RMS
1.3	7.46	.12	.183	.233	4	1.75	.24
	6	.12	.267	.267	6.67	2.167	.316
	4.54*	.12	.2	.267	4	1.67	.267
	5.7-2.2*	.12	.2	.3	4.53	2.	.3

\*typical of performance in the linear range of the radio programmer

The performance exhibited indicates no problem. Performance capable of Cat. II performance has been achieved. Servo or control activity as can be seen from Table 6-3 is satisfactory.

#### 6.4.3 Longitudinal Gust Performance

As was the case for vertical gusts, Reference 5 provided the following  $2\sigma$  longitudinal gust transfer function:

$$\text{white noise} \rightarrow \frac{K}{1+(L/V)S} \rightarrow u_g$$

where

- S = complex variable of Laplacian operator
- L = longitudinal scale length (600 ft)
- V = approach speed (200 f/sec)
- $u_g$  = 6 ft/sec RMS ( $2\sigma$  level)

An RMS output of 6 ft/sec was employed during simulated approaches. Again data runs were made at fixed distances inside, outside, and at altitudes corresponding to the knee of the radio gain programmer. Table 6-4 summarizes the data recorded.

Table 6-4. System Deviations to Longitudinal Gusts

Gust Strength (f/s) RMS	Airspeed (ft/sec) RMS	Pitch (deg) RMS	Pitch Command (deg) RMS	Deviation (ft) RMS	Altitude Rate (f/s) RMS	Servo Command (deg) RMS	Distance (nm)
6.	1.5	.266	.88	5.33	2.0	.267	4.36
	1.5	.317	.567	12.0	2.83	.383	6.0
	1.67	.383	.767	13.3	3.75	.333	7.64
	1.625	.3	.567	7.65	2.75	.333	3.2-.377

\*typical approach condition

From Table 6-4 it can be seen that the system tracks the glideslope beam quite well during the longitudinal turbulence. Cat. II performance is achieved. Servo or control activity is indicative of that known acceptable from past experience on other systems.

#### 6.4.4 Radio Noise Performance

The following noise model was used to estimate system performance in the presence of beam noise:

$$\text{white noise} \rightarrow \boxed{\frac{K}{\tau S + 1}} \rightarrow \sigma_y \text{ Radio Simulation Output}$$

where

$S$  = complex variable of Laplacian operator

$\tau$  = 4 sec.

$\sigma_y$  = 10 ua RMS

This model is considered a low quality Cat. I facility.

Table 6-5 summarizes the performance from some of the recordings for various distances. Table 6-5 illustrates that Cat. II performance is achieved and servo or control activity is not excessive.



Table 6-5. System Deviations to Radio Noise

Radio Noise (ua)	Distance (nm)	Airspeed (ft/sec) RMS	Pitch (deg) RMS	Pitch Command (deg) RMS	Deviation (ft) RMS	Altitude Rate (ft/sec)	Servo Command (deg) RMS
(12.5 ft) 3.35	7.46	.12	.18	.35	8.0	1.25	.167
(10.65 ft) 3.55	6.0	.117	.25	.434	6.67	1.5	.217
(7.85 ft) 3.45	4.54	.117	.183	.33	7.35	1.25	.125

#### 6.5 CONCLUSION

Simulation and analysis results indicate category II performance can be expected from these glideslope control laws. In addition, these control laws have been shown to be capable of acceptable performance when glideslope captures are initiated from other than an altitude hold mode. This capability may be considered a first step to area navigation aided vertical approach maneuvers.

APPENDIX A

Program Listing of the Flight Plan

Editor Utility Module

A-2



```

57 PRESET SEVENTEEN=03FFFEFFH
58 ... ***** PROCEDURE OF DECLARATIONS *****
59 POINTER PROCEDURE
60 MASSACHUSETTS
61 ... RMS SEARCH ROUTINE //
62 ... CLEAR ALL OFFSETS //
63 ... ZERO FILL ROUTINE //
64 ... ORG-QUEST USED //
65 ... RMS COPY RTN //
66 REAL PROCEDURE
67 SIGN //
68 ... SIGN OF REAL NUMBER //
69 ... ***** EXTERNAL DECLARATIONS *****
70 EXTERNAL
71 ... *****
72 ... *****
73 ... *****
74 ... *****
75 ... *****
76 ... *****
77 ... *****
78 ... *****
79 ... *****
80 ... *****
81 ... *****
82 ... *****
83 ... *****
84 ... *****
85 ... *****
86 ... *****
87 ... *****
88 ... *****
89 ... *****
90 ... *****
91 ... *****
92 ... *****
93 ... *****
94 ... *****
95 ... *****
96 ... *****
97 ... *****
98 ... *****
99 ... *****
100 ... *****
101 ... *****
102 ... *****
103 ... *****
104 ... *****
105 ... *****
106 ... *****
107 ... *****
108 ... *****
109 ... *****
110 ... *****
111 ... *****
112 ... *****
113 ... *****

```

00000094

00000106

... \*\*\*\*\* PROCEDURES \*\*\*\*\* //

REPLACE

VALUE = REPLACE(STARTNO, STOPNO, NOITEMS, PROC, NKPTR)

THIS IS AN INTEGER PROC USED AS THE FET REPLACE ROUTINE.  
ITEMS FROM EVENT NUM STARTNO THRU EVENT NUM STOPNO ARE  
DELETED. ANY NEW ITEMS ARE THEN INSERTED WITH ADJUSTING.

DEFINE INTEGER PROCEDURE REPLACE(STARTNO, STOPNO, NOITEMS, PROC, NKPTR)  
WHERE INTEGER STARTNO, STOPNO, NOITEMS;  
POINTER PROC;  
POINTER NKPTR

TOPE BEGIN  
ON POINTER START  
ON POINTER STOP  
ON POINTER PROC;  
ON INTEGER NOITEMS;  
ON INTEGER STARTNO;  
ON INTEGER STOPNO;

... \*\*\*\*\* PROC REPLACE \*\*\*\*\* //

```

114      ITEM*NO*ITEMS!
115      IF SVEVRSF=VERSFL NQO VERS(WKPTR)
116      THEN BEGIN
117          REPLACFL=OVERNT
118          GOTO RETURN!
119      END!
120      ***** VERSION MISMATCH*****
121      ***** INHIBIT ACCESS TO FET *****
122      ***** MAKE START OF DELETE PTR *****
123      ***** MAKE STOP OF DELETE PTR *****
124      ***** CHECK RAS FOR ROOM *****
125      ***** CALL CHANCE RAS OVERFLOW *****
126      ***** A ONE-FOR-ONE REFLAC IS *****
127      ***** A SPECIAL CASE WHERE ONE *****
128      ***** LATERAL EVENT IS *****
129      ***** OVERWRITTEN BY ANDSHFF. A *****
130      ***** ONE-FOR-ONE REFLAC *****
131      ***** REQUIRES THE FOLLOWING *****
132      ***** 1. EVENTS MUST BE *****
133      ***** LATERAL EVENTS *****
134      ***** 2. ONE ITEM MUST BE *****
135      ***** DELETED *****
136      ***** 3. ONE ITEM MUST BE *****
137      ***** ADDED *****
138      ***** 4. ID'S MUST MATCH *****
139      ***** MUST BE LATERAL EVENT *****
140      ***** ***** LATERAL EVENT ***** *****
141      ***** ID'S MUST MATCH *****
142      ***** ***** ***** ***** *****
143      ***** ***** ***** ***** *****
144      ***** ***** ***** ***** *****
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170      ***** ***** ***** ***** *****

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171 ... NEW ITEMS ARE ADDED USING
172 THE ROUTINE ADDSTR.
173 RATHER THAN ADDATE SO
174 THAT VERSFL CAN BE
175 INDEPENDENTLY CONTROLLED
176 BY BOTH REPLACF AND
177 ADDATE
178 ... OVERWRITE REPLACED EVENTS //
179
180 GOODRTN:
181   ACOSTENG(PNTR,ITEM,NO,PROC,WPTR) //
182   ... ADD NEW EVENTS //
183   ... FIXFLT WILL VALIDATE ALL
184   RMS ITEMS, CALCULATE OFTO
185   FOR ALL ITEMS AND
186   CALCULATE FLIGHT PARAMS
187   IN NEIGHBORHOOD OF NEW
188   ITEMS //
189   ... FIXUP FET AND PAS //
190   ... PUMP VERSION NUMBER //
191   ... REPORT GOOD RETURN //
192   ... ***** PROC REPLACF ***** //
193   ...
194   ...
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```





```

285 DEFINE PROCEDURE ANDSTRNGIAT,PNTN,NOITEMS,PROC,WKPTR)
286 WHERE
287   POINTER AT,PNTN:
288   INTEGER NOITEMS:
289   POINTER PROCEDURE PROC:
290   POINTER WKPTR TOBE
291 BEGIN
292   OWN POINTER FETCH:
293   OWN POINTER PNT1:
294   OWN POINTER PNT2:
295   OWN POINTER PNT3:
296   OWN POINTER PNT4:
297   OWN POINTER PNT5:
298   OWN POINTER PNT6:
299   OWN INTEGER TYPE:
300   PNT1 SET PNT1:
301   PNT2 SET PNT2:
302   PNT3 SET PNT3:
303   PNT4 SET PNT4:
304   PNT5 SET PNT5:
305   PNT6 SET PNT6:
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531   PNT232 SET PNT232:
532   PNT233 SET PNT233:
533   PNT234 SET PNT234:
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537   PNT238 SET PNT238:
538   PNT239 SET PNT239:
539   PNT240 SET PNT240:
540   PNT241 SET PNT241:
541   PNT242 SET PNT242:
542   PNT243 SET PNT243:
543   PNT244 SET PNT244:
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342 AND 'TO' EVENTS ARE
343 DEFINED. THE START OF THE
344 FLT IS FOUND. EVENT
345 NUMBER 1 IS FOUND
346 FIRST, MAKE TOEVE & FRMEV//
347 ... INVALID ON ALL ITEMS. //
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[illegible]

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513 OF A SEVFEK COURSE CHANGE
514 IORT 160 DEGJ FOR'E ANFS
515 TO ZERO WAKING TURN PFGIN
516 WHEN AIRCRAFT EVEN WITH
517 WAYPOINT.
518
519 IF PFSTAT EOL PARALLEL AND
520 ((ANG GRT DEGRD AND
521 HALF * POFSEF6 GE3 0.0)
522 OR ANG LES DEGRD)
523 THEN ANFSLE=POFSFE*NSIN(HALF)/NCOS(HALF);
524 GOTO RETURN;
525 END;
526
527 ... ***** PROC AUFSE *****
528
529 *****
530 INSERT
531
532 *****
533
534 THIS ROUTINE USES THE INFO IN THE WORK AREA POINTED AT
535 BY FR..PTR TO BUILD AN FET ITEM OF THE APPROPRIATE TYPE
536 AND PLAC IT AT THE ITEM POINTED AT WITH TO.PTR.
537
538 *****
539
540 DEFINE PROCEDURE INSERT(FRM..PTR, TO.PTR)
541 WHERE POINTER FRM..PTR, TO.PTR
542 TUBE
543 BEGIN
544   OWN POINTER FROM;
545   OWN POINTER IT;
546   OWN INTEGER TYPE;
547   OWN INTEGER SAVE;
548   OWN POINTER PTR1;
549   OWN INTEGER TEPP;
550
551   FROM = FRM..PTR;
552   IT = TO.PTR;
553   TYPE = EMTYPE(FROM);
554   TYPEFF(IT) = TYPE;
555   GOTO TYPE.SN(TYPE - 2);
556
557   SWITCH TYPE.SN = STOR.CW, HE.TYPE, VE.TYPE, LC.TYPE;
558
559   HE.TYPE:
560
561   LC.TYPE:
562
563   IF PTRHEWSSRCH(MYPID(FROM)) EOL NULL ... ID IN RMS?
564   THEN BEGIN
565     PTRHEWSSRCH(0);
566     DEFPTH(PTR) = ZERO;
567     ENCL;
568     SAVE=DEFPTH(PTR);
569     COPYTH(PTR, FROM);
570     CTL=ORD(PTR);
571     (CATH=ORD(FROM) .RS. 17) .A. "ON;
572     ROTTECHS(LFROM);
573     SPECITTE(LFROM);
574     IF TEMPEOFSE(FROM) EOL PARALLEL
575     THEN TYPE=JCOPE;
576     OFFG,IT)=IFXPI;
577
578   ... POINT AT WORK AREA
579   ... POINT AT EMPTY ITEM
580   ... GET EVENT TYPE
581   ... SET FIELD IN NEW ITEM
582   ... JUMP THRU ITEM TYPE TABLE
583   ... HOLD EVENT TYPE ITEM
584
585   ... LATERAL EVENT TYPE ITEM
586
587   IF PTRHEWSSRCH(MYPID(FROM)) EOL NULL ... ID IN RMS?
588   THEN BEGIN
589     PTRHEWSSRCH(0);
590     DEFPTH(PTR) = ZERO;
591     ENCL;
592     SAVE=DEFPTH(PTR);
593     COPYTH(PTR, FROM);
594     CTL=ORD(PTR);
595     (CATH=ORD(FROM) .RS. 17) .A. "ON;
596     ROTTECHS(LFROM);
597     SPECITTE(LFROM);
598     IF TEMPEOFSE(FROM) EOL PARALLEL
599     THEN TYPE=JCOPE;
600     OFFG,IT)=IFXPI;

```



```

570 REPTPR:PTRN)=SAVEI; ... RESTORE RAS POINTER //
571 RASFE(17)=IPNTH-STRI,RAS+31/231 ... CALC RAS ITEM NUMBER//
572 //
573 VE.TYPE: W2(17)=A10(FROM1) ... ALTD AND A-YID GO IN WRG2//
574 //
575 STOR.CN: C.LITS(17)=
576 (CMTPRON(FROM),RS,3) .V. 61 ... TORVF=FMMELV=INVALID // 0000065A
577 IF TYPE NEW LTP
578 THEN RYTES(17)=AUX*CTL(FROM); ... STORE EXTRA CTL BITS // 00000659
579 GOTO RETURN;
580 END; ... ***** PROC INSERT ***** //
581 //
582 *****
583 CMTPRSE(STAT,STOP)
584 *****
585 NEW-STOP = CMTPRSE(EDT,STR1,EDT,STOP)
586 *****
587 THIS ROUTINE EXPANDS THE SPAN OF THE EDIT TO INCLUDE ANY
588 TRAILING EVENTS DEPENDENT UPON EDITED LATERAL EVENTS. IT
589 THEN COMPRESSES THE FET BY MOVING ANY ITEMS BETWEEN FESHT
590 AND THE START OF THE EDIT. A POINTER TO THE LAST ITEM IN
591 THE EXPANDED FET SPAN IS RETURNED.
592 *****
593 *****
594 DEFINE POINTER PROCEDURE CMTPRSE(EDT,STR1,EDT,STOP)
595 WHERE POINTER EDT,STR1,EDT,STOP TOBE
596 BEGIN
597 ... ***** PROC CMTPRSE *****//
598 OWN POINTER STR1;
599 OWN POINTER STOP;
600 STOP=EDT,STOP+17P,SIZE;
601 STR1 = EDT,STR1;
602 IF SMOUFF(STR1-17P,SIZE+LDSK) LES STOP
603 THEN STOP=SCHUFF(STR1-17P,SIZE+LDSK); ... INCL DUP FVTS//
604 CMTPRSE = STOP; ... RETURN NEW END POINT// 00000651
605 *****
606 LOOP:
607 STR1 = STR1-1;
608 STOP = STOP-1;
609 IF STOP LES FESHT
610 THEN BEGIN
611 WOSTUR)=WOST(STR1);
612 GOTO LOOP;
613 END;
614 FESHT = FLSTR1*(STOP-STR1); ... CALC NEW TABLE START //
615 GOTO RETURN;
616 END;
617 *****
618 *****
619 F1AFET
620 *****
621 F1AFET(LACTIP,NOITEMS)
622 *****
623 THIS ROUTINE REPAIRS THE FET FOLLOWING AN F01T, AND IT
624 REVALIDATES ALL ITEMS IN THE RAS. IT MAKES A SINGLE PASS
625 OVER THE FET. DURING THIS PASS, IT CALCULATES ALL VERTICAL
626 PATH ANGLES. WITHIN THE SPAN OF THE EDIT, IT CALCULATES

```

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```

684 POFS.TMP = POFSFEI
685 MAYOR2 = FETENOI
686 MAYOR1 = FESJTI
687
688 IF MAYOR1 LEQ FESJTI
689 THEN DISTFEIESTAT=0.01
690 GOTO DOW11
691
692
693 IF ITNCRHUFET(ITEM,OLVMSK)EQL NULL ... DEST. LEAVE
694 THEN REGIN
695 IF C-BITS(FESTAT) .A. "80" NEQ ZERO ... OUT OF ITEMS
696 THEN CRSTFEIESTAT=CRSOF(FESTAT) ... INIT 1ST FVT
697 FOR PTR=STNT,MAS STEP 3
698 UNTIL STOP=MS
699 DO IF CILANDPTR GRK "7F" ... MSN OF BYTH 0 SFT
700 THEN M0(PNTR) = 0
701 GOTO RETURN1
702
703 IF TYPEFE(ITEM) EQL DTYP
704
705
706
707
708
709
710 THEN REGIN
711 PRSUF(PRV.LE)=0.01
712 GOTO DONE1
713
714
715
716
717
718 IF TYPEFE(ITEM) EQL VTYP
719 THEN REGIN
720 V.EVENT = ITEM1
721 VPRFLV.EVNT)=0.01
722 VPRFLV.EVNT)=0.01
723 GOTO NXT.1TH1
724
725 IF ITEM LES MAYOR1
726
727 THEN GOTO DONE1
728 IF PRV.LE EQL MAYOR2
729 THEN REGIN
730
731 TNP.REAL=OSTWUPRV.LE)+AUF5FF(1PRV.LE)1
732 OSTWUPRV.LE)+TMP.REAL1 ... COMPLETE DIST FOR MAYOR2
733 TYPEFE(1PRV.LE)ELTYP1 ... RESTORE ITEM TYPE
734 DELTA=TNP.REAL-OLD.DIST1 ... CALC INCREASED DIST.
735
736 IF ITEM GRT MAYOR2
737 THEN REGIN
738
739
740

```



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741 DST=RU(ITEM)=OSTWRO(ITEM)+DELTA; ... FIX DISTANCE. //
742 GOTO CORRE1
743 END;
744 ... BEYOND EDIT ***** //
745 ... WITHIN SPAN OF EDIT, ALL //
746 FLIGHT PARAMS ARE //
747 CALCULATED //
748 IF RWSE(PRV.LE) EQL ZERO OR //
749 (CTLWD(PSWSPTR(PSV.LE)) .V. ... BITS FOR EITHER POINT // 00000049
750 CTLWD(PSWSPTR(ITEM))) .A. ... FIRST LINK IN CHAIN. // 00000850
751 "30" NEW 0 //
752 THEN REGN //
753 DST=RU(ITEM)=OSTWRO(PSV.LE)+ITEM+1; ... BYPASS LLTD ***** //
754 PRSFE(ITEM)=CMSOFE(PSV.LE) ... DEFEAT 1/10 LINK //
755 IF FOC.PTH EQL NULL ... LAST LAT ANGLES = //
756 THEN LOC.PTR=SMCHFE(ITEM,VMSK) ... VPAT IS FLAGGED //
757 GOTO CORRE1 //
758 END;
759 LLTD(PSWSPTR(PSV.LE)+1)=RWSPT(ITEM)+1; ... BYPASS LLTD ***** //
760 TMP.REAL=RU(ANSRD); ... CALC CRSD //
761 TMP.INTG=(TMP.REAL+INTG ... SWITCH NAME OF OWN REP SC // 00000860
762 .A. "FFFFF000") ... WE CAN PROTECT BYTE 3 // 00000661
763 .V. C.BITS(PSV.LE);
764 CRSD(PSV.LE)=TMP.REAL;
765 IF C.BITS(ITEM) .A. "80" EQL ZERO
766 THEN REGN //
767 IF ITEM EQL ANS.1 //
768 THEN GOTO CALCAGS1 //
769 C.BITS(ITEM)=C.BITS(ITEM) .V. "80"; ... CRSD INVALID //
770 END;
771 TMP.REAL=RU(ANSRD)+UEGRH01 //
772 TMP.INTG=(TMP.REAL+INTG ... CALC CRST //
773 .A. "FFFFF000") //
774 .V. RWSE(ITEM); ... ADD BYTE 3 //
775 CRSD(ITEM)=TMP.REAL; ... STORE //
776
777 CALCAOFS:
778 TMP.REAL=AUFSE(PSV.LE); ... CALC AOF //
779 DST=RU(PSV.LE)=OSTWRO(PSV.LE)+TMP.REAL; ... REPAIR BYTF 3 //
780 TYPEFF(PSV.LE)=LTP; ... SAVE OLD DIST FOR DELTA //
781 OLD.DIST=OSTWRO(ITEM); ... STORE PARTIAL DIST. AOF //
782 TMP.REAL=OSTWRO(PSV.LE) ... IS ADDED NEXT LL. //
783 +R2(ANSRD)+TMP.REAL; ... THE FOLLOWING LOGIC CORRECTS //
784 ... THE DISTANCE VALUE FOR BASE //
785 OFFSETS. THE DIST VALUES FOR //
786 THE 1ST WAYPOINT OF THE //
787 OFFSET CONFIG & THE WAYPOINT //
788 PAST THE LAST OFFSET EVENT //
789 HAVE THE OFFSET VALUE //
790 30000.
791 IF OFFE(ITEM) EQL STRT90 //
792 OR OFFE(ITEM) EQL STRTBASE ... START OF 2-EVENT PATTERN //
793 OR OFFE(PSV.LE) EQL ENJ90 ... START OF 3-EVENT PATTERN //
794 OR OFFE(PSV.LE) EQL INTERCEP ... FVT PAST 2-EVENT PATTERN //
795 THEN TMP.REAL=TMP.REAL+PJSFEI ... FVT PAST 3-EVENT PATTERN //
796 DSTWRO(ITEM)=TMP.REAL; ... ADD OFFSET TO DISTANCE //
797 IF RWSE(ITEM) EQL RWSE(PSV.LE) ... BUT IN THIS FILE //
    
```

```

798 THEN BEGIN
799   ITEM=CMPSRFL(ITEM,ITEM)
800   ADJUSTING(ITEM,0,0,0,0)
801   COTO 8011
802   END
803   DONE:
804   DONE1:
805   IF V-VE=0 THEN
806     THEN BEGIN
807       IF PRV-VE=0 THEN
808         THEN BEGIN
809           IF PRV-VE=0 THEN
810             THEN BEGIN
811               IF PRV-VE=0 THEN
812                 THEN BEGIN
813                   IF PRV-VE=0 THEN
814                     THEN BEGIN
815                       IF PRV-VE=0 THEN
816                         THEN BEGIN
817                           IF PRV-VE=0 THEN
818                             THEN BEGIN
819                               IF PRV-VE=0 THEN
820                                 THEN BEGIN
821                                   IF PRV-VE=0 THEN
822                                     THEN BEGIN
823                                       IF PRV-VE=0 THEN
824                                         THEN BEGIN
825                                           IF PRV-VE=0 THEN
826                                             THEN BEGIN
827                                               IF PRV-VE=0 THEN
828                                                 THEN BEGIN
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833                                                           IF PRV-VE=0 THEN
834                                                             THEN BEGIN
835                                                               IF PRV-VE=0 THEN
836                                                                 THEN BEGIN
837                                                                   IF PRV-VE=0 THEN
838                                                                     THEN BEGIN
839                                                                       IF PRV-VE=0 THEN
840                                                                         THEN BEGIN
841                                                                           IF PRV-VE=0 THEN
842                                                                             THEN BEGIN
843                                                                               IF PRV-VE=0 THEN
844                                                                                 THEN BEGIN
845                                                                                   IF PRV-VE=0 THEN
846                                                                                     THEN BEGIN
847                                                                                       IF PRV-VE=0 THEN
848                                                                                         THEN BEGIN
849                                                                                           IF PRV-VE=0 THEN
850                                                                                             THEN BEGIN
851                                                                                               IF PRV-VE=0 THEN
852                                                                                                 THEN BEGIN
853                                                                                                   IF PRV-VE=0 THEN
854                                                                                                     THEN BEGIN

```

```

855      ...      PROC HSPTR *****//
856      ...      ...
857      ...      ...
858      ...      ...
859      ...      ...
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912 NOITEM:      THEN REGIN      ... ***** SEARCH FAILED *****//
913      GETTYPE = NOEVTI      //
914      GOTO RETURN1          //
915      FND:                  //
916      IF TYPVASK .A. EVMASK(TYPEFE(PNTR)) ... SEARCH FAILED *****//
917      ... COMPARE TYPVASK//
918      FCL 0                  ... WITH LOOKUP TABLE MASK //
919      THEN GOTO NXT.ITM:      ... NO MATCH //
920      IF CNTR=CNTR+1 NEQ 0    ... FOUND ONF. BUMP COUNTER //
921      THEN REGIN            ... ***** BACK-UP POINTER *****//
922      NXT.ITM:              //
923      PNTR=PNTR-ITM-SIZE:    ... DECREMENT POINTER //
924      GOTO LOOP2:          ... TRY AGAIN //
925      FND:                  //
926      FOUND:                //
927      GETTYPE=BUILDFE(PNTR,WKPTR): ... BUILD A WORK AREA //
928      GOTO RETURN1          //
929      ENCL                  //
930      ...                   //
931      ***** PROC GETTYPE *****//
932      ...                   //
933      GETNXAFE              //
934      ...                   //
935      RESULT = GETNXAFE(TYPVASK,ABSEVNO,WKPTR)
936      ...                   //
937      THIS ROUTINE FINDS THE FIRST EVENT OF THE TYPE INDICATED
938      BY TYPVASK AFTER THE EVENT SPECIFIED BY ABSEVNO. IF AN
939      EVENT IS FOUND, IT IS RETURNED IN THE WORK AREA SPECIFIED
940      BY WKPTR.
941      ...                   //
942      ***** PROC GETNXAFE *****//
943      ...                   //
944      DEFINT INTEGER RECURSIVE PROCEDURE GETNXAFE(TYPVASK,ABSEVNO,WKPTR)
945      WHERE INTEGER TYPVASK,ABSEVNO:1
946      POINTER WKPTR TOBE
947      BEGIN
948      OWN POINTER PNTR:
949      IF PNTR=SEARCHFE(CONVFE(ABSEVNO),TYPVASK)
950      FCL NULL
951      THEN REGIN
952      GETNXAFE=NOEVTI
953      GOTO RETURN1
954      FND:
955      GETNXAFE=BUILDFE(PNTR,WKPTR): ... SUCCESS, BUILD WORK AREA //
956      GOTO RETURN1          //
957      ENCL                  //
958      ...                   //
959      ***** PROC GETNXAFE *****//
960      ...                   //
961      BUILDFE
962      VALUE=BUILDFE(ITEM,PTR,WKPTR)
963      ...                   //
964      THIS ROUTINE BUILDS THE EXTERNAL WORK AREA FOLLOWING A
965      SUCCESSFUL FETCH.
966      ...                   //
967      ***** PROC GETNXAFE *****//
968      ...                   //
969      ***** PROC GETNXAFE *****//
970      ...                   //
971      ***** PROC GETNXAFE *****//
972      ...                   //
973      ***** PROC GETNXAFE *****//
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979      ***** PROC GETNXAFE *****//
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981      ***** PROC GETNXAFE *****//
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995      ***** PROC GETNXAFE *****//
996      ...                   //
997      ***** PROC GETNXAFE *****//
998      ...                   //
999      ***** PROC GETNXAFE *****//

```

```

969 DEFINE INTEGER RECURSIVE PROCEDURE BUILDFOE(ITEM, PTR, WKPTR)
970 WHERE POINTER ITEM, PTR, WKPTR TO BE
971 BEGIN
972   OWN REAL RTSIGNI
973   OWN REAL CUCHI
974   OWN POINTER TO, PTRI
975   OWN POINTER LE, PTRI
976   OWN POINTER LTM, PTRI
977   OWN POINTER HXS, PTRI
978   OWN INTEGER TEMPI
979   OWN INTEGER INDI
980   OWN INTEGER SVE, VERSI
981   INDI = 3
982   CUCHI = 3
983   IF VRSFEED, FFT INHIBITED
984     AND VERSION MISMATCH IS
985     RETURNED.
986   //
987   IF SVF, VRSFEED EOL ZERO
988     THEN GOTO NO, MATCH
989   //
990   TO, PTR = PTRI
991   ITEM, PTR = LE, PTRI
992   VERSI, PTR = SVE, PTRI
993   INDI = ITEM, PTR = ABS, I
994   IF INDI = 0
995     THEN INDI = INDI + ITEM, SIZEI
996   AFEVNI(ITEM, PTR) = INDI, ITEM, SIZEI
997   INDI = FCWTP(ITEM, PTR) = TYPE, ITEM, PTRI
998   IF INDI IS NOT
999     THEN REGN
1000   CTRWORD(ITEM, PTR) = CTRWORD(ITEM, PTR) + V, "FFFFFF"
1001   GOTO EXIT
1002   ELSE
1003     FIND, IE:
1004     IF TYPE, ITEM, PTR = NO, LTYPE
1005     THEN REGN
1006     IE, PTR = LE, PTR - ITEM, SIZEI
1007     GOTO, FIND, LEI
1008     FIND
1009     R = S, PTR = R, SPTR(LE, PTR)
1010     //
1011     FIND LE ASSOC WITH EVENT //
1012     *** LAT EVENT SEARCH *** //
1013     *** BACK UP POINTER *** //
1014     TRY AGAIN //
1015     *** LAT EVENT SEARCH *** //
1016     POINT AT HAS ITR //
1017     LOAD LATERAL EVENT, USED //
1018     BY ALL EVENTS,
1019     BUILD CTRWORD, C, BITS HAS
1020     BITS 3-11, HAS ITEM HAS
1021     BITS 21-23, TYPE IS STORED
1022     IN BYTE 5, ALL OTHER BITS
1023     ARE SET TO VALID EXCEPT
1024     BITS 16 WHICH IS EAPOF ARE
1025     BITS 12, 13 FOR HOLD AND VER
1026     EVENTS WHICH COME FROM
1027     AUX, CTL FIELD.
1028     //
1029     TEMP = C, BITS(ITEM, PTR) + LS, 3) + V,
1030     (C, LKWORD(ITEM, PTR) + LS, 17)
1031     + V, "50000"
1032     *** EACH A EAPOF INVALID // 00001102
1033     IF ITEM, PTR EOL FSTMT AND PPSST
1034     *** IF PRESENT POSITION IS NOT
1035     VALID, THE COUNTER-IN OF THE
1036     FIRST EVENT IS INVALID. //
1037     00001134

```

```

1026 THEN TEMP=TEMP+.V. "80000"
1027 CATWORD(TO,PIR)=TEMP;
1028 ECATW(IN,PIR)=INDX;
1029 EANYIN(TO,PIR)=NO; APTAG(TO,PIR) ... ONE OR THE OTHER //
1030 IF INX NEG LYP
1031 THEN AUX CTL(TO,PIR)=
1032   V(ITH,PIR) .A. "30";
1033 COPYR(TO,PIR)=AS,PIR;
1034 AFS(TO,PIR)=AFOF(TO,PIR)=AOFSEFI(TH,PIR) ... CALC AOF // 00001131
1035 CFTU(TO,PIR)=ESTAND(LE,PIR) ... SIMU(ABS,1) ... CALC OFTO // 00001015
1036 IF INX EOL LYP
1037 THEN BEGIN
1038   ... EXIT VE'S ***** // 00001004
1039   COPYW(TO,PIR)=ITM,PIR) ... VPAL,VPAL, AND ALTO // 00001007
1040   IF FOC,PIR EOL ITM,PIR ... FIXFLT FLAG VE AFTER FOC // 00001004
1041   THEN EVAL(TO,PIR)=TRUE; ... AS VPAL HERE IS INVAL ID. // 00001000
1042   GOTO EXIT1;
1043   ... ***** EXIT VE'S ***** // 00001130
1044   ... CMST, CRSU, AND ANYIN // 00001010
1045   INSI(TO,PIR)=SPEED(LE,PIR) ... RETURN IAS WORD. // 00001164
1046   MOISL(TO,PIR)=MOISL2(TO,PIR)=ZERO; ... FLANK OUT GARRAGE //
1047   POFSTO,PIR)=POFSFEI; ... SLOPE FOR NOPOFS & PAPAL //
1048   IF POFSEFTU,PIR)=EFFSTAT EOL BASEOFS;
1049   THEN BEGIN
1050     ... ***** BASE OFFSET ***** //
1051     POFIN(TO,PIR)=0.0; ... FOR STRTRASE & STRT9 //
1052     CCOH=CRSO+DILE,PIR)-CRSINU(LE,PIR); ... COURSE CHG //
1053     PTRSIGN=SIGN(CCOH);
1054     IF TEMPEOFTG(LE,PIR) EOL ENDRASE
1055     THEN POFSTO,PIR)=-POFSFE+RTNSIGN; ... ENDURASF //
1056     IF TEMP EOL INIENCF
1057     THEN BEGIN
1058       POFSTO,PIR)=
1059       -POFSFE+RTNSIGN+NSIN(AS(COCH));
1060       AOFSTO,PIR)=
1061       -POFSFE+NCOS(AS(COCH));
1062       ENDI;
1063       IF TEMP EOL SIMTBASE ON TEMP EOL STRT9 ... STRTRASE //
1064       THEN AOFSTO,PIR)=POFSFE; ... ON STRT9 //
1065       POFSEFTO,PIR)=TEMP; ... OVERWRITF FLAG COMPONENT //
1066       ENDI; ... ***** BASE OFFSET ***** //
1067       BUILDOR=CONTIN;
1068       IF VERSFE EOL SVE,VERS
1069       THEN GOTO RETURN1;
1070       BUILDOR=OVER;
1071       GOTO RETIN1;
1072       ENDI;
1073       ENCF;
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PHYS 001TILF6AZ



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... 3D/4D FLIGHT PLAN EDITOR UTILITY MODULE

THIS MODULE CONTAINS THE SPECIAL INTERFACE BETWEEN THE
FLIGHT PLAN EDITOR AND THE 3D/4D SYSTEM. IT CONTAINS
THE FOLLOWING PROCEDURES:

    ADD4U      ADD EVENTS TO FLIGHT PLAN
    REPLVD     REPLACE EVENTS IN FLIGHT
               PLAN & ENTER A BASE OFFSET
    ADDO4R     SPECIAL "DIRECT TO" INTERFACE
               FOR GOING DIRECT TO ORIGIN
               REPLACEMENT.
    REPO4R     SPECIAL "DIRECT TO" INTERFACE
               FOR "SUAL" "DIRECT TO".
    SCANBASE   FIND THE SPAN OF THE BASE
               OFFSET IN THE SET.
    BCLEAR     CLEAR ALL BASE OFFSET FLAGS
    CK90       CALC ANGLE ERROR FOR WIL-1)
    TOTLERR    CHECK TOTAL DISTANCE ERROR
    ABSCOUCH   CALC ABS VALUE OF COURSE
               CHANGES FM W(X) TO W(Y).

... GLOBAL SPAN ...
... FPE EXTERNAL INSERIS ...
... FPE INTERNAL INSERIS ...

REALS
REAL ARRAY
    ANGLE(12)
    ... ANGLE ERROR ARRAY FOR TEST//

PRESET ANGLE(0) TO ANGLE(12) = 0.01
EXTERNAL ANGLE(1)

REAL AREA
    TOINTER(12)
    ... TUT DIST ERROR FOR TESTING//

PRESET TOINTER(0) TO TOINTER(12) = 0.01
EXTERNAL TOINTER(1)

REAL
    C160,
    C90,
    C2,
    ORLOP1,
    CPT2,
    ... 180 DEGPES
    ... 90 DEGPES
    ... 2 DEGPES
    ... 1/PI
    ... 0.2 NAUTICAL MILES

```

```

57 EXTERNAL
58  CNEUP1,
59  DIGN,
60  P901
61
62 PRESET BEGIN
63  R2 = 0.011111111 // ... 2 DEGREES //
64  NMPT2 = 0.000016511 // ... 2/10 NAUTICAL MILE //
65
66 END1
67
68 ... ***** POINTERS *****
69
70 POINTER
71  PSTRT,
72  RSTRT,
73  RSTRT,
74  RSTRT,
75  RSTRT,
76  RSTRT,
77  RSTRT,
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80  RSTRT,
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114 POINTER PROC, WKPTRM
115 YDBE BEGIN
116
117 O=H POINTER WKPTRM
118 O=H POINTER O=STRT
119 O=H REAL ANG.ERR
120 O=H INTEGER SVERSFL
121 O=H INTEGER POF.S.FLG
122 O=H INTEGER I
123 I=SVERS.FLG
124
125
126 FOR I=0 STEP 1 UNTIL 2
127 DO
128   REGIN
129   TOI=TKN(I)=0.01
130   ANG=CK(I)=0.01
131   FLD:
132   REPLAN=EAQASE
133   WKPTR=WKPTRM
134   POF.S.FLG=POF.S.FLG(WKPTRM)
135   O=STRT=CONVFL(STABEVNU)
136   IF POF.S.FLG EQL BASEOFST
137   THEN REGIN
138   IF SVERSFL=VERSE EQL ZERO
139   THEN BEGIN
140     REPLAN=NOVER
141     GOTO RETURN
142   END
143   IF ANG.ERR=ANGLER(0)=CK90(D,STRT) GRT D2 ... CK W(1-1) //
144   THEN GOTO RETURN
145   IF TOILER(WKPTR,ANG.ERR,TOISTER(0)) ... CK DIST ERR //
146   THEN GOTO RETURN
147   ... CALC ANG COUMSE CHANG
148   ... FM W(1-1) TO W(1) //
149   ANG.ERR=ABS(ABSCCH(1+O,D,STRT)-D)
150   ANG=EM(1)=ANG.ERR
151   IF ANG.ERR GRT D2 ... CK ADSC COCH ANG ERR //
152   THEN GOTO TRIAU
153   IF TOILER(WKPTR,ANG.ERR,TOISTER(1)) ... CK DIST ERR //
154   THEN GOTO TRIAU
155   ... TOO BIG
156   ... ANGLE AT W(1) MUST BE 90
157   ... DEG +/- 2 DEG
158   IF ANG.ERR=ANGLER(2)=CK90(D,STRT+1TH,SIZE) ... CK90 CANS //
159   GRT D2
160   ... W(1) INSTEAD OF W(1-1) //
161   THEN GOTO TRIAU
162   IF TOILER(WKPTR,ANG.ERR,TOISTER(2)) ... CK DIST ERR //
163   THEN GOTO TRIAU
164   ... TOO BIG
165   ... SATISFIES P-WAYPOINT,
166   ... BASE-OFFSET GEOMETRY
167   ... CLEAR FLT OF OLD OFFSETS //
168   ... FLAG W(1) AS END90 //
169   OFTGIPREV,VALUE(0,STRT)=STRT90 ... FLAG W(1-1) = START90 //
170
171   SVERSFL=SVERSFL+1
172   POF.S.FLG=POF.S.FLG
173   POF.S.FLG=POF.S.FLG(WKPTR)
174   FIVEIT(STABEVNU,NOITEMS)
175   ... CALC VP=VAIVP/NOITEMS
176   ... AND OFTO COMPONENTS //
177
178 CLOSE:
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171      GOTO MEXIT;
172      ... TWO-POINT BASE OFFSET
173      GEOMETRY WAS NOT SATISFIED.
174      THIS SECTION CHECKS THREE-
175      POINT BASE OFFSET
176      GEOMETRY.
177      //
178
179      ... CALC ABS COURSE CHANGE ERR
180      FM #11) TO #11+1).
181      //
182      ANG. ERR=ABS(ABS(COCH(1),D,STRT))-390);
183      ANG. ERR(1)=ANG. ERR;
184      IF ANG. ERR GRT D2
185      THEN GOTO RETURN;
186      IF TOTLERK(PNTR,ANG,ERR,TOISTER(1)) ... CR DIST ERR//
187      THEN GOTO RETURN;
188      ... CALC ABS COURSE CHANGE ERR
189      FM #11-1) TO #11+1).
190      //
191      ANG. ERR=ABS(ABS(COCH(1),D,STRT))-390);
192      ANG. ERR(2)=ANG. ERR;
193      IF ANG. ERR GRT D2
194      THEN GOTO RETURN;
195      IF TOTLERK(PNTR,ANG,ERR,TOISTER(2)) ... CR DIST ERR//
196      THEN GOTO RETURN;
197      ... TWO-POINT BASE OFFSET
198      GEOMETRY SATISFIED
199      ... CLEAR ANY OLD OFFSET
200      ... IF THERE IS NOT A CASEKIT
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228 REPLACED=REPLACE(STABEVNO,SPABEVNO,NOITEMS,PROC,WKPTR) I
229 END I
230 GOTO RETURN I
231 REPLACED=CHTRI
232 GOTO RETURN
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285 1 = FLIP:
286 ENDO:
287
288 STATE=INIT:
289 LE.PTR = ADS.1-ITM.SIZE:
290 BSTR = SCHEFFILE.PTR.LMSK:
291
292 ... INITIALIZE SWITCH //
293 ... INIT SEARCH POINTER //
294 ... INITIALIZE B-OFFSET STMT //
295
296 LE.PTR = SCHEFFILE.PTR.LMSK:
297 IF LE.PTR EQL NULL //
298 THEN BEGIN
299   SCHEFFILE=END:
300   GOTO RETURN:
301 ENDO:
302
303 ... NO BASE OFFSET ***** //
304 ... RETURN NEXT //
305
306 ... NO BASE OFFSET ***** //
307
308 IF STATE EQL INIT
309 THEN BEGIN
310   IF NOT(IGILE.PTR) NEO NOPOFS
311   THEN BEGIN
312     STATE=FLIP:
313     GOTO LOOP:
314   END:
315   BSTR = LE.PTR:
316   GOTO LOOP:
317 ENDO:
318
319 BSTOP = LE.PTR:
320 IF NOT(IGILE.PTR) NEO NOPOFS
321 THEN GOTO LOOP:
322 SCHEFFILE = BSTR:
323 GOTO RETURN:
324 ENDO:
325
326 ... ***** PROC SCHEFFILE ***** //
327
328 ... ***** PROC SCHEFFILE ***** //
329
330 BCLEAR:
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199 ... THIS PROC FINDS THE LF
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201 ... AT IN THE FET. THUS IT IS
202 ... A BACKWARD SEARCH ROUTINE.//
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APPENDIX B  
Program Listing of the Speed Profile  
Algorithm



Donnerstag, 8. April 2026

1.3.3.7.2

\*\*\*\*\* EXTERNAL DATA STRUCTURE \*\*\*\*\*

1) PREFIX	LIBRARY FILE	DECLARATION	DESCRIPTION
		SYMBOLIC NAME	TYPE

B-2

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57	ALTD	REAL COMPONENT	SPECIFIED WAYPOINT TO THE TO-WAYPOINT.
58			FLIGHT PLAN EDITOR FLIGHT PLAN
59			COMPONENT USED TO RECORD
60			ALTITUDE FOR A VERTICAL
61			EVENT.
62	IASH	REAL COMPONENT	FLIGHT PLAN EDITOR FLIGHT PLAN
63			COMPONENT USED TO RECORD
64			INDICATED AIRSPEED LEITS WAGE
65			VIA THE SPECIF PART.
66	IASF	INTEGER COMPONENT	FLIGHT PLAN EDITOR FLIGHT PLAN
67			COMPONENT USED TO RECORD IAS
68			TYPE.
69	PIAS	SYNONYM	CODE RETURNED TO THE IASF
70			COMPONENT THAT INDICATES A
71			PILLOT-DEFINED IAS.
72	PROOUTF	SYNONYM	CODE RETURNED IN THE IASF
73			COMPONENT THAT INDICATES THAT
74			THE IAS ENTRY FOR THE GIVEN
75			WAYPOINT IS IDENTICAL TO THAT
76			OF THE PRECEDING WAYPOINT IN
77			THE WAYPOINT.
78	PROOM	SYNONYM	CODE RETURNED TO THE IASF
79			COMPONENT THAT INDICATES THAT
80			THE GIVEN IAS IS PART OF A
81			DECREASING PROFILE.
82	PROP	SYNONYM	CODE RETURNED TO THE IASF
83			COMPONENT THAT INDICATES THAT
84			THE GIVEN IAS IS PART OF AN
85			ASCENDING PROFILE.
86			
87			
88			
89			
90			
91	WMA1	POINTER	CONTAINS ADDRESS OF WORK AREA
92			USED BY THE CDM CHANNEL.
93	ZILCH	INTEGER PROCEDURE	NULL PROCEDURE USED TO SATISFY
94			PROCEDURE ARGUMENT REQUIREMENTS
95			FOR CASES WHERE SPECIAL DEFAULT
96			LOGIC IS NOT REQUIRED.
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114	VALID	SYNONYM	PERFORMED.
115			VALUE ASSIGNED TO INTEGER FLAG
116	TCOMF	INTEGER	TO INDICATE VALID STATUS.
117			VALIDITY FLAG THAT IS ASSIGNED
118			A VALID STATUS BY SENSOR
119			WHENEVER SPECIFIC PROFILE
120			COMPUTATIONS ARE UPDATED.
121			TCOMF IS ASSIGNED AN INVALID
122			STATUS BY THE TIME CONTROL
123			PROCEDURE WHENEVER THE
124			CORRELATION COMPUTATIONS ARE
125			PERFORMED.
126	5) AFOLIB INSERT FILE	DECLARATION	DESCRIPTION
127	SYMBOLIC NAME	TYPE	
128			
129	•CMT	PROCEDURE	SUPERVISORY SOFTWARE ROUTINE
130			THAT IS CALLED TO YIELD OWN
131			CHANNEL TIME FOR CLAMP
132			CYCLE.
133	6) MATHPACK INSERT FILE	DECLARATION	DESCRIPTION
134	SYMBOLIC NAME	TYPE	
135			
136	RLMTF	REAL	ROUTINE THAT LIMITS THE FIRST
137		PROCEDURE	ARGUMENT TO THE MAGNITUDE
138			GIVEN BY THE SECOND ARGUMENT.
139	RMAXF	REAL	ROUTINE WHOSE RETURN ARGUMENT
140		PROCEDURE	IF THE LARGER OF TWO VALUES
141			SPECIFIED AS INPUT ARGUMENTS.
142	R711F	REAL	ROUTINE WHOSE RETURN ARGUMENT
143		PROCEDURE	IS THE SMALLER OF TWO VALUES
144			SPECIFIED AS INPUT ARGUMENTS.
145	ABS	REAL	PROCEDURE THAT DETERMINES THE
146		PROCEDURE	MAGNITUDE OF A GIVEN INPUT
147			ARGUMENT.
148	RROOT2	REAL	PROCEDURE THAT DETERMINES THE
149		PROCEDURE	SQUARE ROOT OF A GIVEN INPUT
150			ARGUMENT.
151	7) NTARI611 INSERT FILE	DECLARATION	DESCRIPTION
152	SYMBOLIC NAME	TYPE	
153			
154	ADHD	POINTER	POINTER TO ARRAY WHERE SENSOR
155			INPUT FOR HEADING AND AIR DATA
156			INFORMATION IS RECORDED.
157	TAS	REAL	ADHD COMPONENT USED TO RECORD
158		COMPONENT	SENSOR INPUT FOR TRUE AIRSPEED.
159	DELV	REAL	ADHD COMPONENT USED TO RECORD
160		COMPONENT	SENSOR INPUT FOR LAS INSTRUMENT
161			ERROR.
162	WZHZ	REAL	REAL PARAMETER USED TO RECORD
163			PRESENT ESTIMATE OF AIRCRAFT
164			ALTITUDE.
165			
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171 ***** INTERNAL DATA STRUCTURE *****
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COMMENT
INTEGER
FIRSTASR,
  AVEVJ,
  FROMEVRD,
  LEVAT,
  SAVE,
  LCAT,
  GHEITM,
  FIRST,
  LAST,
  FIRST,STATUS :

  ... STATUS OF IAS COMPONENT FOR WPT
  TAGGED AS FIRST FOR A GIVEN PROFILE
  ... ABS EVNT NO. OF JTM LAT EVENT
  ... SPECIFICS LATERAL FROM-EVENT NUMBER
  ... SPECIFICS LATERAL EVENT NUMBERS
  ... IAS DISPLAY CLEAR PARAMETER
  ... FLAG TO INDICATE IF ADJACENT KPTS
  HAVE PIAS
  ... ONE ITEM IS TO BE REPLACED
  ... EVENT NO. FOR INITIAL SPEED CONTROL
  ... WAYPOINT OF A GIVEN PROFILE
  ... EVENT NO. INDEX FOR FINAL SPEED-CONTROL
  ... WAYPOINT OF A GIVEN PROFILE
  ... PARAMETER USED TO RECORD EXISTENCE OF
  ANOTHER SPEED PROFILE IN THE REMAINING
  FLIGHT PLAN

REAL DECLARATIONS
COMMENT
REAL
ACTAS,
ACTIASFR,
ACALT,
F,
FIRSTASR,
LASTASR,
CFTOFRST,
CFTOLAST,
PREVUEFO,
CFTOU,
PREVIASR,
DISTO,
JIASR,
KALT,
PREVSCALE,
PREVSP2,
PREVSP,
PREV,
CJ,
CJLCTST,
FL,
AVEV,
Tc,
LEP :

  ... AIRCRAFT TRUE AIR SPEED
  ... IAS INSTRUMENT ERROR
  ... AIRCRAFT ALTITUDE
  ... AIRCRAFT OR WPT ALTITUDE
  ... SAVES THE IAS VALUE OF *IFRST)
  ... SAVES THE IAS VALUE OF *ILAST)
  ... DIST FROM THE TO-EVENT TO *IFRST)
  ... DIST FROM THE TO-EVENT TO *ILAST)
  ... DIST BETWEEN TO-EVENT AND *TO-1)
  ... DIST BETWEEN TO-EVENT AND *TO)
  ... IAS OF *TO-1)
  ... DIST BETWEEN *IFRST) AND *TO)
  ... TEMP VAR TO HANDLE IAS CALC OF *TO)
  ... ALTITUDE PROPORTIONALITY CONSTANT
  USED TO CONVERT IAS TO TAS
  ... KALT SCALING FACTOR
  ... PREVIASR SCALED
  ... ALONG THE DIST FROM *IFRST) TO *ILAST)
  ... VEL CHNG BETWEEN *TO-1) AND *ILAST)
  ... ALONG THE DIST BETWEEN *TO-1) AND *TO)
  ... ALONG THE DIST BETWEEN *TO) AND *ILAST)
  ... TIME TO FLY FROM *TO-1) TO *ILAST)
  ... AT RATE OF *IFRST)
  ... AVE VEL REQUIRED FOR A LINEAR SPEED
  PROFILE BETWEEN *TO-1) AND *ILAST)
  ... TIME TO FLY FROM *TO-1) TO *ILAST)
  ... WITH CONSTANT VELOCITY OF AVEV
  ... LIST TO REALIZE, ALL COMB OF TALL AT
  ... DATE OF *IFRST)

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285 CAN REAL PREVIOUSLY OCCUR DELIST, JAS, S, CIST, J
286 IF COVER, NEG VALID
287 ... IF FLIGHT PLAN HAS BEEN MODIFIED
288 SINCE THE LAST SPEED PROFILE
289 COMPUTATION, THEN UPDATE SPEED
290 PROFILE, OTHERWISE RETURN,
291 //
292 THEN GOTO VERBULATE
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342      THEN GOTO VERUPDATE ;
343      PRST=-1 ;
344      LEVTIME=1 ;
345      IF PRSTIAS=IAS(ARPT) NED NOIAS
346      ... IF FROM-EVENT HAS AN AIRSPEED
347      ... ASSOCIATED WITH IT
348      ... THEN RPL IAS
349      THEN PRSTIAS=PIAS
350
351      CURRENT FROM-WAYPOINT HAS NO IAS. SEARCH FOR FIRST PILOT-
352      ENTERED IAS AND ASSIGN THIS TO THE FROM-WAYPOINT
353
354      LUSE
355      BEGIN
356      WHILE GETTIME(FLSK,LEVTIME,ARPT) EQL GORTN
357      AND PRSTIAS=IAS(ARPT) NED PIAS
358      DO LEVTIME=LEVTIME+1 ;
359      END ;
360      IF PRSTIAS LNC PIAS
361      THEN GOTO VERUPDATE ;
362      PRSTIAS=IAS(ARPT) ;
363      IF GETTIME(FLSK,LEVTIME,ARPT) NEQ GORTN
364      ... GET FROM-EVENT INTO WORK AREA
365      THEN GOTO VERUPDATE ;
366
367
368      COMMENT UPDATE FLIGHT PLAN TABLE FOR THE FROM-WAYPOINT. INITIALIZE
369      PARAMETERS FOR FIRST SPEED PROFILE COMPUTATION
370
371      IAS(ARPT)=PRSTIAS ;
372      IAS(ARPT)=PIAS ;
373      IF REFAC(ARPT,LEVTIME,ARPT,LEVTIME,ARPT) NEQ NORTH
374      ... (DEFINED IN
375      ... THE REAL
376      ... DECLARATIONS ABOVE
377      ... START SEARCH FOR NEXT ENTERED SPEED
378      ... WITH EVENT AFTER TO-EVENT
379
380
381      COMMENT FIRST VALID LOOP.
382      INITIALIZE PARAMETERS FOR PREVIOUS PROFILE
383
384      PRST-STATUS=VALID ;
385      WHILE PRST-STATUS EQL VALID
386      ... VALIDATE PRST-STATUS. CONCLUSION
387      ... THIS LOOP CONSTRUCTS EACH PROFILE.
388      ... FIRST IT MUST FIND THE NEXT SPEED
389      ... CONTROL WAYPOINT.
390
391      DO
392      BEGIN
393      PREVIOUS=OFT(ARPT) ;
394      PREVIOUS=PRSTIAS ;
395      ... SET ADJACENT SPEED CONTROLS CHECK
396
397
398      COMMENT NEXT SPEED LOOP

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399      SCAN FLIGHT PLAN FOR LAST WAYPOINT OF GIVEN PROFILE.
400
401      GLNEXT,SPEEDWPT :
402      IF GETTIME(LASKEVLEWJ,MPT) NEQ GURTH ... GET NEXT EVENT //
403      THEN GOTO VERUPDATE :
404      IF IASFEWPT) ME PIAS ... YES, IS IT A SPEED CONTROL WPT ? //
405      YES :
406      BEGIN :
407      LCNT=1 :
408      LEVWJ=LEVWJ+1 :
409      GOTO GLNEXT,SPEEDWPT :
410      END :
411
412      CURRENT END OF NEXT SPEED LOOP
413      UPDATE PARAMETERS RELATED TO W(LAST)
414
415      LAST, ASKEVLEWJ,MPT) : ... SAVE LAST SPEED CONTROL VALUE //
416      IASFEWPT) ME PIAS : ... SAVE ONE LESS THAN ACTUAL AOS PV NO. //
417      THIS IS A RESULT OF BEING USED //
418      WITH GELWAVE //
419      PFTOLAST=OFTO(WPT) : ... DEFINED IN THE //
420      PRODESTOFTO(LAST-OFTOFRST) : ... REA, DECLARATIONS //
421
422      COMMENT BYPASS COMPUTATIONS FOR GIVEN PROFILE IF SUCCESSIVE WPTS ARE
423      TAGGED AS SPEED-CONTROL WPTS
424
425      IF LCNT EQ 0 ... DO WE HAVE SUCCESSIVE LATERAL EVENTS //
426
427      THEN GOTO NEXTPROFILE : ... DEFINED AS SPEED CONTROL WPTS ? //
428      IF FIRSTIAS EQ LASTIAS ... ARE SPEEDS W(FIRST) AND W(LAST) EQUAL ? //
429      THEN :
430
431      COMMENT SAVE SPEED LOOP.
432      W(FIRST) AND W(LAST) HAVE THE SAME SPEED. ASSIGN THIS SPEED
433      TO ALL INTERMEDIATE PROFILE WPTS
434
435      BEGIN :
436      FOR ABWJ=FIRST+1 STEP 1 UNTIL LAST-1
437      ... ASSIGN FIRSTIAS TO IAS COMPONENT //
438      ... AND QUOTE TO IAS COMPONENT //
439      ... FOR ALL LAT EVENTS BETWEEN //
440      FIRST AND LAST
441      IF GETTIME(LASKEVLEWJ,MPT) NEQ GURTH :
442      THEN GOTO VERUPDATE :
443      IF IASFEWPT) ME PIAS ... IS IT A LAT EVENT ? //
444      YES :
445      BEGIN :
446      IASFEWPT) ME PIAS : ... ASSIGN SPEED TO IAS //
447      IASFEWPT) ME PIAS : ... ASSIGN QUOTE //
448      IF REPLACE(LASKEVLEWJ,MPT),ABWJ,MPT),OFTO(LAST-OFTOFRST) :
449      THEN GOTO VERUPDATE :
450      END :
451
452      END :

```

```

END
COMMENT END OF SAVE SPEED LOOP.
ELSE

COMMENT VELOCITY CHANGE LOOP.
W(FIRST) AND W(LAST) HAVE DIFFERENT SPEEDS. ALTITUDE ALL
EVENTS BETWEEN W(FIRST) AND W(LAST) AND ASSIGN APPROPRIATE
PROFILE SPEED TO THE LATERAL EVENTS.

FOR AHEAD=FIRST+1 STEP 1 UNTIL LAST-1
DO
  BEGIN
    IF GETXAXF(LA*SK,AHEAD,WAKPT) NEQ GUNT4
      THEN GO TO VUPDATE ;
    IF ECXTYP(WAKPT) EQL VTYP
      THEN
        ... IS THIS A VERT EVENT ?
        ... Y S. SET HZ .
  END

COMMENT VERT LOOP.
VERT IS OF VERTICAL TYPE. UPDATE ALTITUDE THAT IS REQUIRED
FOR IAS TO IAS CONVERSION.

  UPGID
  IF NOT TOWE(WAKPT) ... IS IT ALSO A TO-EVENT
  THEN, HZ=HZ+Z ... FOR TO-EVENT HZ=HACRAFT ALTITUDE//
  ELSE HZ=ALTU(WAKPT) ;
  ... OTHERWISE HZ=PILOT ENTERED ALT

END

COMMENT END OF VERT LOOP

COMMENT LATERAL LOOP.
EVENT IS OF LATERAL TYPE. UPDATE PROFILE VELOCITY.

ELSE
  IF ECWTYP(WAKPT) EQL LTYP ... IS THIS A L. EVENT ?
  NOTICE THAT EVENTS OTHER THAN
  LAT AND VERT ARE BYPASSED //
THEN
  BEGIN
    DTOTJ=DETU(WAKPT) ;
    CDTOTJ=PVELVDFIO ;
    DELDSTE=DTCLAST-DTTOJ ;
    DIST=PCPST-BELD-ST ; ... W(FIRST) TO W(LJ)
    WALTERATE(CACTAS-VL MI/ACIASERN)*KALISCHE.*MZ*ARTAS-WTHR) ;
    WALTERATE(CALIASRN) ;
    WALTERATE(EMTIME(WAKPT,.15),.10) ;
    ... LIMIT ONLY TO THE INTERVAL
    RETURN .1 AND .10 ( IN THE REAL
    WORLD THIS IS EQUIVALENT TO
    .000015 TO .000010 )
  END

DOVE = JANT.FSM - PREVIEWAR ;

```



```

513 T1=ABS(VELL-MINRATE) :
514 AVEV=5*(PREVIASTR+LASTIASTR)/(MAX(1,(KALT-M2)/KALTSCALE)) :
515 T2=(DELJST+D2)/AVEV :
516
517 IF T2 LFO 11 ... IF T2 LEQ 11 THEN THE VELOCITY
518 CHNG BETWEN W(J-1) AND W(LAST)
519 REQUIRES A VEL CHG/ RATE GT OR EQL
520 TO MINRATE //
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T1=ABS(VELL-MINRATE) :  
 AVEV=5\*(PREVIASTR+LASTIASTR)/(MAX(1,(KALT-M2)/KALTSCALE)) :  
 T2=(DELJST+D2)/AVEV :  
 IF T2 LFO 11 ... IF T2 LEQ 11 THEN THE VELOCITY  
 CHNG BETWEN W(J-1) AND W(LAST)  
 REQUIRES A VEL CHG/ RATE GT OR EQL  
 TO MINRATE //  
 //  
 COMMENT LINEAR LOOP.  
 CALCULATE A VELOCITY, JIASP, THAT IS BASED ON A LINEAR SPEED  
 PROFILE BETWEEN W(J-1) AND W(LAST).  
 THEN  
 BEGIN  
 PREVIASTR=PREVIASTR+PREVIASTR :  
 JIASP=K0012(PREVIASTR+(LASTIASTR-PREVIASTR)\*  
 D2/(DELJST+D2)) :  
 ... CALCULATE VEL FOR W(J) BASED ON  
 LINEAR PROFILE BETWEEN W(J-1)  
 AND W(LAST) //  
 IASP(W(J))=JIASP : ... SET SPEED COMPONENT TO NEW SPD //  
 IF JIASP LES PREVIASTR ... IF SPEED DECREASES FROM  
 W(J-1) TO W(J) //  
 THEN IASP(W(J))=PREVIASTR //  
 ... THEN MAKE IASP=APPROX DOWN //  
 ELSE IASP(W(J))=PREVIASTR :  
 ... ELSE EQUAL TO APPROX UP //  
 END  
 COMMENT END OF LINEAR LOOP  
 ELSE  
 COMMENT MINIRAF LOOP.  
 DETERMINE DPP, THE DISTANCE REQUIRED TO REALIZE A VELOCITY  
 CHANGE OF DVEL AT RATE OF 40 KTS/MIN.  
 BEGIN  
 DPP=511\*AVEV : ... DIST REQUIRED TO FLY AT MINIRAF  
 TO REACH W(LAST) //  
 IF DELJST GEQ DPP ... IF DPP LT DIST FROM W(J) TO W(LAST)  
 THEN NO CALCS FOR THIS WPT. //  
 THEN  
 BEGIN  
 COMMENT NO CHANGE IN ...  
 VELOCITY WPT IS LESS THAN MINIRAF. ASSIGN W(J) THE SPEED  
 OF W(J-1).  
 IASP(W(J))=PREVIASTR :

AD-A056 842

ROCKWELL INTERNATIONAL CEDAR RAPIDS IA COLLINS AVION--ETC F/G 1/5  
3D/4D AREA NAVIGATION SYSTEM DESIGN, DEVELOPMENT AND IMPLEMENTA--ETC(U)  
JUN 77 J M BRUCKNER, F B BENSON DOT-FA72WA-3123

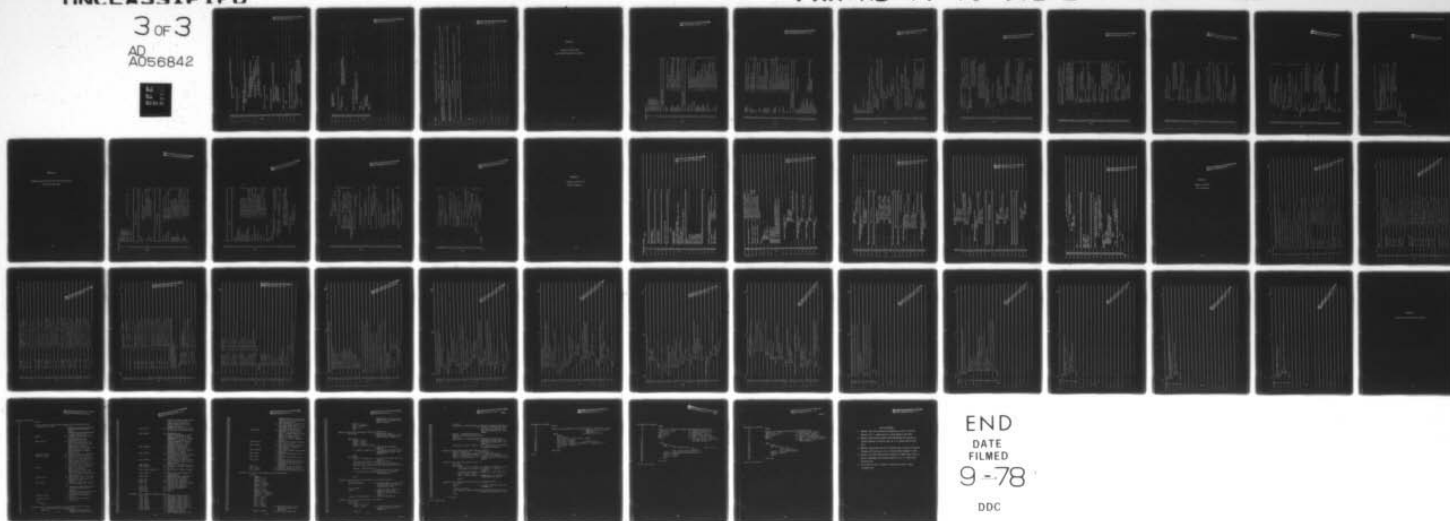
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FAA-RD-77-79-VOL-2

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3 OF 3

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570      ... ASSIGN SAVE SPEED AS PREVIOUS WPT //
571      IASF(WKPT)=PRODUCE !
572      END
573
574      CORRECT END OF NO CHANGE LOOP
575
576      ELSE
577
578      COMMENT MINRATE ZONE LOOP.
579      CALCULATE A VELOCITY FOR W(J) THAT IS BASED ON A 40 KT/MTN
580      VELOCITY RATE BETWEEN W(J-1) AND W(J).
581
582      BEGIN
583      PAVISK2=PREVIAIR*PREVIAIR !
584      JTAIR=PRODOT2(PAVISK2+LASTIAIR*LASTIAIR-PRVIAIR*PRVIAIR) !
585      (OPP-VELCIST)/DPP !
586
587      IASK(WKPT)=JTAIR ! ... CALC SPEED AT W(J)
588      IF JASK LES PREVIAIR ... ASSIGN NEW SPEED
589      IF JASK LES PREVIAIR ... IF SPEED DECREASES FROM
590      W(J-1) TO W(J)
591      THEN IASF(WKPT)=PRODOWN ... AND EITHER ARROW DOWN //
592      ELSE IASF(WKPT)=PROPUP ! ... OR ARROW UP //
593      END !
594
595      COMMENT END OF MINRATE ZONE LOOP
596
597      END !
598
599      CORRECT END OF MINRATE LOOP.
600
601      IF REPLACE(AREVNO(WKPT),AREVNO(WKPT),ONEIM,2ILCH,WKPT)
602      THEN GOTO VERHUPATE !
603
604      PREVIAIR=IASR(WKPT) !
605      PREVVEFT=DUFTO(WKPT) !
606      END !
607
608      COMMENT END OF LATERAL LOOP.
609
610      END !
611
612      CORRECT END OF VELOCITY CHANGE LOOP.
613
614      COMMENT PRIME PARAMETERS FOR NEXT PROFILE COMPUTATION
615
616      ALXTPROFILE !
617      ... RECEIPT PARAMETERS FOR NEXT PROFILE COMPS
618      ... WILL START SEARCH FOR NEXT SPEED
619      ... CONTROL WPT WITH THE LAT. EVENT
620      ... FOLLOWING THE LAST SPEED CONTROL
621      ... MAKE PRST PARAMETERS
622      PRST=LAST !
623
624

```



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627  OFUPRST=DEFTOAST :
628  FFSIIASRELASTASK :
629  FND :
630
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632
633  CURRENT END OF FIRST VALID LOOP
634
635  VERUPDATE $
636  COMPPE=INVALID : ... INVALIDATE COMPPE TO INDICATE THAT
637  SLED PROFILES HAVE BEEN UPDATED FOR
638  EXISTING FLIGHT PLAN.
639  END :
640
641
642
643
644  DEFINE REAL PROCEDURE SIGN(X)
645  ..
646  THIS PROCEDURE TAKES THE SIGN OF A NUMBER .
647  IE SIGN(-5) = -1, SIGN(10) = 1 .
648  //
649  WHERE
650  REAL X :
651  TURE
652  BEGIN
653  IF X GT 0.
654  THEN SIGN=MAX4
655  ELSE SIGN=MIN4
656  END :
657  END FINI

```

NEWS

COLLINS RADIO COMPANY NEWS PROCESSOR LEVEL 1.0 THURSDAY, OCT 23, 1975

MULTI-TPM OCT 22 1975

A NEW TPR PROCESSOR NOW ON THE SYSTEM WILL ALLOW MULTIPLE COPIES TO MULTIPLE SITES. MAXIMUM SITES=3, MAXIMUM COPIES PER SITE=9.  
EX-AMPLE \*\*\*\*\* 7/27PM MMS011/3,MMS011/2,P2/5  
WOULD SEND 3 COPIES TO REMOTE MMS011, 2 COPIES TO REMOTE MMS011, AND 5 COPIES TO THE UNISITE 1104 PRINTER IN BUILDING 400.

NEW-AND-LINE OCT 22 1975

EFFECTIVE IMMEDIATELY NO DEMAND USER WILL BE ALLOWED TO SIGN ON WITH MORE THAN 15 MINUTES ESTIMATED WAKE TIME DURING NIGHT SHIFT.  
NIGHT SHIFT IS 8:00 AM TO 6:00 PM DALLAS TIME.

1100B-OUTAGE OCT 22 1975

THE U-1708 WILL BE OUT OF SERVICE FROM 0400 P.M. UNTIL 1200 P.M. SATURDAY OCTOBER 25, 1975 FOR SYSTEM PROGRAM TEST.

OFFHOURS-INDEX AUG 29 1974

INDEX OF SOFTWARE AVAILABLE ON THE COLLINS U-1108 SYSTEM - FOR LISTING INSERT .. '77 RELEASE SOFTWARE-INDEX' IN YOUR NEWSSTREAM ....

B-14

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APPENDIX C

Program Listing of the  
Base System Time Control Algorithm



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40=CRAWFILL.TL00176A2

```

1 BEGIN
2 .INSTRUMENT DEF611 :
3 .INSTRUMENT STRUCTIST :
4 .INSTRUMENT CONTROLS :
5 .INSTRUMENT DATA611 :
6 .INSTRUMENT AEDLIS :
7 .INSTRUMENT KATIPACK :
8 .INSTRUMENT KATIPACK611 :
9 .EXTERNAL GATSF :
10 .EXTERNAL CBRU :
11
12 .....
13 INTELIGENT DECLARATIONS
14 .....
15
16 INTRINSEIC
17 CBRU,
18
19 .....
20 ... AIRCRAFT TYPE SPECIFIED BY LINK EDIT
21 CBRU = 0 FOR G-1
22 = 1 FOR C-860
23
24 ... AIRCRAFT TYPE SPECIFIED BY LINK EDIT
25 CBRU = 0 FOR G-1
26 = 1 FOR C-860
27
28 ... AIRCRAFT TYPE SPECIFIED BY LINK EDIT
29 CBRU = 0 FOR G-1
30 = 1 FOR C-860
31
32 .....
33 REAL DECLARATIONS
34 .....
35
36 REAL
37 VCUMAX,
38 VLOMAX,
39 VLOMAX,
40 VLOMAX,
41 VLOMAX,
42 VLOMAX,
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57 TIGNOM.
58 CULCPRVL,
59 WALK.
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61 TASPRLV,
62 TASPJ,
63 UV,
64 PLFL,
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66 GP,
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68 WAKTO,
69
70 VU,
71 VP,
72 VNGV,
73 TIGCOM,
74 KSCALL,
75 CATP,
76 CHKZ41,
77
78 P,
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80 WIGOP,
81
82 PLGTAN.5,
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84 GNSICOM,
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87 ORLDVNP1,
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89 TZ,
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91 NPP :
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114 PMLVDFO=0.0. ;
115 KALTSCL=1.1 ;
116 KVAL=0 ;
117 KAU ;
118 KX=0 ;
119 KVL=0.0 ;
120 FWD ;
121 PLANE PROCEEDURE FINISH
122 TIME
123 BODY
124 ONA POINTER WANT ;
125 ONA INTRON ADVU ;
126 ONA REAL ACTAS=DELT.ITTOW=V.TAS*REV.TI.T2*KALT.VGROW ;
127 GRIP 153 GRT ;
128 WAPTRAL ;
129 IF .CLOCK=0-FALCLOCK LFS 1LNSC
130 AND 1CGR NEW VALU
131 THEN GOTO EGGSAT ;
132 FALCLOCK=ALCLOCK ;
133 TIME=INVALID ;
134
135
136
137 IF VCOMI=117 SWITCH GRT 0
138 THEN IVOMI
139 ELSE
140 IF 1ASPLAHD=0 GRT 0
141 THEN 1V1AS
142 ELSE
143 IF 1ASPLAHD 142ZF) GRT 0
144 THEN 1VALT
145 ELSE 142DATA) NEW 142DATA
146
147 THEN GOTO EGGSAT ;
148
149
150
151
152
153 VCOMI*MAX = IF LFC C880 GRT 0 THEN VCOMI*MAX.C880
154 ELSE VCOMI*MAX.GI ;
155
156
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171 ... INITIALIZE NECESSARY PARAMETERS
172 ... PREVIOUS(LASER) : ... INIT. OVERLASH TO LASR COMPONENT
173 ... OF FROM-EVENT
174 ... PREVIOUS(LASER) : ... INIT. PREVIOUS TO DIST FROM TO-EVENT
175 ... TO THE FROM-EVENT
176 ... START WITH ABSOLUTE EVENT NUMBER 0
177 ... TIME TO GO = 0.0
178 ... CUMULATIVE(CRS) = CRS(LASER)
179 ... VTIME = 0
180 ... IF THERE IS NO TFX ENTERED THEN
181 ... TO-EVENT IS TREATED AS TFX. SO WHEN
182 ... TO-EVENT BLOCK IS EXECUTED WE SET
183 ... VTIME = TFX. IF THERE IS NO TFX THEN
184 ... VTIME IS INVALID
185
186 ... BEGIN CALCULATING (CALCULATE TIME TO GO) BLOCK
187 ... THIS BLOCK DETERMINES THE ACTUAL (NOMINAL) TIME
188 ... THE AIRCRAFT WILL USE TO FLY FROM ITS PRESENT
189 ... POSITION TO THE TIME-FIX. ITGROW IS DETERMINED
190 ... AND SAVED FOR EACH LEG UP TO THE TIME-FIX. IF
191 ... THERE IS NO TFX THE TO-EVENT IS TREATED AS ONE
192 ... WHILE APTID(LASER) NEW TFX AND
193 ... GETTAX(LASER, APTID(LASER)) EOL GOTOIN
194 ... AND VTIME IS VALID
195 ... DO
196 ... BEGIN
197 ... BEGIN LATERAL EVENT BLOCK
198 ... CALL TITGROW FOR THE GIVEN LEG
199 ... IF ECR(LASER) EOL LTP
200 ... AND LASR(LASER) NEW NOIAS
201 ... THEN
202 ... BEGIN
203 ... NOTE THAT END-OF-CONTINUITY EVENTS ARE PASSED
204 ... IF ELAT(LASER) ... IF THE PRESENT LATERAL EVENT HAS
205 ... AN INVALID LAT-LONG SET COMPARED
206 ... VELOCITY AND TIMEFROM FLAGS INVALID
207 ... THEN
208 ... BEGIN
209 ... VTIME = TIMEFROM + INVALID
210 ... GOTO LOGSAT
211 ... END
212 ... UREF(TO(LASER)) = PREVIOUS(TO : ... W(J-1) TO W(J)
213 ... PREVIOUS(TO(LASER)) : ... ATTO TO W(J)
214 ... WATK = (CALCULATED(CRS) * ACOS(CRS(LASER))) :
215 ... WIND COMPONENT AT W(J)
216 ... WIND COMPONENT AT W(J)
217 ... WIND COMPONENT AT W(J)
218 ... WIND COMPONENT AT W(J)
219 ... WIND COMPONENT AT W(J)
220 ... WIND COMPONENT AT W(J)
221 ... WIND COMPONENT AT W(J)
222 ... WIND COMPONENT AT W(J)
223 ... WIND COMPONENT AT W(J)
224 ... WIND COMPONENT AT W(J)
225 ... WIND COMPONENT AT W(J)
226 ... WIND COMPONENT AT W(J)
227 ... WIND COMPONENT AT W(J)

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228 I1=ABS(DV*MINRATE) : ... TIME TO FLY REQUIRED BY AT
229 ACCELERATION OF 1/MINRATE
230 AVLEVO=0.5*(IASPREV+TASJ)*AIR :
231 T2=ABS(DV/AVEV) : ... TIME TO FLY THE PRESENT LEG
232 ASSUMING IT IS FLOWN AT AVEV //
233
234 ...
235 CAN NOW DETERMINE THE TYPE OF PROFILE TO BE FLOWN
236 FOR THIS LEG. IF T2 LEQ T1 THEN THE VELOCITY CHANGE
237 BETWEEN W(U-1) AND W(U) WILL BE AT A CONSTANT RATE
238 CLO MINRATE FOR A TIME T2. OTHERWISE THE LEG IS FLOWN
239 AT A CONSTANT VELOCITY FOR DISTANCE DP AND AT AN
240 ACCELERATION OF MINRATE FOR DISTANCE DPP AND TIME T1
241 IF T2 LEQ T1 //
242 THEN
243 FOR GREATER THAN OR EQUAL TO MINRATE
244 BEGIN
245 DLEI12 : ... TIME TO FLY THE LEG
246 DPP=DU : ... DPP IS THE LEG DISTANCE
247 END
248 ELSE
249 FOR LESS THAN MINRATE
250 BEGIN
251 DLEI11 : ... TIME TO FLY THE CHANGE IN VELOCITY //
252 DPP1=AVEV : ... DISTANCE TO DO THE SAME
253 END : ... END MINRATE BLOCK //
254
255 ...
256 DETERMINE IF W(U) IS THE TO-EVENT
257 IF NOT TO-EVENT //
258 THEN IF W(U) IS TO-EVENT
259 THEN
260 BEGIN TO-EVENT BLOCK
261 BEGIN
262 WCONT=IASVALU : ... VALIDATE COMMAND IAS VAL FLAG //
263 VTIMEFIX : ... IFIX IS SET VALID=INVALID BY PHMON.
264 IF THERE IS NO TIME FIX WE LEAVE
265 CALCULC BLOCK AFTER CALCULC THROGA //
266 WATRU=AIR : ... ALONG TRACK WIND COMPONENT TO-EVENT //
267 IF LOWIAS NEG VALID ... IF TRUE AIR SPEED IS LESS
268 THAN TASLIM (150 KTS) * HOLD
269 KALITO CONSANI
270 THEN KALITURKALT : ... OTHERWISE UPDATE KALITO //
271
272 ...
273 NOW DECIDE IF THERE WILL BE A VEL CHNG BETWEEN THE
274 FROM AND TO EVENTS
275 IF T2 LEQ T1 OR DVG LEQ DPP
276 THEN
277 ... DETERMINE DFLT FOR A VELOCITY RATE
278 ... GREATER THAN MINRATE
279 BEGIN
280 VDEIASPREV+KATK : ... W(U-1)*WIND(U) //
281 VDEIAS+KATK : ... W(U)*WIND(U) //
282 LIMIT DVG TO LEQ DPP
283 IF DVG GTI DPP
284 THEN RTGUPP=KATK*4
285 ELSE RTGUPP=DVG/DPP :
286 VDEI=RTGUPP*(V(U-1)+V(U)-V(U-1)*WIND(U)) :
287 VDEI=RTGUPP*(V(U-1)+V(U)-V(U-1)*WIND(U)) :

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285 IF UNTG GTI DPP
286 THEN DELT=T2*(OMTG-DPP)/AVGNOM
287 ELSE
288 DELT=OMTG/10.5*(VGNOM+VFT) ;
289 END
290
291 ELSE ... NO VEL CORR REQUIRED FOR FIRST PART
292 OF THIS LEG INTO TO-EVENT. DETERMINE
293 HOW MUCH OF LEG IS LEFT TO FLY AND
294 HOW LONG IT WILL TAKE //
295
296 BEGIN
297 VGNOM=IASPREV*WATK ;
298 UP=OMTG-DPP ; ... PORTION OF LEG REMAINING TO BE FLOWN
299 AT CONSTANT VELOCITY //
300 DELT=T1+UP/AVGNOM ; ... TIME TO FLY THIS PORTION //
301 END ;
302
303 NOW DETERMINE ITG TO TO-EVENT //
304 ITGOM=ITGOM+DELT ; //
305 END //
306
307 ELSE
308 BEGIN BEYOND TO-EVENT BLOCK
309 DETERMINE T1G UP TO THE TIME FIX. INCLUDED
310 ARE CORRECTIONS FOR LEG CAPTURE AT WIG-1)
311 AND AN ALLOCATION CALCULO COMPUTATIONS FOR
312 COCH GED 160 //
313
314 BEGIN
315 IF T2 GT T1
316 THEN
317 BEGIN
318 OPENJ-DPP ; ... SECTION OF LEG FLOWN AT CONSTANT
319 TASPRLV. //
320 DELT=T1+DP/(TASPREV+WATK) ; ... TOTAL TIME TO FLY LEG
321 //
322 END ;
323 ITGOM=ITGOM+DELT ; ... ADD THIS LEG TO THE TOTAL //
324 TIME TO GO TO T-FIX //
325
326 WILL NOW MAKE ADJUSTMENT FOR SLIGHTLY DIFFERENT
327 PATH FLOWN DUE TO TURN-ECI-NOT ALLOWING //
328 COURSE CHANGES GED 160 DEGREES //
329 IF ABS(COCHPREV) GED D160
330 THEN
331 INVALID COCH //
332 BEGIN
333 VGNOM=IVGNOM ; ... INVALIDATE CORRECTED IAS FOR //
334 COURSE CHANGE GED D160 //
335 GEDU LOGS1 ; //
336 END ;
337
338 VALID COCH //
339 ABS(COCH)=ABS(COCHPREV) ;
340 DELT = GEDU*ABS(COCH)/COS(10.5*ABS(COCH)) ;
341 DELT=IASPREV*DELT*PIGIAN25 ;

```



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342 DELT = DELT/10.5*ACOS(0.5*ABS(COCH)) :
343 ITGCOM=ITGCOM+DELT : ... AND TO TIGOM
344 END :
345 END RETURN TO EVENT BLOCK
346 COCHREV=COCHREV+(ITGCOM-ITGCOMPR) :
347 ... UPDATE COCHREV
348 PREVIAS=PREVIAS+(ITGCOM-ITGCOMPR) : ... UPDATE PREVIAS
349 END :
350 END LATERAL EVENT BLOCK
351 IS EVENT A VERTICAL EVENT ?
352 ...
353 BEGIN VERTICAL EVENT BLOCK
354 ...
355 THEN
356 BEGIN
357 IF NOT TOEVE(MAPT) ... TRUE IF W(J) IS TO-EVENT
358 THEN HZ=CALL ... ASSIGN AIRCRAFT ALT TO HZ
359 ELSE HZ=ALT(MAPT) :
360 ... ASSIGN ALTITUDE TO HZ
361 END :
362 END VERTICAL EVENT BLOCK
363 REV=REV+1 : ... INCREMENT EVENT NUMBER
364 END :
365 END CALCUL BLOCK
366 ...
367 IF (TIME=TIMEF .V. IFIX) THEN VALID ... SET TIME FLAG
368 THEN
369 BEGIN
370 K=SCALE : ... IF THERE IS NO TIME-FIX OR TIGOMF
371 ... THEN ITGCOM AND HZ=CALL ALSO K CAN NOT BE
372 DETERMINED SO LET K=SCALE
373 ... VALID NO WE CAN CALC VCOM1,VCOM2
374 K=SCALE :
375 END
376 ELSE
377 BEGIN
378 K=CON-OMIS : ... CONVERTS INTEGER TO REAL
379 ... BECAUSE GRK 323.0711
380 ITGCOM=ITGCOM/VCOM1 : ... CALC THE COMMANDED TIG FOR ARRIVAL
381 ... AT THE TIME FIX
382 K=SCALE :
383 ... INITIALLY SET K=VAL INVALID
384 IF THE PRODUCT OF TIGOM AND K=SCALE IS LESS
385 THAN THE ABS(ITGCOM) WE WILL HAVE A MEANTIMEFULL
386 CONSTANT K. GENERALLY THIS PROTECTS AGAINST THE CASE
387 WHERE TIGOM GOES TO ZERO
388 IF K=ITGCOM*SCALE LET ABS(ITGCOM)
389 THEN
390 BEGIN
391 K=ABS(ITGCOM) :
392 K=SCALE :
393 K=SCALE :
394 END :
395 END :
396 IF VCOM1EVAL IS VALID ... VCOM1EVAL WILL NOT BE VALID FOR
397 THE CASE WHERE THERE IS NO SPEED DEFINED
398 FOR THE TO-EVENT OTHERWISE ITS VALID//
399 THEN
400 BEGIN

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399      ...
400      IF KVAL EOL VALID
401      THEN
402      BEGIN
403      VCOMI=(KAVGADU)/KSCALE*WATO ; ... CALC COMMANDD TAS
404      VCOMI=(KAVGADU)/KSCALE*WATO ; ... CALC COMMANDD TAS
405      ... CONVERT VCOMI TO IAS
406      VCOMI = KMAXFIRMI*(VCOMI/COMIMAX) ; ... WESTWILL VCOMI
407      TO LIMITS IMPOSED BY THE IAS INSTRUMENT
408      END ;
409      IF TIMEH EOL VALID ... IF THERE IS A TIME-FIX OR COMMANDD
410      TIME THEN CAN CALC TIMEH
411      THEN
412      EARLY=(TIMEH-VCOMI/FACTAS*WATO)-TICCOM ;
413      ... CALC THE EXPECTED TIME ERROR FOR
414      ARRIVAL AT THE TIME FIX
415      TIMEH=ABS(EARLY) ; ... DO THIS TO MAKE CORRECTION FOR NEGATIVE
416      NUMBERS
417      END ;
418      EUSITS
419      TCOMF=INVALID ;
420      END ;
421      END FINI
422
SPRTS D.TCOMZFAI

```

APPENDIX D

Program Listing of the 2D Plus Time Control System  
Time Control Algorithm



42085HMFLL.TUCM7EAL

**D-2**



```

114 THEN IVALT
115 ELSE IF TCOMF EQL INVALID
116 THEN NODATA
117 ELSE IASVALID) EQL IASVALID //
118 ... VCOMI VALID BLOCK //
119
120 GET A SHAPSHOT OF SENSOR DATA USED FOR TIME CONTROLS
121 CAN CALCULATIONS. MUST YIELD CHANNEL TIME FIRST //
122
123 *CPTI) : ... YIELD CHANNEL TIME //
124 ACIAS = IAS(ACHO) : ... AIRCRAFT TRUE AIR SPEED //
125 ACALT = ALT(ACHO) : ... AIRCRAFT ALTITUDE //
126 ACIASERR = BLV(ACHO) : ... IAS INSTRUMENT ERROR //
127 ACALERR = KALD : ... NORTH COMPONENT OF WIND //
128 ACALERR = KALD : ... EAST COMPONENT OF WIND //
129 DESIRED.CRS = INSTRS(ACHO) : ... HSI COURSE INPUT //
130 DETERMINE VCOMIAX, THE UPPER LIMIT FOR VCOMI, AS REQUIRED //
131 BY THE AIRCRAFT IAS INSTRUMENT //
132
133 VCOMIAX = IF LUC C880 GRT 0 THEN VCOMIAX.C880
134 ELSE VCOMIAX.G1 :
135
136
137 FIND THE ALONG TRACK COMPONENT OF THE WIND FOR //
138 THE GIVEN DESIRED COURSE //
139
140 WATK = -(LUCWIND*DESIRED.CRS)*ACALERR*
141 *SIN(DESIRED.CRS)) :
142
143
144 CALCULATE KALT, THE ALTITUDE PROPORTIONALITY CONSTANT //
145
146 KALT = WATK/((ACIAS-VCOMI-ACIASERR)*KALISCALE,
147 ACALT*ACIAS*PIR) :
148 ... LIMIT FUNCTION AND KALISCALE ARE USED //
149 TO PROTECT AGAINST OVERFLOW //
150
151 KALT = KALT/((ACIAS*ACALT)) : ... CALC KALT //
152
153 LIMIT KALT TO THE INTERVAL (.1,.15) //
154
155 KALT = KMAXF(KALINTF(KALT,.15),.10) :
156
157 IF LUCIAS NEQ VALID
158 THEN KALTYC = KALT :
159
160 IF TRUE AIR SPEED IS LESS THAN IASLIN (150 KNOTS) •
161 HOLD KALTYC CONSTANT //
162
163 IF A COMMAND ARRIVAL TIME HAS BEEN ENTERED VIA //
164 THE CUI, THEN COMMAND IAS AND ARRIVAL TIME //
165 ERROR MAY BE CALCULATED. //
166
167 IF TCOMF EQL VALID ... ARRIVAL TIME ENTERED ? //
168 THEN BEGIN ... BEGIN TIME BLOCK //
169
170 ...
171
172 ...
173
174 ...
175
176 ...
177
178 ...
179
180 ...
181
182 ...
183
184 ...
185
186 ...
187
188 ...
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```

171 G*FI = ICOM - G*IS :
172 ... INTER ARITHMETIC MEQUIMLD
173 TIGCOM = G*FI/G*ICOM :
174 ... CONVERT TO NAV TIME UNITS
175 ...
176 CALCULATE VALUES FOR COMMANDS TAS
177 AND COMMANDS IAS.
178
179
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    VCOMI = HMTF(IOMIG,ITIGCOM,MINI/ITIGCOM - MAXI :
    ... CALC COMMANDS IAS
    ...
    VCOMI = (MAXI-(MAXI-MINI)/CALISCALE)*VCOMI :
    ... CONVERT IAS TO IAS
    RESINCI VCOMI TO LIMITS IMPOSED BY THE
    IAS INSTRUMENT
    VCOMI = MAXI*(RESINCI(VCOMI,VCOMIMAX),.0) :
    ...
    DETERMINE EARLY/LATE AND TIMEERR
    ...
    EARLY = IIG - ITIGCOM :
    ... THE SIGN OF EARLY PROVIDES EARLY OR
    LATE INDICATION FOR CDD DISPLAY
    TIMEERR = ABS(EARLY) :
    ... MAGNITUDE OF ARRIVAL TIME ERROR
    FOR CDD DISPLAY
    TIMEERR = VALID : ... INDICATE VALID ARRIVAL
    ... END TIMEERR BLOCK
    ... VCOMI VALID BLOCK
    ... ACKNOWLEDGE DIVISION TO
    THE FLY PLAN
    ... END MAIN BLOCK
    ... END PROCEDURE TIMEERR
    END :
    END FINT
  
```

APPENDIX E

Program Listing of ILS  
Executive Routines

```

10 WORKFI, E, ILSBMDA1
1 BEGIN
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...
.INSERT LCGSDJ1 $.
.INSERT MATHPACK $.
...
.INSERT NTARM611 $.
.INSERT AEDLIB $.
...
DEFINE PROCEDURE MAINLCGS TOBL
...
PROCEDURE GSCMP $.
PROCEDURE LOCCMP $.
...
COMMENT INTERNAL DECLARATIONS $.
BOOLEAN LOCARM, LOCAP, GSCAP, GSCAM, GSCAP, RESETL, RESFTG,
LOCTRY $.
REAL LATUIS, LNCEDIS $.
INTEGER AC, POE $.
COMMENT SET ILS VARIABLES TO ANAV VARIABLES $.
...
SYNONYMS
BEGIN
HUTZ = ALTRTE
H4HZ = ALT
GNDV = GNDSPD
CT = GAMMA
LAMP = LATAP
PHIP = LONGAP
DTOTD = MAGTD
RJMD = RLGMOD
AENG = APENG
END - SYNONYMS
...
COMMENT ***** DATA DECLARATIONS FOR LOGIC USED TO DRIVE
THE MSI TO/FROM FLAG *****
REAL TOCRSDEV I
... TAE RELATIVE TO TOUCHDOWN AND
RAYHUG
... 90 DEGREES
... COORDINATES OF TOUCHDOWN USED FOR
REAL REG90 I
REAL ARRAY TOP0C(11) I

```

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CALL TO LTRD. ARRAY IS NEEDED TO  
ENSURE CONSECUTIVE CORE LOCATIONS  
FOR TOUCHDOWN COORDINATES. //  
USED TO RECORD LTRD BEARING AND  
DISTANCE COMPUTATIONS BETWEEN THE  
AIRCRAFT AND TOUCHDOWN. //  
ACTOTD ELEMENT USED TO RECORD BEARING  
FROM AIRCRAFT TO TOUCHDOWN  
ACTOTD ELEMENT USED TO RECORD BEARING  
FROM TOUCHDOWN TO AIRCRAFT  
ACTOTD ELEMENT USED TO RECORD  
DISTANCE BETWEEN AIRCRAFT AND  
TOUCHDOWN. //

REAL ARRAY ACTOTD(1) //  
SYNONYMS 0 = BRG.ACTOTD //  
SYNONYMS 1 = BRG.TOTD //  
SYNONYMS 2 = DIST.ACTOTD //

PRESET

BEGIN  
TDCSDV = .0  
DEG90 = .5  
TPOS = .0  
ACTOTD = .0  
END

LOCDEV = LOC(ADHD) \$  
GSDV = GSI(ADHD) \$  
AIRSPD = TAS(ADHD) \$  
ACHOG = PSIM(ADHD) \$

SELVAL = IF LOC(ADHD) EOL 0 THEN TRUE ELSE FALSE \$  
COMVAL = IF IBYTEO (LOC HEAD) EOL 0 THEN TRUE ELSE FALSE \$  
SPGVAL = IF GSI(ADHD) EOL 0 THEN TRUE ELSE FALSE \$  
ALTVAL = IF IBYTEO(LUC HZHF) EOL 0 THEN TRUE ELSE FALSE \$

E-3

COMMENT SET ANNUNCIATORS FALSE \$  
PRESET

BEGIN  
LUCARM = FALSE \$  
LUCCAP = FALSE \$  
GSAHM = FALSE \$  
GSCAP = FALSE \$  
END  
... PRESET ANNUNCIATORS FALSE \$

COMMENT SET ACTIVE MODE TO RNAV \*\* RNAV IS ONE \*\* LOC IS TWO \*\*  
APPR AUTO IS THREE \$  
PRESET

BEGIN  
ACTHUE = 1 \$  
END  
... PRESET ACTIVE MODE \$

COMMENT SET LOC TRK FALSE \$  
PRESET

BEGIN  
LOC TRK = FALSE \$  
END  
... SETTING LOC TRK \$

COMMENT INITIATE RESETS \$  
PRESET

BEGIN

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```

114 R-SETL = TRUE $;
115 RESETG = TRUE $;
116 END
117 ... PRESLT RESPTS $;
118 ... END INITIATE BLOCK $;
119
120 COMMENT DISTANCE CALCULATIONS FOR DISTANCE TO TOUCHDOWN AND
121 DISTANCE TO LOC ANTENNA $;
122 BEGIN
123 REAL LATFIX,DLAT,ULONG,IRES,PI $;
124 IRES = 0.02907817 $;
125 PI = 0.31030989 $;
126
127 ...
128
129 LATFIX = NCOS(LATD) $;
130
131 ...
132
133 DLAT = LATD-LATAP $;
134 IF LONGAP LES 0.0
135 THEN IF (1.999999 + LONGAP) LES LONGTD
136 THEN ULONG = -(1.999999 - LONGTD) +
137 (1.999999 + LONGAP)
138 ELSE ULONG = LONGTD - LONGAP
139 ELSE IF (1.999999 - LONGAP) LES -LONGTD
140 THEN ULONG = (1.999999 + LONGTD) +
141 (1.999999 - LONGAP)
142 ELSE DLONG = LONGTD - LONGAP $;
143 LONGDIS = DLONG*LATFIX/(IRES*PI) $;
144 LATDIS = ULAT/(IRES*PI) $;
145
146 ...
147
148 RNGTD = ROOT2((LNGDIS*LNGDIS)+(LATDIS*LATDIS)) $;
149
150 ...
151
152 ... DISTANCE CALCULATIONS $;
153 END
154
155 COMMENT CHECK MODE VALIDITIES $;
156 IF COMVAL AND SELVAL AND LCFVAL
157 THEN LOVAL = TRUE
158 ELSE LOVAL = FALSE $;
159 IF COMVAL AND SELVAL AND LCFVAL AND SFGVAL AND
160 ALVAL
161 THEN AVAL = TRUE
162 ELSE AVAL = FALSE $;
163 IF APENG AND LOCCAP OR LOCTRK
164 THEN RVAL = FALSE
165 ELSE RVAL = TRUE $;
166 ... END CHECK MODE VALIDITIES
167 $;
168
169 COMMENT BEGIN DETERMINING IF REQUESTED MODE IS VALID AND SETTING
170 ACTIVE MODE EQUAL TO REQUESTED MODE $;
171 IF ACTMDE NEO REQMOD
172 THEN BEGIN

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171 IF (IREQMOD EOL 1) AND RHAVAL)
172 THEN BEGIN
173   LOCARM = FALSE $;
174   NAVCAP = FALSE $;
175   LOCCAP = FALSE $;
176   GSARM = FALSE $;
177   GSCAP = FALSE $;
178   END
179   ** RESET ANNUNCIATORS FALSE $;
180   IF (IREQMOD EOL 1) AND RHAVAL) OR (IREQMOD
181     EOL 2) AND LOCVAL) OR (IREQMOD EOL 3) AND
182     AVAL)
183   THEN ACTMDE = REQMOD $;
184   ... END CHECKING REQUESTED
185     MORE VALIDITIES $;
186
187   END $;
188
189   COMMENT SERVICE COMPUTATIONS , SET FLAGS $;
190   IF ACTMDE NEO 1
191   THEN BEGIN
192     IF ((ACTMDE EOL 2) AND LOCVAL) OR ((ACTMDE
193       EOL 3) AND AVAL)
194     THEN CUPFLG = TRUE
195     ELSE CUPFLG = FALSE $;
196
197     ...
198     LOCCHP(RESETL,LOCDFV,BANK,LANGUIC,LATDIS,LOCARM,LOCCAP,
199       LOCCHK,BKCMOA,BKCMDF)
200       $;
201     ...
202     //
203
204     RESETL = FALSE $;
205     IF NOT LOCARM
206     THEN BEGIN
207       PHICA = BKCMOA $;
208       PHICF = BKCMOF $;
209       END ... OUT LATERAL BANK CMOS $;
210     IF ACTMDE NEQ 2
211     THEN BEGIN
212       PTCMDA = VSAC $;
213       PTCMOF = VSAC $;
214
215       ...
216       GSCMP,GSDEV,RNGTO,VALTTE,TIMD,RESETG,GSARM,USCAP,LOCARM,PTCMDA) $;
217       //
218       ...
219       //
220       WESETG = FALSE $;
221       IF NOT GSARM
222       THEN BEGIN
223         VSCCA = PTCMDA $;
224         VSCLF = PTCMOF $;
225
226
227

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```

228 END ... OUT PITCH_CMOS S.
229 END S.
230 END ... END OF PROCESSING STEERING
231 COMPUTATIONS //
232 ELSE BEGIN
233 RESETL = TRUE S.
234 RESETG = TRUE S.
235
236 END S.
237
238
239
240
241 LOCAA = LOCCAP S.
242 LOCCA = LOCCAP S.
243 GSA = GSARM S.
244 GSCA = GSCAP S.
245 STATHN = "CINCE" S.
246
247
248
249
250 COMMENT ***** CONTROL THE HSI TO/FROM FLAG BY ASSIGNING ONE OF THE
251 FOLLOWING VALUES TO THE RNAV FLAG CALLED TOWARD
252
253 TOWARD = 1 IF AIRCRAFT HAS NOT PASSED THE PERPENDICULAR
254 TO RWAYDS AS CONSTRUCTED AT TOUCHDOWN.
255 = 0 OTHERWISE . ***** S.
256
257 IF LOCCAP OR LOFCAP
258 THEN BEGIN
259 TOPOS(0) = LATDUI
260 TOPOS(1) = LONGTD I
261 ILTBD(LOC LATAP, LOC TOPUS, LOC ACTO'D) I
262 TOCKSDEV = RWAYDS - ACTO'D(BRG.TUTOAC) I
263 TOWARD = IF ANS(TOCSDEV) GRT DEG90
264 THEN 1
265 ELSE 0 I
266
267 END I
268
269 ... END OF LOGIC THAT CONTROLS THE
270 HSI TO/FROM FLAG //
271 ... END OF SERVICING COMPUTATIONS, SETTING FLAGS S.
272
273 END S.
274
275 END FINE

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AFIN

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APPENDIX F

Program Listing Of  
Localizer Routine

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```

57 BEGIN
58
59 COMMENT ***** DESCRIPTION OF PROGRAM VARIABLES *****
60
61 *** // *** NAV CAPTURE VARIABLES ***
62
63 *** NAV CAPTURE LOGIC FLAG :
64 *** NAV CAPTURE BANK BEING DOWN COMMAND
65
66 LOGIC FLAG :
67
68 RANGE PARAMETER USED IN LOGIC
69 GENERATOR FOR NAVCAP (FT) :
70
71 ABSOLUTE VALUE OF BEAMS (MAXIMUM) :
72
73 VARIABLE USED IN BEAM LOGIC
74 COMPUTATION :
75
76 TRACK ANGLE ERROR AL BEAM EDGE
77 (DEGREES) :
78
79 DATA CMD - NAV CAP (LOG) :
80
81 DATA OR NAV CAP BANK CDS BEING DOWN :
82
83 ENLIGHTENMENT ARGUMENT OF ARGENT :
84
85 FUNCTIONAL ADDITION ON VALUE IN
86 POLYNOM COMPUTATION : *** //
87
88 *** // *** ILS CAPTURE VARIABLES ***
89
90 TRUE UNTIL ABS(LOPUL) IS LESS THAN
91 240. :
92
93 ILS CAPTURE LOGIC FLAG :
94
95 BANK CMD - BEAM CAPTURE (ILS CAP)
96 (DEG) :
97
98 CROSS TRACK RATE - BEAM CAPTURE - NAV
99 DATA (FT / SEC) :
100
101 CROSS TRACK RATE : BEAM CAPTURE - ILS
102 DATA (FT / SEC) :
103
104 CROSS TRACK RATE - BEAM CAPTURE (FT /
105 SEC) :
106
107 CROSS TRACK DISTANCE UNFILTERED -
108 BEAM CAPTURE (FT) :
109
110 CROSS TRACK DISTANCE - BEAM CAPTURE
111 (FT) :
112
113 GAIN ON PAPER IN BEAM CAPTURE :
114
115 TIME CONSTANT OF PAPER IN BEAM
116 CAPTURE (SEC) :
117
118 GAIN FOR ALLDING Y DOT FROM NAV DATA
119 TO BEAM DATA :
120
121 OUTPUT OF BEAM CAPTURE FAULT (DEG) :
122
123 *** // *** COMMON CAPTURE VARIABLES ***
124
125 TRUE WHEN BEAM ANGLE IS LESS THAN 7
126 DEGREES :
127
128 CAPTURE PARAMETER COMPUTED FROM NAV
129 DATA (FT) :
130
131 CAPTURE PARAMETER COMPUTED FROM ILS
132 DATA (FT) :
133
134 LOCALIZER CAPTURE TRIP POINT (FT) :
135
136 THEORETICAL BANK USED IN CAPTURE
137 (DEG) :

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114 REAL CDBANK *** MAX VALUE OF BANK (RADIANS) :
115 REAL REFROT *** REFERENCE FRAME ROTATION ANGLE
116 (RADIANS) :
117 REAL CTO *** CROSS TRACK DISTANCE FROM NAV DATA
118 (IN) :
119 REAL CTDNAV *** CROSS TRACK DISTANCE FROM NAV DATA
120 (FT) :
121 REAL TAL *** TRACK ANGLE ERROR (RADIANS) :
122 REAL V6 *** GROUND SPEED (FT / SEC) :
123 *** //
124 *** //
125 *** //
126 REAL TRNTP *** LOCALIZER TRACK TRIP POINT
127 (MICROSECS) :
128 REAL ANSDC *** ABSOLUTE VALUE OF DC-BIAS (RADIANS) :
129 REAL TACMP *** VARIABLE USED IN COMPUTATION OF
130 TACTRK :
131 REAL TACTRK *** THEORETICAL TRACK ANGLE ERROR (AT
132 TRACK (RADIANS) :
133 REAL MCOTK *** BANK CRO - TRACK (DEG) :
134 REAL COTRK *** CROSS TRACK RATE - TRACK (FT / SEC) :
135 REAL COTRK *** CROSS TRACK DISTANCE - TRACK (FT) :
136 REAL MCOTK *** GAIN ON CROSS TRACK DISTANCE - TRACK
137 (DEG / FT) :
138 REAL FCOTK *** PRACTICAL MULTIPLIER IN GAIN ON
139 CROSS-TRACK DISTANCE :
140 REAL MCOTK *** GAIN ON CROSS TRACK RATE - TRACK (DEG
141 / FT / SEC) :
142 REAL FCOTK *** PRACTICAL MULTIPLIER IN GAIN ON
143 CROSS-TRACK RATE - TRACK :
144 REAL MAXNG *** MAXIMUM RANGE TO LINEARIZE TRACK LAWS
145 (FT) :
146 REAL RUGROM *** GAIN ON OUTPUT OF RUGROM FOR TRACK :
147 REAL FCOTK *** GAIN ON FASTER IN TRACK :
148 REAL TFOTK *** TIME CONSTANT OF FASTER IN TRACK (SEC)
149 :
150 REAL DELTRK *** OUTPUT OF TRACK FASTER (DEG) :
151 REAL FASTER *** BANK WASHOUT TIME CONSTANT (SEC) :
152 REAL BAKSLP *** BANK WASHOUT LIFT (DEG) :
153 REAL BAKSLP *** LO-PASSED BANK (DEG) :
154 REAL KWIN *** ELAPSED TIME AFTER LOCKIN THAT BANK
155 WASHOUT IS INITIATED (SEC) :
156 REAL TPASTR *** ELAPSED TIME AFTER LOCKIN (SEC) :
157 REAL FILPAD *** GAIN ON FASTER OF FILC :
158 REAL TRNTP *** COUNTER USED TO DETERMINE WHEN TO
159 TRIP IN INCREASED BANDWIDTH IN FILTER
160 C (SEC) :
161 REAL FILTRP *** NUMBER OF SECONDS AFTER TRACK WHEN
162 INCREASED BANDWIDTH IS THIPPED INTO
163 FILTER C (SEC) :
164 REAL VKEILC *** VARYING BANDWIDTH PARAMETER OF FILTER
165 C :
166 REAL DIFILC *** VARYING PARAMETER USED IN COMPUTING
167 VKEILC :
168 REAL FIMELC *** FASTER BANDWIDTH PARAMETER USED IN
169 FILTER C :
170 REAL FASTER *** TIME CONSTANT OF THE INCREASED

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171 BANDWIDTH PAPER WAVE IN FILTER C  
172 (SEC) : ... //

173 ... //

174 ... // \* COMMON I/O VARIABLES \* //

175 ... //

176 ... // RANGE TO LOCALIZER (FT) : ... //

177 ... //

178 ... // \* COMMON VARIABLES \* //

179 ... //

180 ... // LOCALIZER DEVIATION THROUGH RATE  
181 LIMITER (MICROAMPS) :

182 ... // LOCALIZER (MICROAMPS) :

183 ... // MAX LOCALIZER DEVIATION DIFFERENCE  
184 BETWEEN LOCALIZER (MICROAMPS) :

185 ... // COMPUTATIONAL TIME INCH/SEC (SEC) :

186 ... // ACCELERATION FEED INTO FILTER C (FT /  
187 SEC) :

188 ... // POLI - ZERO PARAMETER OF FILTER C :

189 ... // INITIAL BANDWIDTH PARAMETER OF FILTER  
190 C :

191 ... // TRUE UNTIL FIRST GENERATION OF DRCDA  
192 :

193 ... // RATE LIMIT ON BANK CMD (SEC / SEC) :

194 ... // AMPLITUDE LIMIT ON BANK CMD (DB) :

195 ... // MAXIMUM ALLOWABLE CHANGE OF DRCDA  
196 (DB) :

197 ... // LAST VALUE OF DRCDA - SAVED BEFORE  
198 LEAD-LAG (DB) :

199 ... // LAST VALUE OF DRCDA OUTPUT BY LOPASS  
200 OF LEAD-LAG (DB) :

201 ... // DIFFERENCE BETWEEN PRESENT BANK  
202 COMMAND AND LAST (DB) :

203 ... // TIME CONSTANT FOR THE LEAD-ON-BANK  
204 CMD (SEC) :

205 ... // TIME CONSTANT FOR THE LAG ON BANK CMD  
206 (SEC) : ... //

207 ... //

208 REAL SCAL1, SCAL2, SCAL3, SCAL4, SCAL5, SCAL6, SCAL7, SCAL8, SCAL9, SCAL10,  
209 SCAL11, SCAL12, SCAL13, SCAL14, SCAL15, SCAL16, SCAL17, SCAL18, SCAL19,  
210 COMP1, COMP2, COMP3, COMP4, COMP5, COMP6 :

211 REAL PROCEDURE LIMIT, LOPASS, REAP :

212 PROCEDURE PROCE : ... //

213 ... //

214 PRESET

215 BEGIN

216 TIMESTEP = .2 :

217 KVALDC = .016731 ... EXP(-(TIMESTEP / 1.)) :

218 KVALTK = .003709 ... EXP(-(TIMESTEP / 5.)) :

219 F1FAC = .923356 ... EXP(-(TIMESTEP / 30.)) :

220 KVALTK = .023375 ... 1. / ( 1.0 \* (1.4 \* 100. ) / (70. /  
221 125.)) :

222 KVALTK = .350 ... 1. / (135. \* 100. ) / (70. / 125.)) :

223 ...

224 ...

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[illegible]

COMMENT THE FOLLOWING CARDS MUST BE REMOVED BEFORE CROSS-COMPILING :

```
205 CURRENT .....  
206 REAL PROCEDURE LGIN=NCOSIN(TAN) ;  
207 LOCDEV = LOCDEV/300. ;  
208 IF LOCDEV = 1. ;  
209 THEN LOCDEV = .9999 ;  
210 IF LOCDEV = 1. ;  
211 THEN LOCDEV = .9999 ;  
212 IF RESETL  
213 THEN LOCDEV = LOCDEV ;  
214 DATA = LGIN/3.1415927 ;  
215 MARGIN = MARGIN/3.1415927 ;  
216 ACROSS = ACROSS/3.1415927 ;  
217 AIRSPD = AIRSPD/100. ;  
218 GRESPO = GRESPO/100. ;  
219 RAYING = RAYING/3.1415927 ;  
220 GAMMA = GAMMA/3.1415927 ;  
221 REGIO = REGIO/100. ;  
222 LOGSIS = LOGSIS/100. ;  
223 PLYTH = PLYTH/10. ;  
224 LATDIS = LATDIS/100. ;  
225 SCAL11 = 1. ;  
226 SCAL12 = 1. ;  
227 SCAL13 = .01 ;
```

COMMENT .....  
COMMENT THE ABOVE CARDS MUST BE REMOVED BEFORE CROSS-COMPILING ;  
CONVERT .....  
COMMENT ..... DATA PROCESSING MODULE .....  
COMMENT ..... RANGE TO LOCALIZER COMPUTATION .....  
RANGLOC = (PI\*GIL\*PLYTH\*.1) / .0076 ;  
COMMENT ..... TRACK AND CLUTCH COMPUTATIONS .....  
TAE = (MARG-MARGIN)/MARG ;  
COMMENT ..... CHANGE GROUND SPEED FROM KNOTS TO FT / SEC .....  
VS = GRESPO/SCAL1 ;  
COMMENT ..... RATE LIMIT ON LOCDEV .....  
XLOCV = ((MARGIT-PI\*VS\*GINSIN(TAN)/SCAL2)\*.001)/MARGLOC/SCAL17 ;  
IF XLOCV = SCAL16 ;  
THEN XLOCV = SCAL16 ;  
LOCV = LOCDEV-LOCDEV ;  
LOCCL = LOCCL-LIMIT(LOCV,XLOCV) ; ... //  
... //  
IF NOT LOCCLR  
THEN BEGIN  
... //  
... //  
XLOCOT = .005\*.015\*(MARGLOC\*.00076) ;  
IF XLOCOT > SCAL19  
THEN TRAMP = .1\*SCAL19/MARGLOC  
ELSE TRAMP = 1. ;

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```

352 COMMENT ***** NAV CROSS TRACK DISTANCE COMPUTATIONS *****
353 REFPOI = RAYTHOS*5
354 CTD = LATDIS*NCOS(REFPOI)*LNGDIS*NSIN(REFPOI)
355 CTUNAV = (CTD*.6076)/.1
356 END
357 ... //
358 ... //
359 ELSE BEGIN
360
361 COMMENT ***** BANK WASHOUT *****
362 IF TRIMT GEO WGIN
363 THEN BEGIN
364   BANKWP = LOGN(SIBANK*BANKLP*LN(401*SPALN))
365   BANKWP = LIMIT(BANKWP,BANKOL)
366   BANK = BANK*LNKWP
367 END
368 ELSE TRIMT = TRIMT*TIMSP*.01
369 END
370
371 COMMENT ***** LOCALIZER DATA FILTERING *****
372 IF ((ABS(LOCN1) LEQ SCAL2) OR (NOT FSTCAL)) AND DEVEL
373 THEN BEGIN
374   CTUNCV = -VG*NSIN(TAE)
375   CTUNCV = NGLOC*LOCORL*(SCAL3/.1)
376   IF LOCFA
377   THEN BEGIN
378     IF TRIMT GEO FILTP
379     THEN BEGIN
380       DIFILC = DIFILC*FILEAD
381       VFILC = FVALC-DIFILC
382     END
383     ELSE TRIMT = TRIMT*TIMSP*.01
384     END
385   ACCEL = ((NSIN(BANK)/NCOS(BANK))*NCOS(TAE))*(.01/SCAL4)
386   IF FSTCAL
387   THEN BEGIN
388     CTUNCV = CTUNCV
389     CTUNCI = CTUNCI
390   END
391   ELSE BANKF(CIBCU,VFILC,VFILC,TIMSP,CTDEC,CTREC,ACCEL)
392   KYMIL = NCOS(TAE)
393   CTREC = CTREC*(.9999-KYMLN)*CTREC*KYMLN
394   FSTCAL = FALSE
395 END
396 ELSE BEGIN
397   CTUNCV = CTUNAV
398   CTREC = -VG*NSIN(TAC)
399   CTUNCI = CTUNCI
400 END
401
402 COMMENT ***** CAPTURE TRIP POINT COMPUTATION *****
403 IF LOCFA
404 THEN BEGIN
405   CTUNCV = SCAL2*TRIMLOC/SCAL3
406   IF CTUNCV GT SCAL
407   THEN CTUNCV = SCAL
408

```

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```

CAPBOM = (CPBOMX/5)*TAE I
IF AUS(CAPBOM) LES SCALB
THEN CAPBOM = (SCALB-TAE)/AUS(TAE) I
CAPBOM = ((VGO*2)/(1.9999-NCOS(TAE))*SCA/4)/(HCSIN(CAPBOM)/
ACOS(CAPBOM))//1 I
CAPBOM = ((COS(CI*2/3))*SCAL4+NCOS(CAPBOM))/(HCSIN(CAPBOM)*
.9999-NCOS(CAPBOM)/NCOS(TAE)) I
IF (HCSIN(CAPBOM) LES SCAL9
THEN CAPBOM = CAPBOM I
ELSE CAPBOM = CAPBOM I
CAPBOM = CAPBOM*(CAPBOM*VG+.01)/(KATLIN/TIMSP) I
END I ... //

```

CURRENT \*\*\*\*\* VOLUME GENERATOR \*\*\*\*\* : ... //

```

IF NOT LOGTR
THEN BEGIN
IF (TRANSICIDRAW**1)/HMLLOC**31001.LED.SCAL15).OR.UEVFLG
THEN DEVELG = TRUE I
IF LOGCAP
THEN BEGIN
IF (HCSIN(CAPBOM) LES SCAL9) AND DEVELG
THEN BEGIN
IF AUS(CIDOC) LES AUS(CAPBOM) ... TEST FOR ILS
CAPTURE //

```

```

THEN BEGIN
LOGCAP = FALSE I
LOGCAP = TRUE I
NAVCAP = FALSE I
END

```

```

END BEGIN ... TEST FOR NAV CAPTURE //
IF (AUS(TAE) LES SCAL7
THEN ILSON = (AUS(TAE)*(VG-.125))/(.83019)*.02127
ELSE ILSOK = (VGO*(AUS(TAE)-.02233))/(.53722 I
IF (TRANSICIDRAW) LES AUS(CAPBOM) AND (HCSIN(CAPBOM) LES
ILSON)
THEN BEGIN
LOGCAP = FALSE I
NAVCAP = TRUE ... SET NAVCAP I
END I

```

```

END I
IF NAVCAP
THEN BEGIN
IF (AUS(TAE) LES .95*TAE) ... TEST FOR BLKDN //
THEN BLKDN = TRUE I
IF (HCSIN(CAPBOM) LES SCAL9) AND DEVELG ... TEST FOR ILS
CAPTURE //
THEN BEGIN
LOGCAP = TRUE I
NAVCAP = FALSE I
END I

```

```

END I
IF LOGCAP OR ILSCAP
THEN BEGIN
IF (HCSIN(CAPBOM) LES .95*TAE) OR (AUS(TAE) LES .95*TAE)

```

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```

456 ... TEST FOR TRACK //
457 THEN BEGIN
458   ILSCAP = FALSE;
459   LUTRK = TRUE;
460   LCCAP = FALSE;
461   LCCAP = TRUE;
462   END;
463
464 END;
465 LCCAP = ILSCAP OR NAVCAP OR LCCAP;
466 END;
467
468 COMMENT ***** CONTROL COMPUTATIONS ***** //
469
470 IF NOT LOGCAP
471 THEN BEGIN
472
473   CURRENT INTERMEDIATE TRACK COMPUTATIONS;
474   IF BNCLOC LES NAMING
475   THEN BEGIN
476     ELSE BNCLOC = NAMING/BNCLOC;
477     CTDRK = BNCLOC/CTDRK;
478     CTDRK = BNCLOC/CTDRK;
479     BNCLOC = CTDRK/CTDRK;
480   IF NOT LOGTRK
481   THEN BEGIN
482     COMPS = ((CTDRK**2)/.1)*SCAL4;
483     COMPS = CTDRK*.99999-CTDRK*BNCLOC;
484     IF CTDRK LES .0
485     THEN BEGIN
486       COMPS = -COMPS;
487       COMPS = -COMPS;
488     END;
489     BNCLOC = -BNCLOC;
490     IF NOT ILSCAP
491     THEN BEGIN
492       BNCLOC = -BNCLOC;
493       BNCLOC = BNCLOC/COMPS;
494       TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
495       TACDRK = TACDRK/((BNCLOC**2));
496       COMPS = BNCLOC-TACDRK**2;
497       TACDRK = .5*BNCLOC/COMPS;
498       TACDRK = TACDRK/COMPS;
499       IF TACDRK LES SCAL19
500       THEN TACDRK = SCAL19;
501     END;
502
503   COMMENT NAV CAP COMPUTATIONS;
504   IF NAVCAP
505   THEN BEGIN
506     IF NOT BNCLOC
507     THEN BEGIN
508       COMPS = ((BNCLOC**2)/.1)*SCAL4;
509       IF CTDRK LES .0
510       THEN BEGIN
511         COMPS = -COMPS;
512         COMPS = -COMPS;
513       END;
514       BNCLOC = -BNCLOC;
515       IF NOT ILSCAP
516       THEN BEGIN
517         BNCLOC = -BNCLOC;
518         BNCLOC = BNCLOC/COMPS;
519         TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
520         TACDRK = TACDRK/((BNCLOC**2));
521         COMPS = BNCLOC-TACDRK**2;
522         TACDRK = .5*BNCLOC/COMPS;
523         TACDRK = TACDRK/COMPS;
524         IF TACDRK LES SCAL19
525         THEN TACDRK = SCAL19;
526       END;
527
528     COMMENT NAV CAP COMPUTATIONS;
529     IF NAVCAP
530     THEN BEGIN
531       IF NOT BNCLOC
532       THEN BEGIN
533         COMPS = ((BNCLOC**2)/.1)*SCAL4;
534         IF CTDRK LES .0
535         THEN BEGIN
536           COMPS = -COMPS;
537           COMPS = -COMPS;
538         END;
539         BNCLOC = -BNCLOC;
540         IF NOT ILSCAP
541         THEN BEGIN
542           BNCLOC = -BNCLOC;
543           BNCLOC = BNCLOC/COMPS;
544           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
545           TACDRK = TACDRK/((BNCLOC**2));
546           COMPS = BNCLOC-TACDRK**2;
547           TACDRK = .5*BNCLOC/COMPS;
548           TACDRK = TACDRK/COMPS;
549           IF TACDRK LES SCAL19
550           THEN TACDRK = SCAL19;
551         END;
552
553     COMMENT NAV CAP COMPUTATIONS;
554     IF NAVCAP
555     THEN BEGIN
556       IF NOT BNCLOC
557       THEN BEGIN
558         COMPS = ((BNCLOC**2)/.1)*SCAL4;
559         IF CTDRK LES .0
560         THEN BEGIN
561           COMPS = -COMPS;
562           COMPS = -COMPS;
563         END;
564         BNCLOC = -BNCLOC;
565         IF NOT ILSCAP
566         THEN BEGIN
567           BNCLOC = -BNCLOC;
568           BNCLOC = BNCLOC/COMPS;
569           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
570           TACDRK = TACDRK/((BNCLOC**2));
571           COMPS = BNCLOC-TACDRK**2;
572           TACDRK = .5*BNCLOC/COMPS;
573           TACDRK = TACDRK/COMPS;
574           IF TACDRK LES SCAL19
575           THEN TACDRK = SCAL19;
576         END;
577
578     COMMENT NAV CAP COMPUTATIONS;
579     IF NAVCAP
580     THEN BEGIN
581       IF NOT BNCLOC
582       THEN BEGIN
583         COMPS = ((BNCLOC**2)/.1)*SCAL4;
584         IF CTDRK LES .0
585         THEN BEGIN
586           COMPS = -COMPS;
587           COMPS = -COMPS;
588         END;
589         BNCLOC = -BNCLOC;
590         IF NOT ILSCAP
591         THEN BEGIN
592           BNCLOC = -BNCLOC;
593           BNCLOC = BNCLOC/COMPS;
594           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
595           TACDRK = TACDRK/((BNCLOC**2));
596           COMPS = BNCLOC-TACDRK**2;
597           TACDRK = .5*BNCLOC/COMPS;
598           TACDRK = TACDRK/COMPS;
599           IF TACDRK LES SCAL19
600           THEN TACDRK = SCAL19;
601         END;
602
603     COMMENT NAV CAP COMPUTATIONS;
604     IF NAVCAP
605     THEN BEGIN
606       IF NOT BNCLOC
607       THEN BEGIN
608         COMPS = ((BNCLOC**2)/.1)*SCAL4;
609         IF CTDRK LES .0
610         THEN BEGIN
611           COMPS = -COMPS;
612           COMPS = -COMPS;
613         END;
614         BNCLOC = -BNCLOC;
615         IF NOT ILSCAP
616         THEN BEGIN
617           BNCLOC = -BNCLOC;
618           BNCLOC = BNCLOC/COMPS;
619           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
620           TACDRK = TACDRK/((BNCLOC**2));
621           COMPS = BNCLOC-TACDRK**2;
622           TACDRK = .5*BNCLOC/COMPS;
623           TACDRK = TACDRK/COMPS;
624           IF TACDRK LES SCAL19
625           THEN TACDRK = SCAL19;
626         END;
627
628     COMMENT NAV CAP COMPUTATIONS;
629     IF NAVCAP
630     THEN BEGIN
631       IF NOT BNCLOC
632       THEN BEGIN
633         COMPS = ((BNCLOC**2)/.1)*SCAL4;
634         IF CTDRK LES .0
635         THEN BEGIN
636           COMPS = -COMPS;
637           COMPS = -COMPS;
638         END;
639         BNCLOC = -BNCLOC;
640         IF NOT ILSCAP
641         THEN BEGIN
642           BNCLOC = -BNCLOC;
643           BNCLOC = BNCLOC/COMPS;
644           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
645           TACDRK = TACDRK/((BNCLOC**2));
646           COMPS = BNCLOC-TACDRK**2;
647           TACDRK = .5*BNCLOC/COMPS;
648           TACDRK = TACDRK/COMPS;
649           IF TACDRK LES SCAL19
650           THEN TACDRK = SCAL19;
651         END;
652
653     COMMENT NAV CAP COMPUTATIONS;
654     IF NAVCAP
655     THEN BEGIN
656       IF NOT BNCLOC
657       THEN BEGIN
658         COMPS = ((BNCLOC**2)/.1)*SCAL4;
659         IF CTDRK LES .0
660         THEN BEGIN
661           COMPS = -COMPS;
662           COMPS = -COMPS;
663         END;
664         BNCLOC = -BNCLOC;
665         IF NOT ILSCAP
666         THEN BEGIN
667           BNCLOC = -BNCLOC;
668           BNCLOC = BNCLOC/COMPS;
669           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
670           TACDRK = TACDRK/((BNCLOC**2));
671           COMPS = BNCLOC-TACDRK**2;
672           TACDRK = .5*BNCLOC/COMPS;
673           TACDRK = TACDRK/COMPS;
674           IF TACDRK LES SCAL19
675           THEN TACDRK = SCAL19;
676         END;
677
678     COMMENT NAV CAP COMPUTATIONS;
679     IF NAVCAP
680     THEN BEGIN
681       IF NOT BNCLOC
682       THEN BEGIN
683         COMPS = ((BNCLOC**2)/.1)*SCAL4;
684         IF CTDRK LES .0
685         THEN BEGIN
686           COMPS = -COMPS;
687           COMPS = -COMPS;
688         END;
689         BNCLOC = -BNCLOC;
690         IF NOT ILSCAP
691         THEN BEGIN
692           BNCLOC = -BNCLOC;
693           BNCLOC = BNCLOC/COMPS;
694           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
695           TACDRK = TACDRK/((BNCLOC**2));
696           COMPS = BNCLOC-TACDRK**2;
697           TACDRK = .5*BNCLOC/COMPS;
698           TACDRK = TACDRK/COMPS;
699           IF TACDRK LES SCAL19
700           THEN TACDRK = SCAL19;
701         END;
702
703     COMMENT NAV CAP COMPUTATIONS;
704     IF NAVCAP
705     THEN BEGIN
706       IF NOT BNCLOC
707       THEN BEGIN
708         COMPS = ((BNCLOC**2)/.1)*SCAL4;
709         IF CTDRK LES .0
710         THEN BEGIN
711           COMPS = -COMPS;
712           COMPS = -COMPS;
713         END;
714         BNCLOC = -BNCLOC;
715         IF NOT ILSCAP
716         THEN BEGIN
717           BNCLOC = -BNCLOC;
718           BNCLOC = BNCLOC/COMPS;
719           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
720           TACDRK = TACDRK/((BNCLOC**2));
721           COMPS = BNCLOC-TACDRK**2;
722           TACDRK = .5*BNCLOC/COMPS;
723           TACDRK = TACDRK/COMPS;
724           IF TACDRK LES SCAL19
725           THEN TACDRK = SCAL19;
726         END;
727
728     COMMENT NAV CAP COMPUTATIONS;
729     IF NAVCAP
730     THEN BEGIN
731       IF NOT BNCLOC
732       THEN BEGIN
733         COMPS = ((BNCLOC**2)/.1)*SCAL4;
734         IF CTDRK LES .0
735         THEN BEGIN
736           COMPS = -COMPS;
737           COMPS = -COMPS;
738         END;
739         BNCLOC = -BNCLOC;
740         IF NOT ILSCAP
741         THEN BEGIN
742           BNCLOC = -BNCLOC;
743           BNCLOC = BNCLOC/COMPS;
744           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
745           TACDRK = TACDRK/((BNCLOC**2));
746           COMPS = BNCLOC-TACDRK**2;
747           TACDRK = .5*BNCLOC/COMPS;
748           TACDRK = TACDRK/COMPS;
749           IF TACDRK LES SCAL19
750           THEN TACDRK = SCAL19;
751         END;
752
753     COMMENT NAV CAP COMPUTATIONS;
754     IF NAVCAP
755     THEN BEGIN
756       IF NOT BNCLOC
757       THEN BEGIN
758         COMPS = ((BNCLOC**2)/.1)*SCAL4;
759         IF CTDRK LES .0
760         THEN BEGIN
761           COMPS = -COMPS;
762           COMPS = -COMPS;
763         END;
764         BNCLOC = -BNCLOC;
765         IF NOT ILSCAP
766         THEN BEGIN
767           BNCLOC = -BNCLOC;
768           BNCLOC = BNCLOC/COMPS;
769           TACDRK = .99999-((BNCLOC/COMPS)/BNCLOC);
770           TACDRK = TACDRK/((BNCLOC**2));
771           COMPS = BNCLOC-TACDRK**2;
772           TACDRK = .5*BNCLOC/COMPS;
773           TACDRK = TACDRK/COMPS;
774           IF TACDRK LES SC
```

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```

513 END I
514 BOMCNC = -RTAN(COM2*COM1) I
515 IF CPMONE... COMPUTE JABE... ON FIRST ITERATION
516 OF NAVCAP //
517 THEN BEGIN
518   ADDON = ADDON*COM1 I
519   BOMCNC = COM2*(((RTAN(ASIN(NAV/BCU1)
520   ADDON)))+(BOMCNC-SCAL11)/SCAL4)/(VGA*P1)
521   COM1 = SQR(1-ADDON*ADDON) I
522   TABE = 5-RTAN(BOMCNC*COM1) I ... VALUE
523   = ADDON*COM1 //
524 END I
525 EXPARC = -TAN(PI*0.01/(VGA*DELUPH*INEM*SCAL4)
526 /ADDON*P1) I
527 KOLNOR = EXPARC*EXPARC I
528 END
529 ELSE BOMCNC = BOMCNC*KOLNOR I
530 BOMCNC = BOMCNC I
531 DELCAP = BOMCNC-BOMCNC I
532 END
533 ELSE BEGIN
534   ... //
535   ... FINAL ILS CAPTURE COMPUTATIONS //
536   DELCAP = DELCAP*EXPARC I
537   BOMCNC = BOMCNC*DELCAP I
538   BOMCNC = BOMCNC I
539   DELINK = BOMCNC-CONDTK I
540 END
541 END
542 ELSE BEGIN
543   ... //
544   ... FINAL TRACK COMPUTATIONS //
545   DELINK = DELINK*EXPARC I
546   CONDTK = BOMCNC*DELINK I
547   BOMCNC = BOMCNC I
548 END I
549
550 CURRENT ..... OUTPUT CONTROL PROCESSING ..... I ... //
551 ... //
552 ... BANK END AND END MAIN LAY
553 COMPUTATIONS //
554
555 DELCND = BOMCNC-BOMCNC I
556 RATE = LIMIT(DELCONV*RATE) I
557 BOMCNC = BOMCNC*RATE I
558 BOMCNC = LIMIT(BOMCNC*AMPLIM) I
559 IF CPMONE
560 THEN BEGIN
561   BOMCNC = BOMCNC I
562   CPMONE = FALSE I
563 END I
564 BOMCNC = ((BOMCNC/SCAL11)/SCAL12)+(EXPARC*EXPARC*BOMCNC/SCAL13
565 +SCAL14)-((COMASS(BOMCNC,EXPARC,SCAL13,SCAL14)/SCAL11)/
566 SCAL12)
567 ... PASS BOMCNC THROUGH 425 + 1) / (.55
568 ... //
569 END I

```

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```

570 COMMENT .....
571 .....
572 COMMENT THE FOLLOWING CARDS MUST BE REMOVED BEFORE CROSS-COLLING :
573 .....
574 COMMENT .....
575 .....
576 .....
577 .....
578 .....
579 COMMENT .....
580 .....
581 COMMENT THE ABOVE CARDS MUST BE REMOVED BEFORE CROSS-COLLING :
582 .....
583 COMMENT .....
584 .....
585 .....
586 .....
587 .....
588 END FINI

```

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13-000000000000

1 BEGIN

2 DEFINE REAL PROCEDURE LIMIT(INPUT,LIMVAL) WHERE ... //

3 REAL INPUT,LIMVAL ... //

4

5

6

7

8

9

10

11

12

IF ABS(INPUT) LES LIMVAL

THEN LIMIT=LINPUT

ELSE LIMIT = (LIMVAL+ABS(INPUT))/INPUT ;

END ;

END FIN

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```

1 LS=ALS.LOP155
2 BEGIN
3 DEFINE REAL PROCEDURE LOPASS(INPUT,LSLOPS,STC,STINST) WHERE ... //
4 REAL INPUT,STC,STINST,LSLOPS ... //
5
6 BEGIN
7 LSLOPS = LSLOPS*(INPUT-LSLOPS)*(STINST/SFC) ;
8 LOPASS = LSLOPS ;
9 END ;
10
11 END FMI

```

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```

1  BEGIN
2
3  DEFINE REAL PROCEDURE NEXP(X) WHERE ... //
4  REAL X      ... //
5  FOR
6  BEGIN
7  X = -X
8  NEXP = 4922998 - 9990504 * X + 4962922 * X * X - 1525332 * X * X * X + 2721691 * X *
9  X * X * X
10 END
11
12 END FMT

```

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APPENDIX G

Program Listing Of Glideslope Routines



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J:WORKFILE.GSCF6DA1

```

1      BEGIN
2
3      DEFINE PROCEDURE GSCMP(GSLEV,D,HDOCT,T,RESETG,GSARM,GSCAP,
4      LOCAPM,PTCMDA) WHERE      ...
5      *****
6      *****
7      INPUTS
8      *****
9      ***** //
10     REAL D      ... DISTANCE TO TOUCHDOWN 100
11     NM FULL SCALE (+)
12     APPROACHING THE RMWY ;
13     REAL PTCMDA  ... EXTERNALLY SUPPLIED
14     STEERING COMMAND, 180 DEG
15     FULL SCALE ***NOTE*** THE
16     INPUT VALUE WILL BE
17     OVERWRITTEN IF AND ONLY IF
18     THIS ROUTINE IS IN THE
19     GSCAP STATUS. + IMPLIES
20     PITCH DOWN ;
21     BOOLEAN LOCAPM  ... TRUE PRIOR TO LOC CAPTURE ;
22     BOOLEAN RESETG  ... INITIALIZATION COMMAND ;
23     ... GSCMP IS SET TO THE ARM
24     STATUS AND ALL FILTERS ARE
25     INITIALIZED *** NOTE ***
26     THIS BOOLEAN SHOULD BE
27     EXTERNALLY SET FALSE AFTER
28     THE FIRST CALL TO GSCMP //
29     REAL T      ... TIME SINCE LAST CALL TO
30     GSCMP .. INTERNAL
31     COMPUTATIONS ASSUME THE
32     NOMINAL SAMPLE INTERVAL ON
33     THE FIRST ACCESS 10.804 HRS
34     FULL SCALE ;
35     REAL GSLEV    ... GLIDESLOPE RADIO DEVIATION
36     300 U-AMPS FULL SCALE (+)
37     ABOVE THE RMWY ;
38     REAL HDOCT    ... VERTICAL RATE 500 FEET /
39     SEC FULL SCALE (+) UPWARD ;
40     ...
41     *****
42     *****
43     OUTPUTS
44     *****
45     ***** //
46     BOOLEAN GSARM  ... GLIDESLOPE COMPUTATION
47     STATUS ;
48     BOOLEAN GSCAP  ... GLIDESLOPE COMPUTATION
49     STATUS //
50     TOBE
51     BEGIN
52
53     COMMENT ***** GAINS CONSTANTS AND CONVERSION FACTORS ***** ;
54     REAL PROCEDURE LOPASS,WSHOOT,LIMIT ;
55     REAL RY      ... DIVIDED BY 10) EQUALS
56     DEGREES OF PITCH COMMAND /

```

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```

57      FOOT OF LINEAR DEVIATION OR
58      MULTIPLIED BY MAXRNG /
59      .2016 EQUALS DEGREES OF
60      PITCH COMMAND PER U-AMP
61      BEYOND MAXRNG NM. ;
62      REAL KHDOT      ... DEGREES OF PITCH COMMAND /
63      FT PER SEC OF VERTICAL RATE
64      ;
65      REAL KYDOT      ... MULTIPLIED BY
66      KHDOT*KDIS*MAXRNG / .2016
67      EQUALS DEGREES OF PITCH
68      COMMAND PER U-AMP / SEC OR
69      MULTIPLIED BY KHDOT / 10.
70      EQUALS DEGREES OF PITCH
71      COMMAND PER FT / SEC OF
72      LINEAR DEVIATION RATE ;
73      REAL MAXRNG      ... DISTANCE BEYOND WHICH
74      DEVIATION (DELTA) IS
75      EXPRESSED IN U-AMPS (SCALE
76      IDENTICAL TO RNGID) ;
77      REAL DYTOT      ... NM(DISTANCE) -SMALL
78      DOTS(DEVIATION) PER FOOT OF
79      DEVIATION, A 2.5 DEGREE
80      GLIDESLOPE IS ASSUMED ;
81      REAL GAIN10      ... REAL GAIN10 ...DIVISION BY
82      THIS CONSTANT WILL YIELD A
83      GAIN OF 10 ;
84      REAL GAIN5      ... DIVIDE BY FOR GAIN OF 5 ;
85      REAL GAIN.5      ... MULTIPLY BY GAIN.5 FOR GAIN
86      OF .5 ;
87      REAL ARRAY SCALE(1) ... AND ARRAY OF SCALE FACTORS
88      ;
89      REAL DELTAT      ... SAMPLE INTERVAL 1000. SEC
90      FULL SCALE ;
91      REAL TNOF      ... NOMINAL SAMPLE INTERVAL
92      SAME SCALE AS DELTAT ;
93      REAL TC1      ... FILTER TIME CONSTANT ;
94      REAL TC2      ... FILTER TIME CONSTANT ;
95      REAL TC3      ... FILTER TIME CONSTANT SCALE
96      THE SAME AS DELTAT ;
97      REAL TC4      ... FILTER TIME CONSTANT ;
98      REAL TC5      ... LAG TIME CONSTANT ;
99      REAL ONE      ... UNITY ;
100     REAL ZERO      ... 0.0 ;
101
102     COMMENT ***** INTERNAL VARIABLES ***** ;
103     REAL LIN2      ... PREVIOUS FILTER INPUT ;
104     REAL LIN3      ... PREVIOUS FILTER INPUT ;
105     REAL LIN4      ... PREVIOUS FILTER INPUT ;
106     REAL LOUT1      ... PREVIOUS FILTER OUTPUT ;
107     REAL LOUT2      ... PREVIOUS FILTER OUTPUT ;
108     REAL LOUT3      ... PREVIOUS FILTER OUTPUT ;
109     REAL LOUT4      ... PREVIOUS FILTER OUTPUT ;
110     REAL LOUT5      ... PREVIOUS FILTER OUTPUT ;
111     REAL DELTAH      ... LINEAR FEET TO THE
112     GLIDESLOPE CLIM //
113     ... OR ( BEYOND MAXRNG ) THE

```

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114		ANGULAR ERROR IN THE FLIGHT
115		PATH ANGLE WITH RESPECT TO
116		THE GLIDESLOPE //
117		... DIVIDE MAXRNG BY DYTOFT TO
118		GET FULL SCALE FEET - - -
119		NUM 1000 FOR 3.76 NM AND A
120		2.5 DEGREE GLIDESLOPE ;
121	REAL YDOT	... RADIO DEV RATE ( BEYOND
122		MAXRNG ) OR CONVERGENCE
123		RATE ( INSIDE MAXRNG ) FULL
124		SCALE U - AMPS / SEC =
125		MAXRNG / DYTOFT OF FULL
126		SCALE FT / SEC = MAXRNG /
127		DYTOFT ;
128	REAL DEVRTE	... BLAM CLOSURE RATE U-AMPS /
129		SEC OR FT / SEC ;
130	REAL PTCMD	... PITCH COMMAND 100 DEGREES
131		FULL SCALE. + INFLIES
132		PITCH DOWN ;
133	REAL MAXCMD	... ILS PITCH COMMAND LIMIT 100
134		DEGREES ;
135	REAL TMAX	... LARGEST RECOGNIZED TIME
136		STEP ;
137	REAL TMIN	... SMALLEST RECOGNIZED TIME
138		STEP ;
139	REAL IEMP	... INITIAL COMPOSITE ILS AND
140		EXTERNAL PITCH COMMAND FOR
141		TRANSITION TO TOTAL ILS
142		CONTROL ;
143	REAL Y	... FILTERED RADIO DEVIATION ;
144	REAL HDUTLL	... FILTERED ALTITUDE RATE ;
145	REAL LOGRFR	... LEAD BREAK FREQUENCY RAD/SEC
146		
147	COMMENT ***** COMPILATION VALUES ***** ;	
148	PRESET	
149	BEGIN.	
150	GAIN.5 = .5 ;	
151	GAIN.5 = .2 ;	
152	GAIN.10 = .1 ;	
153	INOM = .0002 ;	
154	DYTOFT = .1008 ;	
155	KHDCI = .15 ;	
156	KY = .75 ;	
157	KYDOT = .66 ;	
158	MAXRNG = .0556 ;	
159	SCALE(0) = .5667 ;	
160	SCALE(1) = .025707 ;	
161	LOGRFR = .5 ;	
162	TC1 = .0005 ;	
163	TC2 = .002 ;	
164	TC3 = .02 ;	
165	TC4 = .005 ;	
166	TC5 = .001 ;	
167	TMAX = .00025	
168		... SET TO ONE HALF OF THE
169		SMALLEST FILTER TIME
170		CONSTANT ;
	TMIN = .0001	... SET TO AT LEAST THE



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```

171
172
173
174      MAXCMD = .1 ;
175      ONE = .99999999 ;
176      ZERO = .0 ;
177      END ;
178
179      COMMENT *****EXECUTABLE PROGRAM ***** ;
180      IF RESETG      ... INITIALIZE STATE
181                      LOGIC,RADIO LOWPASS FILTER
182                      AND THE TIME INTERVAL //
183      THEN BEGIN
184          DELTA1 = TNOM ;
185          GSARM = TRUE ;
186          GSCAP = FALSE ;
187          HDOTLL = LOUT5 = HDOT ;
188                      ... INITIALIZE LEAD-LAG ON
189                      HDOT //
190          Y = LOUT1 = GSDEV $, ... INITIALIZE FILTERED RADIO
191                      DEVIATION TO AVOID FALSE
192                      CAPTURES //
193      END
194      ELSE BEGIN
195          DELTA1 = 1/SCALE(1) ; ... CONVERT TO 1000 SEC FULL
196                      SCALE //
197          IF DELTA1 GEQ Tmax OR DELTA1 LEQ Tmin
198          THEN DELTA1 = TNOM ... LIMIT SAMPLE INTERVAL ;
199          HDOTLL = HDOT-(LOPASS(HDOT,LOUT5,TC5,DELTA1))*LDBRR
200                      ;
201          HDOTLL = HDOTLL/LDBRR ;
202                      ... LEAD-LAG FILTERED HDOT //
203          Y = LOPASS(GSDEV,LOUT1,TC1,DELTA1) ... FILTER
204                      RAW DEVIATION ;
205      END ;
206
207      COMMENT ***** ESTIMATE THE DISTANCE TO THE BEAM ***** ;
208      DELTAH = Y*
209      IF D GEQ MAXRNG      ... BEYOND MAXRNG THE DEVIATION
210                      IS ESTIMATED WITH RESPECT
211                      TO ANGULAR ERROR //
212
213      THEN MAXRNG
214      ELSE 0      ... INSIDE MAXRNG DELTAH IS
215                      EQUAL TO THE LINEAR
216                      DISTANCE TO THE BEAM IN
217                      FEET ;
218      DELTAH = DELTAH/DTTOFT      ... UNITS CONVERSION ;
219
220      COMMENT ***** DERIVE BEAM CLOSURE RATE ***** ;
221      IF RESETG
222      THEN BEGIN
223          LINT2 = DELTAH $,
224          LOUT2 = ZERO      ... INITIALIZE RATE DERIVER TO
225                      CURRENT INPUT AND ZERO
226                      OUTPUT //
227      END $,

```

```

228      IF GSARM
229      THEN YDOT = WSHOUT(DELTAH,LOUT2,TC2,DELTAI,LIN2)*GAIN.5
230      ... AFTER THE CAPTURE CONDITION
231      HAS BEEN MET CLOSURE RATE
232      WILL BE COMPUTED FROM HDOT
233      ALONE ;
234      DEVRTL = KYDOT+YDOT/GAIN.10 ;
235      DEVRTL = (HDOTLL+DEVRTL)/GAIN.5 ;
236      IF GSCAP
237      THEN DEVRTL = WSHOUT(DEVRTL,LOUT3,TC3,DELTAI,LIN3)
238      ... WASHOUT THE YDOT BIAS AND
239      THE STEADY STATE VALUE OF
240      HDOT //
241      ELSE LIN3 = LOUT3 = DEVRTL ... INITIALIZE THE WASHOUT
242      TO EXACTLY DEVRTL ;
243
244      COMMENT ***** COMPUTE THE PITCH COMMAND ***** ;
245      PTCMD = KY*DELTAH ... FORWARD FEED ;
246      PTCMD = PTCMD+(DEVRTL*KHDOT) ... RATE DAMPENING ;
247      PTCMD = LIMIT(PTCMD,MAXCMD) ... LIMIT THE COMMAND SIZE ;
248      PTCMD = PTCMD*SCALE(0) ... CONVERT TO 180 DEGREES FULL
249      SCALE ;
250
251      COMMENT ***** TEST FOR CAPTURE ***** ;
252      IF GSARM
253      THEN BEGIN
254      GSCAP = ((Y LEQ ZERO) AND (PTCMD GEQ ZERO)) OR ((Y
255      GEQ ZERO) AND (PTCMD LEQ ZERO)) ... TEST FOR
256      CAPTURE ;
257      IF LOCARM THEN GSCAP = FALSE ; ... WAIT FOR LOC //
258      GSAPL = NOT GSCAP ;
259      TEMP = LIN4 = LOUT4 = PTCMDA-PTCMD ... PREPARE TO
260      TRANSITION TO ILS //
261      END ;
262
263      COMMENT ***** OUTPUT THE PITCH STEERING COMMAND ***** ;
264      IF GSARM
265      THEN ... DO NOT OVERWRITE EXTERNAL
266      COMMAND //
267      PTCMDA = PTCMD
268      ELSE PTCMDA = PTCMD+WSHOUT(TEMP,LOUT4,TC4,DELTAI,LIN4)
269      ... FADE OUT EXTERNAL COMMAND ;
270      END ;
271
272      END FINI

```

RT+S D-LIMRGAL

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WORKFILE.LIMRGOA1

```
1      BEGIN
2
3      DEFINE REAL PROCEDURE LIMIT(INPUT,LIMVAL) WHERE REAL LIMVAL,
4                                     ... LARGEST ALLOWABLE OUTPUT
5                                     MAGNITUDE //
6      INPUT                                     ... INPUT VALUE : TEMP
7      BEGIN
8      REAL TEMP ;
9      IF INPUT LES .0 THEN TEMP = -INPUT
10     ELSE TEMP = INPUT ;
11     IF TEMP GT LIMVAL ... LIMIT TEST //
12     THEN LIM1 = LIMVAL*TEMP/INPUT ... SATURATION //
13     ELSE LIM1 = INPUT ;
14     END ;
15
16     END FIN1
```

FIN



DD:POPKFILE.SHRGDA1

```

1      BEGIN
2
3      DEFINE REAL PROCEDURE WSHOUT(INPUT,LSTOUT,TC,T,LASTIN)
4      WHERE REAL INPUT      ... CURRENT INPUT SIGNAL ;
5      REAL LASTIN           ... LAST INPUT SIGNAL ;
6      REAL LSTOUT           ... LAST OUTPUT SIGNAL ;
7      REAL TC               ... FILTER TIME CONSTANT ;
8      REAL T                ... REAL T ...SAMPLE INTERVAL
9                               ... NOTE TC AND T MUST HAVE
10                              THE SAME SCALING !!
11
12      TCBE
13      BEGIN
14      REAL K1,K2 ;
15          K1 = TC/(TC+.5*T) ...      FOR T = 0. 10
16          TC / 2 ;
17          K2 = (TC-.5*T)/(TC+.5*T) S.
18      LSTOUT = K2*LSTOUT+(INPUT-LASTIN)*K1 S.
19      WSHOUT = LSTOUT ;
20      LASTIN = INPUT ;
21      END ;
22      END FTHI

```

SPRTS D.LINRGA1

40\*WORKFILE.LCPRGDA1

```

1      BEGIN
2
3      DEFINE REAL PROCEDURE LOPASS(INPUT,LSTOUT,TC,T)
4      WHERE REAL INPUT      ... CURRENT INPUT SIGNAL ;
5      REAL LSTOUT           ... LAST OUTPUT SIGNAL ;
6      REAL TC               ... FILTER TIME CONSTANT ;
7      REAL T                ... REAL T ...SAMPLE INTERVAL ;
8                           ... NOTE TC AND T MUST HAVE THE
9                           SAME SCALING //
10
11     TOBL
12     BEGIN
13     REAL K1,K2 ;
14         K1 = T/TC ;
15         K2 = (TC-T)/TC ;
16     LSTOUT = K1*INPUT+K2*LSTOUT ;
17     LOPASS = LSTOUT ;
18     END ;
19     END FINI

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40PRT.S D.WSRGDA1

LIST OF REFERENCES

1. AGM-329, "Use of Area Navigation Computations to Aid in Localizer Capture," by T. G. Sharpe and W. A. Savold dated 21 June 1972.
2. Digital Flight Director Proposal (523-0764380-00111P), Section 2.2, "Initial Synthesis of Control Laws", by T. G. Sharpe dated 26 April 1972.
3. AGM-501, "Second Order Filter for Localizer Data to Improve Performance of Capture and Track Laws", by T. G. Sharpe dated September 4, 1975.
4. AGM-497, "Area Nav Aided Localizer Captures for 3D/4D Program, Part II: Software Development and Simulation Results", by L. H. Hogle dated 28 August 1975.
5. FAA Advisory Circular, "Automatic Landing System (ALS)", dated 12 January 1971.